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A COMPUTER CODE FOR A ONE-DIMENSIONAL DYNAMIC MODEL OF  
THE MESOSPHERES AND (U) AIR FORCE GEOPHYSICS LAB  
HANSCOM AFB MA T J KENESHA ET AL. 07 MAR 84

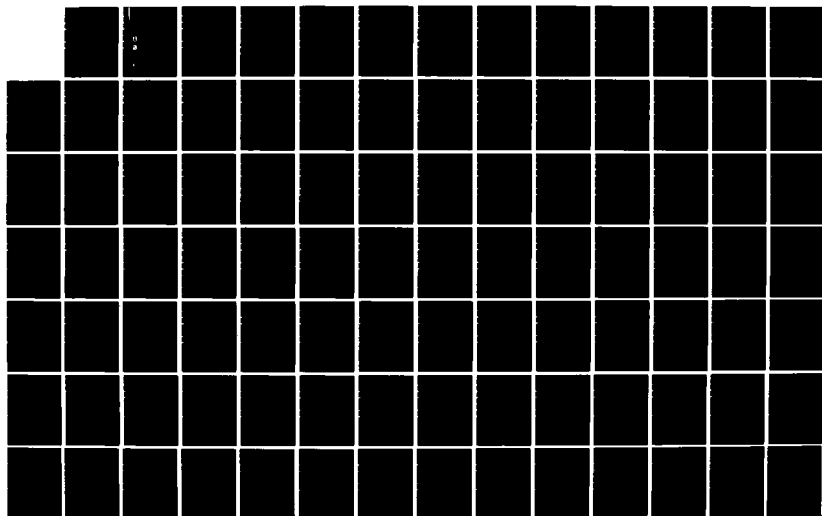
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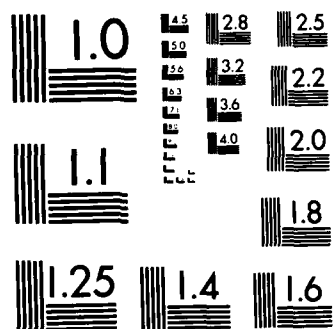
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## A Computer Code for a One-Dimensional Dynamic Model of the Mesosphere and Lower Thermosphere

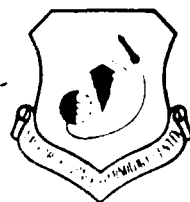
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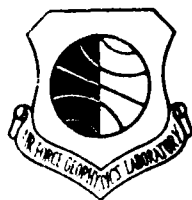
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ATMOSPHERIC SCIENCES DIVISION

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## Contents

1. INTRODUCTION	7
2. THE EQUATIONS OF STATE	8
3. THE FINITE DIFFERENCE EQUATIONS	11
4. BOUNDARY CONDITIONS	15
5. COLLISION FREQUENCIES	19
6. THE CHEMISTRY AND PHOTOCHEMISTRY	21
6.1 The Photodissociation Rate Coefficients	23
6.2 The Photoionization Rate Coefficients	24
6.3 Electron Impact Ionization	25
6.4 The Thermal Diffusion Factors	26
7. A MID-LATITUDE ATMOSPHERE SIMULATION	26
7.1 Initial Conditions	27
7.2 Thermospheric Results	30
7.3 Mesospheric Results	32
REFERENCES	51
APPENDIX A: THE CHEMICAL REACTIONS	55
APPENDIX B: PHOTODISSOCIATION PROCESSES AND THEIR RATE COEFFICIENTS	65
APPENDIX C: THE COMPUTER CODE	130

1. The Static Temperature Profile	29
2. The Turbulent Diffusion Coefficients as Determined From the Chemical Release Data Obtained From the ALADDIN I Experiments	29
3. The Time Invariant Height Profiles of $N_2$ , $O_2$ , Helium, and Argon. Above about 100 km, atomic oxygen is also invariant. Below 100 km, the noon and midnight profiles of atomic oxygen are shown	33
4. The Ratio of Atomic to Molecular Oxygen at Four Different Times During the Day. These curves reflect the diurnal variations of atomic oxygen in the mesosphere	
5. The Noontime Profiles of $H_2$ , $H_2O$ , $NO$ , $N_2O$ , $CO$ , and $CO_2$ in the Mesosphere and Lower Thermosphere	34
6. The Ratio of Carbon Dioxide to Argon at Four Different Times During the Day. The curves show the diurnal variation of carbon dioxide in the lower thermosphere	34
7. The Iso-Density Contours for Atomic Nitrogen	35
8. The Iso-Density Contours for Nitric Oxide	35
9. The Iso-Density Contours for $N^2D$	36
10. The Iso-Density Contours for Carbon Dioxide. The contours indicate a lack of any diurnal variation for this species below 150 km	36
11. The Iso-Density Contours for $O^1D$	37
12. The Iso-Density Contours for $O^+$ . The contours show the daytime F-layer peak ionization in excess of $10^6 \text{ cm}^{-3}$	37
13. The Iso-Density Contours for $O^+(^2D)$	38
14. The Iso-Density Contours for $O_2^+$	38
15. The Iso-Density Contours for $NO^+$	39
16. The Iso-Density Contours for $H^+$	39
17. The Iso-Density Contours for $N^+$	40
18. The Iso-Density Contours for $N_2^+$ . At night, the concentration of $N_2^+$ falls below $1 \text{ cm}^{-3}$ at all altitudes	40
19. The Iso-Density Contours for the Electrons Showing the Diurnal Change in the Altitude of the Peak Electron Concentration	41
20. Measurements of the Height of the F-Layer Peak at Eglin AFB, Fla., on 20/21 November 1970	41
21. The Total Electron Content Compared With Calculations Including Horizontal Winds	42
22. The Total Electron Content Compared With Measurements Taken at Boulder, Colo.	42
23. The Total Electron Content Compared With Measurements Taken at Boulder, Colo., and Lancaster, England	44
24. The Iso-Density Contours for $O_2^-$ in the Mesosphere	44
25. The Iso-Density Contours for $CO_3^-$ in the Mesosphere	45
26. The Iso-Density Contours for $NO_3^-$ in the Mesosphere	45

27. The Iso-Density Contours for $H_5O_2^+$ in the Mesosphere	46
28. The Iso-Density Contours for $H_7O_3^+$ in the Mesosphere	46
29. The Iso-Density Contours for $H_9O_4^+$ in the Mesosphere	47
30. The Iso-Density Contours for $H_{11}O_5^+$ in the Mesosphere	47
31. The Iso-Density Contours for $NO^+ \cdot H_2O$ in the Mesosphere	48
32. The Iso-Density Contours for $NO^+ \cdot (H_2O)_2$ in the Mesosphere	48
33. Altitude Profiles of Electron Density From Three Rocket Experiments at Wallops Island	49
34. Altitude Profiles of the Electron Concentration From This Model at Several Zenith Angles During Sunrise	49
35. Altitude Profiles of $NO^+$ , $O_2^+$ , $NO^+ \cdot H_2O$ , Electrons and $\lambda$ , the Ratio of Negative Ions to Electrons	50

Tables

1. Polarizabilities of Neutral Cases	20
2. The Average Reduced Charge Exchange Collision Frequencies Between Like Particles	21
A1. Chemical Reaction Scheme	56-60
B1. Solar Fluxes and Absorption Cross Sections for $O_2$ , $O_3$ , $H_2O$ , $H_2O_2$ , $NO_2$ , $NO_3$ , and $N_2O$	72-75
B2. Absorption Cross Sections for $N_2O_5$ , $HNO_2$ , $HNO_3$ , $CH_4$ , $CO_2$ , $CH_2O$ , and $HO_2$	76-78
B3. Total Photodissociation Rate Coefficients for Unattenuated Solar Flux	79
B4. Total Photodissociation Rate Coefficients for the Process $O_2 + h\nu \rightarrow O + O(^1D)$ for the Wavelengths Below 175 nm	80-82
B5. Total Photodissociation Rate Coefficients for the Process $O_2 + h\nu \rightarrow O + O$ for Wavelengths From 175 to 242.2 nm	83-85
B6. Total Photodissociation Rate Coefficients for the Process $O_3 + h\nu \rightarrow O(^1D) + O_2(^1\Delta_g)$ for Wavelengths Below 310 nm	86-88
B7. Total Photodissociation Rate Coefficients for the Process $O_3 + h\nu \rightarrow O + O_2$ for Wavelengths From 310 to 730 nm	89
B8. Total Photodissociation Rate Coefficients for the Process $H_2O + h\nu \rightarrow OH + H$ for Wavelengths From 121.9 to 186.4 nm	90-92
B9. Total Photodissociation Rate Coefficients for the Process $H_2O_2 + h\nu \rightarrow OH + OH$ for Wavelengths From 188.2 to 303 nm	93-95

B10.	Total Photodissociation Rate Coefficients for the Process $\text{NO}_2 + h\nu \rightarrow \text{NO} + \text{O}(^1\text{D})$ for Wavelengths From 190 to 420 nm	96-97
B11.	Total Photodissociation Rate Coefficients for the Process $\text{NO}_3 + h\nu \rightarrow \text{NO} + \text{O}_2$ for Wavelengths From 450 to 680 nm	98
B12.	Total Photodissociation Rate Coefficients for the Process $\text{N}_2\text{O} + h\nu \rightarrow \text{N}_2 + \text{O}(^1\text{D})$ for Wavelengths From 190 to 315 nm	99-101
B13.	Total Photodissociation Rate Coefficients for the Process $\text{N}_2\text{O}_5 + h\nu \rightarrow \text{NO}_2 + \text{NO}_2 + \text{O}$ for Wavelengths From 210 to 380 nm	102-104
B14.	Total Photodissociation Rate Coefficients for the Process $\text{HNO}_2 + h\nu \rightarrow \text{OH} + \text{NO}$ for Wavelengths From 300 to 390 nm	105
B15.	Total Photodissociation Rate Coefficients for the Process $\text{HNO}_3 + h\nu \rightarrow \text{OH} + \text{NO}_2$ for Wavelengths From 192 to 325 nm	106-108
B16.	Total Photodissociation Rate Coefficients for the Process $\text{CH}_4 + h\nu \rightarrow \text{CH}_3 + \text{H}$ and $\text{CH}_4 + h\nu \rightarrow \text{CH}_2 + \text{H}_2$ for Wavelengths From 116 to 164 nm	109-111
B17.	Total Photodissociation Rate Coefficients for the Process $\text{CO}_2 + h\nu \rightarrow \text{CO} + \text{O}(^1\text{D})$ for Wavelengths From 116.2 to 166 nm	112-114
B18.	Total Photodissociation Rate Coefficients for the Process $\text{CO}_2 + h\nu \rightarrow \text{CO} + \text{O}$ for Wavelengths From 166 to 215 nm	115-117
B19.	Total Photodissociation Rate Coefficients for the Process $\text{CH}_2\text{O} + h\nu \rightarrow \text{CHO} + \text{H}$ and $\text{CH}_2\text{O} + h\nu \rightarrow \text{CO} + \text{H}_2$ for Wavelengths From 240 to 360 nm	118-119
B20.	Total Photodissociation Rate Coefficients for the Process $\text{HO}_2 + h\nu \rightarrow \text{O}_2 + \text{H}$ for Wavelengths From 180 to 274 nm	120-122
B21.	EUV Solar Fluxes and Cross Sections	123-124
B22.	Electron Impact Ionization Cross Sections	125
B23.	Rate Coefficients for Energetic Electron Impact Reactions	125-127

# A Computer Code for a One-Dimensional Dynamic Model of the Mesosphere and Lower Thermosphere

## 1. INTRODUCTION

T.J. Keneshea, one of the authors, pioneered studies of the numerical solution of sets of continuity equations in the atmosphere. He was the first to find that these equations were "stiff" and were not solvable efficiently by any numerical technique then available. His efforts<sup>1,2,3</sup> led to a computer simulation of the composition of the upper atmosphere that could be run inexpensively on the large scale computers available in those days. After these computer codes were applied to the undisturbed atmosphere<sup>4</sup> and to several natural<sup>5</sup> and manmade atmospheric disturbances, it became apparent that they could not predict long term atmospheric behavior.

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(Received for publication 1 March 1984)

1. Keneshea, T.J. (1962) A Computer Program for Solving the Reaction Rate Equations in the E Ionospheric Region, AFCRL-62-828.
2. Keneshea, T.J. (1963) A Solution to the Reaction Rate Equations in the Atmosphere Below 150 Kilometers, AFCRL-63-711.
3. Keneshea, T.J. (1967) A Technique for Solving the General Reaction Rate Equations in the Atmosphere, AFCRL-67-0221, AD654010.
4. Keneshea, T.J., Narcisi, R.S., and Swider, W., Jr. (1970) Diurnal model of the E-region, J. Geophys. Res. 75:845-854.
5. Keneshea, T.J., and Fowler, R.J. (1966) Computed Electron, Ion, and Neutral Density Profiles for the Solar Eclipse of 12 November 1966, AFCRL-66-741, AD646975.

Such simple computer codes, in which only chemical reactions among the atmospheric gases are considered, are excellent for determining short term variations of the atmosphere, but give completely erroneous results for solutions beyond a few hours. In fact, these codes are valid only for solution times shorter than the transport time constants for the various atmospheric gases.

It then became obvious that any realistic atmospheric simulation should be based upon the equations of motion for the particles as well as their continuity equations. This report describes in detail a computer scheme for solving large sets of coupled partial differential equations of conservation of mass and momentum and also presents the computer code itself with instructions for using it. Also included are the results of an application of the code to the development of a one-dimensional midlatitude winter simulation of the composition of the mesosphere and lower thermosphere.

## 2. THE EQUATIONS OF STATE

The equation for the conservation of particles of a particular gas within a multicomponent gas mixture is

$$\frac{\partial n_i}{\partial t} = P_i - n_i L_i - \nabla \cdot \vec{\Phi}_i \quad (1)$$

where  $n_i$  is the concentration of species  $i$ ,  $P_i$  is the rate at which it is formed, and  $n_i L_i$  is the rate at which it is removed through gas phase chemical reactions with other members of the ensemble. The vector flux of the species,  $\vec{\Phi}_i$ , is induced by a combination of all nonchemical processes. In this report, only molecular and eddy diffusion will be considered in the flux term

$$\vec{\Phi}_i = n_i \vec{C}_i + n_i \vec{V}_i \quad (2)$$

where  $\vec{C}_i$  is the velocity of species  $i$  resulting from molecular diffusion and  $\vec{V}_i$  is the velocity resulting from eddy diffusion. Since only the vertical distribution of species is to be considered here, the continuity equation can be written as

$$\frac{\partial n_i}{\partial t} = P_i - n_i L_i - \frac{\partial}{\partial Z} (n_i w_i + n_i v_i) \quad (3)$$

where  $w_i$  and  $v_i$  are the vertical components of the velocities  $\vec{C}_i$  and  $\vec{V}_i$  respectively.



The equation of motion for a neutral gas particle in a multicomponent gas mixture can be written as<sup>6</sup>

$$\frac{\partial \vec{C}_i}{\partial t} + \frac{1}{\rho_i} \nabla p_i + \frac{\alpha_i p_i}{\rho_i} \nabla \ln T - \vec{g} = - \sum_j \nu_{ij} (\vec{C}_i - \vec{C}_j) \quad (4)$$

where  $\rho_i = n_i m_i$  is the mass density of species  $i$ ,  $\alpha_i$  is its thermal diffusion factor in a multicomponent mixture,  $p_i$  is its partial pressure,  $T$  is the temperature of the mixture,  $\vec{g}$  is the acceleration of gravity, and  $\nu_{ij}$  is the collision frequency of species  $i$  with species  $j$ . The equation of motion is written here in terms of the collision frequencies between particles rather than the molecular diffusion coefficients in a multicomponent gas as was done by Keneshea and Zimmerman<sup>7</sup> and Keneshea et al.<sup>8</sup> The pressure of the gas is simply

$$p_i = n_i kT \quad (5)$$

where  $k$  is Boltzmann's constant. Therefore, in the one-dimensional case

$$\frac{1}{\rho_i} \nabla p_i + \alpha_i \frac{p_i}{\rho_i} \nabla \ln T + g = \frac{kT}{m_i} \left[ \frac{1}{n_i} \frac{\partial n_i}{\partial Z} + \frac{(1 + \alpha_i)}{T} \frac{\partial T}{\partial Z} + \frac{1}{H_i} \right] \quad (6)$$

where  $m_i$  is the mass of species  $i$  and  $H_i = kT/m_i g$  is its scale height. The equation of motion in the vertical direction for a neutral gas particle can then be written as

$$\frac{\partial w_i}{\partial t} + \frac{kT}{m_i} \left[ \frac{1}{n_i} \frac{\partial n_i}{\partial Z} + \frac{(1 + \alpha_i)}{T} \frac{\partial T}{\partial Z} + \frac{1}{H_i} \right] = - \sum_j \nu_{ij} (w_i - w_j). \quad (7)$$

If inertial effects are ignored, then the equation of motion for ions and electrons in the presence of both magnetic and electric fields are<sup>9</sup>

6. Chapman, S., and Cowling, T.G. (1970) The Mathematical Theory of Non-Uniform Gases, Cambridge University Press
7. Keneshea, T.J., and Zimmerman, S.P. (1970) The effect of mixing upon atomic and molecular oxygen in the 70-170 km region of the atmosphere, J. Atmos. Sci. 27:831-840.
8. Keneshea, T.J., Zimmerman, S.P., and Philbrick, C.R. (1979) A dynamic model of the mesosphere and lower thermosphere, Planet. Space Sci. 27:385-401.
9. Banks, P.M., and Kockarts, G. (1973) Aeronomy, Part A and Part B, Academic Press, New York.

$$\frac{\partial \vec{C}_i}{\partial t} + \frac{1}{\rho_i} \nabla p_i - \vec{g} - \frac{q_i}{m_i} (\vec{E} + \frac{1}{c} \vec{C}_i \times \vec{B}) = - \sum_j \nu_{ij} (\vec{C}_i - \vec{C}_j) \quad (8)$$

and

$$\frac{\partial \vec{C}_e}{\partial t} + \frac{1}{\rho_e} \nabla p_e - \vec{g} - \frac{q_e}{m_e} (\vec{E} + \frac{1}{c} \vec{C}_e \times \vec{B}) = - \sum_j \nu_{ej} (\vec{C}_e - \vec{C}_j)$$

where  $q$  is the particle charge,  $m$  is its mass,  $\vec{E}$  is the total electric field vector,  $c$  is the speed of light, and  $\vec{B}$  is the magnetic field vector. After much algebra, ignoring the horizontal component of the electric field as well as the horizontal velocities of the particles, and assuming that the electron and the ion temperatures are the same as the temperature of the neutral gas mixture, the equation of motion for the vertical velocities of the ionic species becomes

$$\begin{aligned} \frac{\partial w_i}{\partial t} + \frac{kT}{m_i} \left[ \frac{1}{n_i} \frac{\partial n_i}{\partial Z} + \frac{1}{n_e} \frac{\partial n_e}{\partial Z} + \frac{2}{T} \frac{\partial T}{\partial Z} + \frac{1}{H_i} \right] \\ = -w_i \sum_j \nu_{ij} \left\{ \frac{\Omega_i^2 + \left( \sum_j \nu_{ij} \right)^2}{\Omega_i^2 \sin^2 I + \left( \sum_j \nu_{ij} \right)^2} \right\} + \sum_j \nu_{ij} w_j \end{aligned} \quad (9)$$

where  $n_e$  is the concentration of the electrons,  $I$  is the magnetic dip angle, and

$$\Omega_i = \frac{B_0 e}{m_i c} \quad (10)$$

where  $B_0$  is the magnitude of the magnetic field and  $e$  is the charge on the electron.

The eddy diffusion velocity, taken from the formulation of Colegrove et al,<sup>10</sup> is

$$v_i = -K \left[ \frac{1}{n_i} \frac{\partial n_i}{\partial Z} + \frac{1}{T} \frac{\partial T}{\partial Z} + \frac{1}{H} \right] \quad (11)$$

where  $K$  is the vertical eddy diffusion coefficient and  $H$  is the scale height of the mean mass.

10. Colegrove, F.D., Johnson, F.S., and Hanson, W.B. (1966) Atmospheric composition in the lower thermosphere, J. Geophys. Res. 71:2227-2236.

Whenever a photodissociation rate coefficient is needed in the calculations, the  $O_2$  and  $O_3$  column densities are estimated and a simple table look-up is made for the particular  $J_j$  required.

A short discussion of each photodissociation process and the photodissociation rate coefficient tables are presented in Appendix B.

## 6.2 The Photoionization Rate Coefficients

Reactions 185 through 191 and reactions 206 and 207 in the list of reactions in Appendix A are the photoionization processes considered in this report. The EUV solar fluxes, the total absorption cross sections for  $O_2$ ,  $N_2$ , and  $O$ , and the ionization cross sections for  $O_2$ ,  $N_2$ ,  $O$ ,  $H$ , and  $He$  are listed in Table B21. The EUV solar fluxes from 1 to 121.57 nm are from the compilation of Manson.<sup>18</sup> The X-ray fluxes below 1 nm are taken from Swider.<sup>19</sup> The cross sections for total absorption and for total photoionization of  $O_2$ ,  $N_2$ , and  $O$  were obtained from a consideration of reported experimental and theoretical values. References, definitions, and a discussion of the absorption spectra can be found in Huffman<sup>20</sup> for wavelengths to 30.4 nm. For shorter wavelengths, the values given by Swider<sup>19</sup> were used. A discussion of some photoionization rate coefficients can be found in Keneshea and Huffman.<sup>21</sup> The photoionization cross sections for  $N$ ,  $H$ , and  $He$  are taken from Banks and Kockarts.<sup>9</sup>

The photoionization of the metastable  $O_2(^1\Delta_g)$  molecule has been included in these calculations. The wavelength region of interest is from 102.7 to 111.8 nm, where ground state  $O_2$  is the primary absorber of the incident solar radiation but is not ionized itself. The effective absorption coefficient for  $O_2$  and the ionization cross section for  $O_2(^1\Delta_g)$  are taken from Huffman et al.<sup>22</sup> Nitric oxide is ionized readily by Lyman  $\alpha$  radiation. The ionization cross section for  $NO$  at Lyman  $\alpha$  is  $2 \times 10^{-18} \text{ cm}^2$  as given by Watanabe.<sup>23</sup>

- 
18. Manson, J.E. (1976) Satellite Measurements of Solar UV During 1974, AFCRL-TR-76-0006, AD A021490.
  19. Swider, W., Jr. (1969) Ionization rates due to the attenuation of 1-100A non-flare solar X rays in the terrestrial atmosphere, Rev. Geophys. 7:573-594.
  20. Huffman, R.E. (1972) Photochemical processes. Cross-section data, Chapter 12, in Defense Nuclear Agency Reaction Rate Handbook, DNA 1948H.
  21. Keneshea, T.J., and Huffman, R.E. (1972) Solar Photoionization Rate Constants and Ultraviolet Intensities, AFCRL-72-0667.
  22. Huffman, R.E., Paulsen, D.E., Larrabee, J.C., and Cairns, R.B. (1971) Decrease in D-region  $O_2(^1\Delta_g)$  photoionization rates resulting from  $CO_2$  absorption, J. Geophys. Res. 76:1028-1038.
  23. Watanabe, K. (1954) Photoionization and total absorption cross sections of gases. I. Ionization potentials of several molecules. Cross sections of  $NH_3$  and  $NO$ , J. Chem. Phys. 22:1564-1570.

The total rate coefficient is obtained simply by summing  $J_j(\lambda)$  over all the wavelengths.

$$J_j = \sum_{\lambda} \sigma'_j(\lambda) I_0(\lambda) e^{-\sum_i \sigma_i(\lambda) N_i} \quad (54)$$

## 6.1 The Photodissociation Rate Coefficients

Reactions 192 through 205 in the list of reactions in Appendix A are the photodissociation processes considered in this report. In computing the transmittance, only molecular oxygen and ozone are considered as absorbers of the solar radiation. In addition to these two species, the absorption and subsequent photodissociation of  $H_2O$ ,  $H_2O_2$ ,  $NO_2$ ,  $NO_3$ ,  $N_2O$ ,  $HNO_2$ ,  $CO_2$ , and  $HO_2$  are discussed in Appendix B. Also presented in Appendix B are the photodissociation of  $N_2O_5$ ,  $HNO_3$ ,  $CH_4$ , and  $CH_2O$ , even though these species are not included in the aeronomic calculations discussed in this report.

The incident solar flux  $I_0(\lambda)$  and the absorption cross sections for  $O_2$ ,  $O_3$ ,  $H_2O$ ,  $H_2O_2$ ,  $NO_2$ ,  $NO_3$ , and  $N_2O$  used in calculating the photodissociation rate coefficients are listed in Table B1. The cross sections for  $O_2$  in the wavelength region of the Schumann Runge bands (175-205 nm) are not tabulated here. In this wavelength region, the molecular oxygen dissociation data of Hudson and Mahle<sup>15</sup> are used. The incident solar fluxes listed here are those tabulated by Ackerman.<sup>16</sup> In the wavelength region 123 to 190 nm, however, the Ackerman fluxes have been replaced by the measurements of Heroux and Swirbalus.<sup>17</sup> The absorption cross sections for  $N_2O_5$ ,  $HNO_2$ ,  $HNO_3$ ,  $CH_4$ ,  $CO_2$ ,  $CH_2O$ , and  $HO_2$  are listed in Table B2.

In computing the time dependence of atmospheric composition, the computation of the photodissociation rate coefficients using Eq. (54) can be a time consuming process. As the solar zenith angle changes, the column densities  $N_i$  will change and, with them, the  $J_j$ 's. It is desirable to have available tables of these coefficients that are not dependent upon specific distributions of molecular oxygen and ozone. To keep the tables perfectly general, therefore, the coefficients are computed and tabulated in Appendix B as functions of the column densities of  $O_2$  and  $O_3$ .

15. Hudson, R.D., and Mahle, S.H. (1972) Photodissociation rates of molecular oxygen in the mesosphere and lower thermosphere, J. Geophys. Res. 77:2902-2914.
16. Ackerman, M. (1971) Ultraviolet solar radiation related to mesospheric processes, in Mesospheric Models and Related Experiments, G. Fiocco, Ed., D. Reidel, Dordrecht, Netherlands.
17. Heroux, L., and Swirbalus, R.A. (1976) Full-disc solar flares between 1230 and 1940 A, J. Geophys. Res. 81:436-440.

the composition of the atmosphere is computed, the dissociation and ionization of atmospheric gases by incident solar radiation must be considered. In most calculations, these photoprocesses are handled as chemical reactions. Consequently, the rate coefficients for dissociation and ionization of the various gases must be known.

The photodissociation and photoionization rate coefficients for a gas particle at any altitude in the atmosphere is a product of the flux of the solar radiation arriving at that altitude and its photodissociation, or photoionization cross section. Several excellent reviews of the absorption properties of atmospheric gases can be found in the literature. Among these are Hudson<sup>12</sup> and Johnston and Graham,<sup>13</sup> Also, an excellent survey article by Turco<sup>14</sup> includes a discussion of photodissociation processes for several gases.

Beer's Law expresses the fractional transmission of radiation through a gas mixture

$$T(\lambda) = \frac{I(\lambda)}{I_0(\lambda)} = e^{-\tau(\lambda)} \quad (51)$$

where  $I_0(\lambda)$  is the intensity of the incident radiation,  $I(\lambda)$  is the intensity of the transmitted radiation, and  $\tau(\lambda)$  is the optical depth of the absorbing layer, all at the wavelength  $\lambda$ . The optical depth is given by

$$\tau(\lambda) = \sum_i \sigma_i(\lambda) N_i \quad (52)$$

where  $\sigma_i(\lambda)$  is the absorption cross section of the  $i$ 'th type of particle and  $N_i$  is the total number of particles of this type in a  $\text{cm}^2$  column along the ray path to the sun.

The rate coefficient for the photoprocess for  $j$ -type particles at wavelength  $\lambda$  is determined by

$$J_j(\lambda) = \sigma'_j(\lambda) I_0(\lambda) T(\lambda) \quad (53)$$

where  $\sigma'_j(\lambda)$  is the cross section for photodissociation or photoionization of the gas.

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12. Hudson, R.D. (1971) Critical review of ultraviolet photoabsorption cross sections for molecules of astrophysical and aeronomic interest, Rev. Geophys. Space Phys. 9:305-406.
  13. Johnston, H.S., and Graham, R. (1974) Photochemistry of  $\text{NO}_x$  and  $\text{HNO}_x$  compounds, Can. J. Chem. 52:1415-1423.
  14. Turco, R.P. (1975) Photodissociation rates in the atmosphere below 100 km, Geophys. Surveys 2:153-192.

Therefore, the average collision frequency for charge exchange is

$$\bar{\nu}_{in} = 1.73725 n \gamma. \quad (48)$$

The average reduced charge exchange collision frequencies between like particles are given in Table 2. Again, it is assumed that the ion and neutral gas temperatures are equal.

Table 2. The Average Reduced Charge Exchange Collision Frequencies Between Like Particles

$H^+ + H$	$1.0 \times 10^{-10}$	$H (2T)^{1/2}$
$O^+ + O$	$1.6 \times 10^{-11}$	$O (2T)^{1/2}$
$N^+ + N$	$1.7 \times 10^{-11}$	$N (2T)^{1/2}$
$He^+ + He$	$3.0 \times 10^{-11}$	$He (2T)^{1/2}$
$O_2^+ + O_2$	$1.1 \times 10^{-11}$	$O_2 (2T)^{1/2}$
$N_2^+ + N_2$	$2.2 \times 10^{-11}$	$N_2 (2T)^{1/2}$

The average ion-ion momentum transfer collision frequency is given by

$$\bar{\nu}_{ij} = 1.3 n_j \left( \frac{1}{\mu^{1/2} T^{3/2}} \right) \text{sec}^{-1} \quad (49)$$

assuming that the charge states of the colliding particles are both unity.

The collision frequency between i and j-type particles is then simply

$$\nu_{ij} = \frac{m_i}{(m_i + m_j)} \bar{\nu}_{ij}. \quad (50)$$

## 6. THE CHEMISTRY AND PHOTOCHEMISTRY

The chemical reactions included in this model are listed in Appendix A. When

Table 1. Polarizabilities of Neutral Gases

GAS	$\alpha (10^{-24} \text{ cm}^3)$
N <sub>2</sub>	1.76
O <sub>2</sub>	1.59
O <sub>2</sub> ( <sup>1</sup> Δg)	1.59
O	0.79
H	0.667
H <sub>2</sub>	0.82
N	1.1
N( <sup>2</sup> D)	1.1
NO	1.74
He	0.21
N <sub>2</sub> O	3.00
CO <sub>2</sub>	2.63
CO	1.97

Let

$$\bar{Q}_E = \sigma = \frac{\gamma}{v} \quad (46)$$

where  $\gamma$  is the chemical reaction rate constant and  $v$  is the velocity of the colliding particle.

Since

$$v = \left( \frac{3kT}{m} \right)^{1/2}, \text{ then}$$

$$\bar{v}_{in} = \frac{4}{3} n \left( \frac{16kT}{\pi m} \right)^{1/2} \frac{\gamma}{\left( \frac{3kT}{m} \right)^{1/2}}. \quad (47)$$

## 5. COLLISION FREQUENCIES

A good review of collision processes can be found in Banks and Kockarts.<sup>9</sup> All of the material that follows was taken from that source.

The average neutral-neutral collision frequencies are given by

$$\bar{\nu}_{ij} = 2n_j \sigma_{ij}^2 \left( \frac{2\pi kT}{\mu} \right)^{1/2} \text{sec}^{-1} \quad (43)$$

where  $\mu$ , the reduced mass, is given by

$$\mu = \frac{m_i m_j}{m_i + m_j}$$

and

$$\sigma_{ij} = \frac{1}{2} (\sigma_i + \sigma_j)$$

where  $\sigma_i$  and  $\sigma_j$  are the diameters of the colliding particles.

The average collision frequency for momentum transfer between ions and neutral particles is

$$\bar{\nu}_{in} = 2.6 \times 10^{-9} n_n \left( \frac{\alpha}{\mu} \right)^{1/2} \text{sec}^{-1} \quad (44)$$

where  $n_n$  is the concentration of the neutral particles,  $\alpha$  is the neutral gas atomic polarizability in units of  $10^{-24} \text{cm}^3$ , and  $\mu$  is in amu. Table 1 lists the polarizability of several atmospheric gases.<sup>9</sup>

The average collision frequency for charge exchange between unlike particles is given by

$$\bar{\nu}_{in} = \frac{4}{3} n \left( \frac{8k}{\pi m} \right)^{1/2} (2T)^{1/2} \bar{Q}_E \quad (45)$$

where  $\bar{Q}_E$  is the average charge transfer cross section for ion-neutral collisions. In Eq. (45), the ion and neutral temperatures are assumed to be equal.



The calculation of  $F_K$ , however, requires the upper boundary velocity at the end of the time step. At the upper boundary,  $O_2^+$ ,  $NO^+$ ,  $O_3$ ,  $OH$ ,  $H$ ,  $HO_2$ ,  $H_2O$ ,  $H_2O_2$ ,  $H_2$ ,  $NO_2$ ,  $O_2$  (' $\Delta g$ '), and argon are all minor species. It is assumed, therefore, that they are in diffusive equilibrium there. This means that their diffusion velocities are zero at the upper boundary, but they are still subject to the mean mass motion.

The remaining species, however, do have diffusion velocities at the upper boundary that must be defined. It is impossible to calculate the upper boundary velocities from Eq. (18) because concentrations are required at  $K + 1$ . Since this altitude is outside the volume, the concentrations are not known there. Therefore, to estimate the velocities at the upper boundary at the end of the time step, we investigate the continuity equation, Eq. (3), at the upper boundary where  $v_i = 0$  (since the upper boundary is outside of the turbulence region).

$$\frac{\partial n_i}{\partial t} = P_i - n_i L_i - \frac{\partial}{\partial Z} (n_i w_i). \quad (41)$$

Setting the time derivative to zero and solving the resulting equation for  $dw_i/dZ$  gives

$$\frac{dw_i}{dZ} = - \frac{w_i}{n_i} \frac{dn_i}{dZ} + \frac{P_i - n_i L_i}{n_i}. \quad (42)$$

This ordinary differential equation can be solved numerically over the last height step to give values of  $w_i$  at the upper boundary. Since Eq. (42) is solved in every iteration, the final iteration will give the upper boundary value of  $w_i$  at the end of the time step.

The new concentration profiles at  $t + \Delta t$  are therefore computed as follows: Starting at the lower boundary, the E and F arrays are computed in the increasing height direction up to the upper boundary. The new concentrations are then computed starting at the upper boundary and applying Eq. (27) in the decreasing altitude direction down to the lower boundary. This procedure is repeated over each time step until the solutions converge for that time step. Once a solution has been accepted, the time step is doubled (provided it has not reached the maximum value set by the program). Using the concentrations and velocities computed at the end of the last time step, the equations are solved over the next time step. In this manner, the solution advances.

Eq. (36) can be written as

$$\tilde{B}_K^{\ell} n_K^{\ell+1} - \tilde{C}_K^{\ell} n_{K-1}^{\ell+1} = \tilde{D}_K^{\ell} \quad (37)$$

where

$$\tilde{A}_K^{\ell} = 0$$

$$\tilde{B}_K^{\ell} = -A_K^{\ell} \left[ 1 - \Gamma_K \Delta Z_K - \frac{m_i \Delta Z_K}{k T_K} \sum_j \nu_{ij} (w_i - w_j)_K^{\ell+1} \right] + B_K^{\ell}$$

$$\tilde{C}_K^{\ell} = C_K^{\ell}$$

$$\tilde{D}_K^{\ell} = D_K^{\ell} \quad (38)$$

Eq. (28) can be rewritten at level K as

$$E_K = \frac{\tilde{A}_K^{\ell}}{[\tilde{B}_K^{\ell} - \tilde{C}_K^{\ell} E_{K-1}]}$$

and

$$F_K = \frac{\tilde{D}_K^{\ell} + \tilde{C}_K^{\ell} F_{K-1}}{\tilde{B}_K^{\ell} - \tilde{C}_K^{\ell} E_{K-1}} \quad (39)$$

It is obvious, then, that

$$E_K = 0$$

and

$$F_K = \frac{D_K^{\ell} + C_K^{\ell} F_{K-1}}{B_K^{\ell} - A_K^{\ell} \left[ 1 - \Gamma_K \Delta Z_K - \frac{m_i \Delta Z_K}{k T_K} \sum_j \nu_{ij} (w_i - w_j)_K^{\ell+1} \right] - C_K^{\ell} E_{K-1}} \quad (40)$$

$$n_o^{\ell+1} = \frac{n_o^{\ell} + P_o^{\ell+1} \Delta t}{[1 + L_o^{\ell+1} \Delta t]} \quad (30)$$

$E_o$  and  $F_o$  at the lower boundary are simply

$$E_o = 0$$

and

$$F_o = n_o^{\ell+1} \quad (31)$$

At the upper boundary, the time derivative of the velocities in Eq. (7) is set to zero:

$$\frac{kT}{m_i} \left[ \frac{1}{n_i} \frac{dn_i}{dZ} + \frac{(1+\alpha_i)}{T} \frac{dT}{dZ} + \frac{1}{H_i} \right] = - \sum_j \nu_{ij} (w_i - w_j) \quad (32)$$

Solving Eq. (32) for  $dn_i/dZ$  gives

$$\frac{dn_i}{dZ} = -n_i \Gamma_i - \frac{n_i m_i}{kT} \sum_j \nu_{ij} (w_i - w_j) \quad (33)$$

Writing Eq. (33) at the upper boundary (K) in finite difference notation gives

$$\frac{n_{K+1}^{\ell+1} - n_K^{\ell+1}}{\Delta Z_K} = n_K^{\ell+1} \Gamma_K - \frac{n_K^{\ell+1} m_i}{kT_K} \sum_j \nu_{ij} (w_i - w_j)_K^{\ell+1} \quad (34)$$

Solving Eq. (34) for  $n_{K+1}^{\ell+1}$  gives

$$n_{K+1}^{\ell+1} = n_K^{\ell+1} \left[ 1 - \Gamma_K \Delta Z_K - \frac{m_i \Delta Z_K}{kT_K} \sum_j \nu_{ij} (w_i - w_j)_K^{\ell+1} \right] \quad (35)$$

Replacing  $n_{K+1}^{\ell+1}$  in Eq. (25) written at level K with Eq. (35) gives

$$\left\{ -A_K^{\ell} \left[ 1 - \Gamma_K \Delta Z_K - \frac{m_i \Delta Z_K}{kT_K} \sum_j \nu_{ij} (w_i - w_j)_K^{\ell+1} \right] + B_K^{\ell} \right\} \\ n_K^{\ell+1} - C_K^{\ell} n_{K-1}^{\ell+1} = D_K^{\ell} \quad (36)$$

From Eqs. (26) and (27), the following definitions are obtained:

$$E_k = \frac{A_k^\ell}{[B_k^\ell - C_k^\ell E_{k-1}]}$$

and

$$F_k = \frac{D_k^\ell + C_k^\ell F_{k-1}}{[B_k^\ell - C_k^\ell E_{k-1}]} \quad (28)$$

Using Eqs. (27) and (28), the height profiles for the concentrations can be calculated provided  $n_0^{\ell+1}$  and  $n_k^{\ell+1}$  can be specified at the lower and upper boundaries respectively. The boundary conditions will be discussed in Section 4.

It should be noted that only some of the terms on the right-hand side of the equations for  $A_k^\ell$ ,  $B_k^\ell$ ,  $C_k^\ell$ , and  $D_k^\ell$  are specified at the beginning of the time step. The chemistry terms and the velocity sums are specified at the end of the time step. Because of this, the solutions require iteration over the time step. At the end of each iteration of the concentrations, the chemistry and the velocities from Eq. (18) are recomputed. New concentrations are then calculated using these updated values. This procedure is repeated until, on successive iterations, the concentrations of all species change by less than 1 percent at all altitudes.

#### 4. BOUNDARY CONDITIONS

At the lower boundary, the concentrations of  $N_2$ ,  $O_2$ ,  $H_2O$ ,  $H_2$ , and Ar are held fixed for all time at their initial values ( $n_0^{\ell+1} = \text{constant}$ ). All of the other species in the transport mode prove to be chemically controlled at 50 km, so their concentrations are computed from the simplified continuity equations. With the divergence of the flux set to zero in Eq. (1), that equation becomes

$$\frac{dn_i}{dt} = P_i - n_i L_i \quad (29)$$

If the derivative in Eq. (29) is replaced by simple differences, then, at the lower boundary, we have

in which

$$Q_k = \frac{1}{[1 + \Delta t \lambda \sum_j \nu_{ij}]}$$

$$S_k = (1 - \Gamma_k \Delta Z_k)$$

$$\bar{S}_k = (1 - \bar{\Gamma}_k \Delta Z_k).$$

It is possible, therefore, to write a tridiagonal matrix between the lower and upper boundaries for each species using Eq. (21). These tridiagonal matrices are then solved for the vertical distribution of the concentration using the method of Richtmyer and Morton.<sup>11</sup>

Substituting the recurrence relation

$$n_{k-1}^{\ell+1} = E_{k-1} n_k^{\ell+1} + F_{k-1} \quad (23)$$

into Eq. (21) gives

$$-A_k^{\ell} n_{k+1}^{\ell+1} + B_k^{\ell} n_k^{\ell+1} - C_k^{\ell} E_{k-1} n_k^{\ell+1} - C_k^{\ell} F_{k-1} = D_k^{\ell}. \quad (24)$$

This can be written as

$$-A_k^{\ell} n_{k+1}^{\ell+1} + [B_k^{\ell} - C_k^{\ell} E_{k-1}] n_k^{\ell+1} = D_k^{\ell} + C_k^{\ell} F_{k-1}. \quad (25)$$

Solving Eq. (25) for  $n_k^{\ell+1}$  gives

$$n_k^{\ell+1} = \frac{A_k^{\ell}}{[B_k^{\ell} - C_k^{\ell} E_{k-1}]} n_{k+1}^{\ell+1} + \frac{D_k^{\ell} + C_k^{\ell} F_{k-1}}{[B_k^{\ell} - C_k^{\ell} E_{k-1}]}. \quad (26)$$

Eq. (23) written at level  $k$  is

$$n_k^{\ell+1} = E_k n_{k+1}^{\ell+1} + F_k. \quad (27)$$

11. Richtmyer, R.D., and Morton, K.W. (1967) Difference Methods for Initial-Value Problems, Interscience Publishers, New York.

$$\begin{aligned}
\phi_{k-1}^{\ell+1} = & \frac{1}{[1 + \Delta t \lambda_i \sum_j \nu_{ij}]} \left\{ n_{k-1}^{\ell+1} w_{k-1}^{\ell+1} - \frac{kT_{k-1}}{m_i} \frac{\Delta t}{\Delta Z_{k-1}} \right. \\
& \left[ n_k^{\ell+1} - n_{k-1}^{\ell+1} (1 - \bar{r}_{k-1} \Delta Z_{k-1}) \right] \\
& + n_{k-1}^{\ell+1} \Delta t \sum_{j \neq i} \nu_{ij} w_{j_{k-1}}^{\ell+1} \left. \right\} \\
& - \frac{K_{k-1}}{\Delta Z_{k-1}} \left\{ n_k^{\ell+1} - n_{k-1}^{\ell+1} (1 - \bar{r}_{k-1} \Delta Z_{k-1}) \right\}. \quad (20)
\end{aligned}$$

Substituting Eqs. (19) and (20) into Eq. (12) and collecting like terms in  $n$  gives

$$-A_k^\ell n_{k+1}^{\ell+1} + B_k^\ell n_k^{\ell+1} - C_k^\ell n_{k-1}^{\ell+1} = D_k^\ell \quad (21)$$

where

$$\begin{aligned}
A_k^\ell &= \frac{\Delta t}{\Delta Z_k \Delta Z_{k-1}} \left[ Q_k \frac{kT_k \Delta t}{m} + K_k \right] \\
B_k^\ell &= 1 + L_k^{\ell+1} \Delta t + \frac{\Delta t}{\Delta Z_k \Delta Z_{k-1}} \\
&\quad \left[ Q_k \left( w_k^\ell \Delta Z_k + S_k \frac{kT_k \Delta t}{m} + \Delta t \Delta Z_k \sum_{j \neq i} \nu_{ij} w_{j_k}^{\ell+1} \right) \right. \\
&\quad \left. + \bar{S}_k K_k + Q_{k-1} \frac{kT_{k-1} \Delta t}{m} \frac{\Delta Z_k}{\Delta Z_{k-1}} + K_{k-1} \frac{\Delta Z_k}{\Delta Z_{k-1}} \right] \\
C_k^\ell &= \frac{\Delta t}{\Delta Z_k \Delta Z_{k-1}} \left[ Q_{k-1} \left( w_{k-1}^\ell \Delta Z_k + S_{k-1} \frac{kT_{k-1} \Delta t}{m} \frac{\Delta Z_k}{\Delta Z_{k-1}} \right. \right. \\
&\quad \left. \left. + \Delta t \Delta Z_k \sum_{j \neq i} \nu_{ij} w_{j_{k-1}}^{\ell+1} \right) + \bar{S}_k K_{k-1} \frac{\Delta Z_k}{\Delta Z_{k-1}} \right] \\
D_k^\ell &= n_k^\ell + P_k^{\ell+1} \Delta t \quad (22)
\end{aligned}$$

both computed at level k. Also

$$\lambda_i = \frac{\Omega_i^2 + \left( \sum_j \nu_{ij} \right)^2}{\Omega_i^2 \sin^2 I + \left( \sum_j \nu_{ij} \right)^2} \quad (17)$$

The finite difference equations, Eqs. (13) and (14), can be solved for the velocities  $w_k^{\ell+1}$  at the end of the time step:

$$w_k^{\ell+1} = \frac{1}{\left[ 1 + \Delta t \lambda_i \sum_j \nu_{ij} \right]} \left\{ w_k^{\ell} - \frac{kT_k}{m_i} \frac{\Delta t}{\Delta Z_k} \left[ \frac{n_{k+1}^{\ell+1} - n_k^{\ell+1}}{n_k^{\ell+1}} + \Gamma_k \Delta Z_k \right] + \Delta t \sum_j \nu_{ij} w_{jk}^{\ell+1} \right\} \quad (18)$$

This equation holds for both the ionic and neutral species using the above definitions of  $\Gamma_k$  and with  $\lambda_i = 1$  for the neutral species. The total molecular and eddy diffusion flux at level k can then be written as

$$n_k^{\ell+1} w_k^{\ell+1} = \phi_k^{\ell+1} = \frac{1}{\left[ 1 + \Delta t \lambda_i \sum_j \nu_{ij} \right]} \left\{ n_k^{\ell+1} w_k^{\ell} - \frac{kT_k}{m_i} \frac{\Delta t}{\Delta Z_k} \left[ n_{k+1}^{\ell+1} - n_k^{\ell+1} (1 - \Gamma_k \Delta Z_k) \right] + n_k^{\ell+1} \Delta t \sum_{j \neq i} \nu_{ij} w_{jk}^{\ell+1} \right\} - \frac{K_k}{\Delta Z_k} \left\{ n_{k+1}^{\ell+1} - n_k^{\ell+1} (1 - \bar{\Gamma}_k \Delta Z_k) \right\} \quad (19)$$

where

$$\bar{\Gamma}_k = \frac{1}{T_k} \frac{\partial T}{\partial Z} + \frac{1}{\bar{H}} \quad \text{and} \quad \bar{H} = \frac{kT}{mg}.$$

A similar expression can be derived for  $\phi_{k-1}^{\ell+1}$  at level k-1.

### 3. THE FINITE DIFFERENCE EQUATIONS

If  $l$  denotes the grids on the time mesh and  $k$  the grids on the height mesh, then the continuity equations, Eq. (1), can be written in finite difference notation at the height level  $k$  as

$$\frac{n_k^{l+1} - n_k^l}{\Delta t} = P_k^{l+1} - n_k^{l+1} L_k^{l+1} - \frac{\phi_k^{l+1} - \phi_{k-1}^{l+1}}{\Delta Z_{k-1}} \quad (12)$$

where, for the sake of clarity, the subscript  $i$  has been dropped. Using the equations of motion, Eqs. (7) and (9), the  $\phi_k^{l+1}$  and  $\phi_{k-1}^{l+1}$  will be replaced in Eq. (12) with their equivalent expressions.

The equations of motion, Eq. (7), for the neutral species can be written in finite difference form at height level  $k$  as

$$\begin{aligned} \frac{w_k^{l+1} - w_k^l}{\Delta t} = & - \frac{k T_k}{m_i} \left[ \frac{n_{k+1}^{l+1} - n_k^{l+1}}{n_k^{l+1} \Delta Z_k} + \Gamma_k \right] - w_k^{l+1} \sum_j \nu_{ij} \\ & + \sum_{j \neq i} \nu_{ij} w_{jk}^{l+1} \end{aligned} \quad (13)$$

and Eq. (9) for the ionic species as

$$\begin{aligned} \frac{w_k^{l+1} - w_k^l}{\Delta t} = & - \frac{k T_k}{m_i} \left[ \frac{n_{k+1}^{l+1} - n_k^{l+1}}{n_k^{l+1} \Delta Z_k} + \Gamma_k \right] - w_k^{l+1} \lambda_i \sum_j \nu_{ij} \\ & + \sum_{j \neq i} \nu_{ij} w_{jk}^{l+1}. \end{aligned} \quad (14)$$

For the neutral species,

$$\Gamma_k = \frac{(1 + \alpha_i)}{T} \frac{\partial T}{\partial Z} + \frac{1}{H_i} \quad (15)$$

and for the ionic species

$$\Gamma_k = \frac{1}{n_e} \frac{\partial n_e}{\partial Z} + \frac{2}{T} \frac{\partial T}{\partial Z} + \frac{1}{H_i} \quad (16)$$



In computing the transmittance of EUV radiation, O, O<sub>2</sub>, and N<sub>2</sub> are considered as the primary absorbers. The photoionization rate coefficients are computed by using Eq. (54), where the sum is taken from 0.1 to 102.57 nm. Radiation below 15 nm is considered to be X-rays, and its ionization is partitioned among O, O<sub>2</sub>, N<sub>2</sub>, and N in accordance with Swider.<sup>19</sup>

The calculations also take into account the scattering of some radiation from the sunlit hemisphere into the nighttime hemisphere. These scattered radiations include Lyman  $\alpha$  at 121.57 nm, Lyman  $\beta$  at 102.57 nm, the HE I line at 58.4 nm, and the HE II line at 30.4 nm. For simplicity, the amount of radiation that scatters into the dark hemisphere is taken to be a fraction of the direct noontime radiation at the particular altitude under consideration. These fractions are: Lyman  $\alpha$ , 0.01; Lyman  $\beta$ , 0.004; HE I, 0.0011; and HE II, 0.001.

Finally, the contribution of cosmic rays to the photoionization rate coefficients is also included. This is simply<sup>24</sup>

$$q_i = 1 \times 10^{-17} n_i. \quad (55)$$

### 6.3 Electron Impact Ionization

Reactions 208 through 215 in the list of reactions in Appendix A are the energetic electron processes. The flux of energetic electrons appropriate to the calculations made here were supplied by Jasperse.<sup>25</sup> The ionization rate coefficients for the energetic electron reactions are computed from<sup>9</sup>

$$I = \int_{\xi} \sigma(\xi) \Phi(\xi) d\xi \quad (56)$$

where  $\sigma(\xi)$  is the electron impact ionization cross section and  $\Phi(\xi)$  is the energetic electron flux, both at energy  $\xi$ . The ionization cross section is given by<sup>9</sup>

$$\sigma(\xi) = \int_I^{\frac{\xi+I}{2}} S(\xi, W) dW \quad (57)$$

24. Nicolet, M., and Aikin, A.C. (1960) The formation of the D region of the ionosphere, J. Geophys. Res. 65:1469-1483.

25. Jasperse, J.R. (1978) Private communication.

in which

$$S(\xi, W) = \left( \frac{q_0 c_0 f_0}{W^2} \right) \left( \frac{I}{W} \right)^P \left[ 1 - \left( \frac{W}{E} \right)^\gamma \right]^\nu \left( \frac{W}{\xi} \right)^\Omega$$

where  $I$  is the ionization threshold for a particular ion state,  $q_0 = 6.51 \times 10^{-14} \text{ ev}^2 \text{ cm}^2$ ,  $c_0 f_0$  is a constant,  $W$  is the excitation threshold energy in ev, and  $P$ ,  $\gamma$ ,  $\nu$ , and  $\Omega$  are parameters obtained from the best fit of Eq. (58) to experimental and theoretical results. Table B22 lists the values of these parameters used in the model presented here. The values of the rate coefficients computed for the energetic electron reactions are given in Table B23.

#### 6.4 The Thermal Diffusion Factors

The thermal diffusion factors are assumed to be zero except for the following species: O(-0.27), O<sub>2</sub>(+0.08), H(-0.39), H<sub>2</sub>(-0.31), and He(-0.36). A discussion of the thermal diffusion factors can be found in Zimmerman and Keneshea,<sup>26</sup> from which source these values were taken.

### 7. A MID-LATITUDE ATMOSPHERE SIMULATION

The computer code presented here describes the distribution of 56 individual atmospheric species. Not all of them have the full coupled sets of equations in the system, however. Some gases in the atmosphere have such short chemical time constants that they will react chemically long before they can be moved out of a unit volume by any transport process. The vertical distribution of these species can be determined quite accurately by considering only the chemical reactions in which they are involved and ignoring any transport effects on them.

The species for which the coupled sets of mass and momentum equations are solved are:

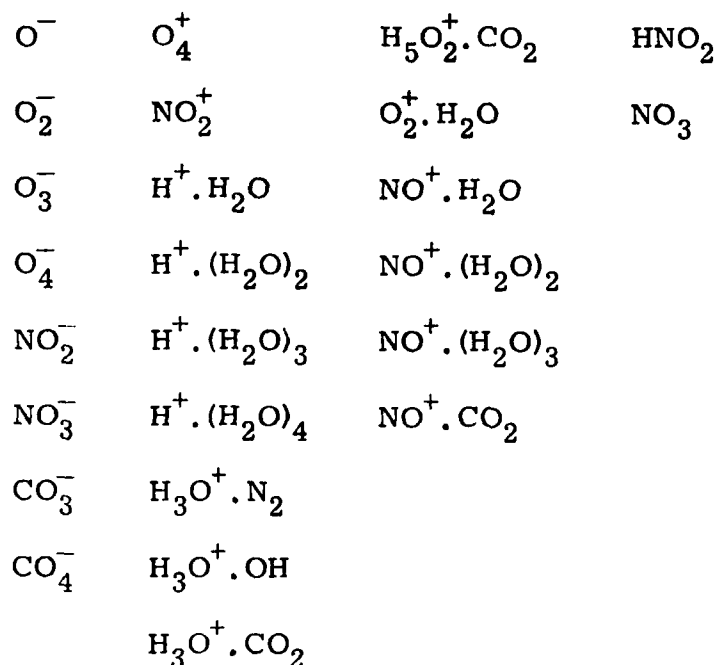
O	H	N	CO	AR	H <sup>+</sup>
O <sub>2</sub>	H <sub>2</sub>	N( <sup>2</sup> D)	CO <sub>2</sub>		HE <sup>+</sup>
O <sub>2</sub> ( <sup>1</sup> Δg)	HO <sub>2</sub>	N <sub>2</sub>			O <sup>+</sup>
O <sub>3</sub>	H <sub>2</sub> O	NO			O <sub>2</sub> <sup>+</sup>
OH	H <sub>2</sub> O <sub>2</sub>	NO <sub>2</sub>			NO <sup>+</sup>
		N <sub>2</sub> O			N <sup>+</sup>

Those species whose distributions are determined neglecting transport are

26. Zimmerman, S.P., and Keneshea, T.J. (1976) The thermosphere in motion, *J. Geophys. Res.* 81:3187-3197.

$O(^1D)$ ,  $N_2^+$ ,  $O^+(^2D)$ , and the electrons. The height distributions of all 56 species are computed over the entire altitude range, which is from 50 to 400 km.

In addition, the vertical distributions of the following species are computed over a reduced altitude range. The temporal variation of these species is also computed with the transport term removed from their continuity equations. The distributions of these species are computed between 50 and 120 km because, above this altitude, they do not exist in significant quantities. These species are:



Neither negative cluster ions nor metallic ions are considered here. To ensure that the atmosphere remains electrically neutral, one of the negatively charged species is always computed from the imposed condition of balance of charge. Below 120 km, where there are several types of negative ions in addition to the electrons, the most abundant negatively charged species is always computed from conservation of charge. That is, its concentration is computed as the difference between the sum of all the positive and the sum of all the other negative ions. Above 120 km, where the only negatively charged particles are the electrons, their concentration is always set equal to the sum of all the positive ions.

### 7.1 Initial Conditions

Throughout the development of the time-dependent solution of Eq. (1), the temperatures and the turbulent diffusion coefficients are held fixed at all altitudes in the code presented here. For the simulation developed in this report, both of these parameters were derived from data obtained during the ALADDIN I experiments of

20 November 1970.<sup>27,28</sup> The temperatures shown in Figure 1 between 50 and 125 km were taken from measurements of Theon and Horvath.<sup>29</sup> From 125 to 160 km, the measurements of Golomb<sup>27</sup> were used. Above 160 km, the temperatures were taken from the 900 K exospheric temperature winter model of the U.S. Standard Atmosphere Supplements, 1966. A discussion of the turbulent diffusion coefficients obtained from the ALADDIN I experiments can be found in Keneshea et al.<sup>8</sup> The coefficients presented there represent the minimum turbulent diffusion coefficients determined from the observations on the chemical trails. Following arguments given there, the turbulent diffusion coefficients (Figure 2) used in these calculations are three times larger than those presented in that paper.

Keneshea et al.<sup>8</sup> found that stability considerations required that the height steps in the mesosphere not exceed 150 m. In the thermosphere, however, stability could be maintained with somewhat larger height steps. Therefore, to reduce the amount of core storage required for saving the numerous arrays as well as to reduce the amount of computer time per solution, a variable height step array was used. From the lower boundary, 50 km, up to 90 km, the height steps were fixed at 150 m. From 90 km up to the upper boundary, 400 km, the height steps were computed by assuming that they were proportional to the pressure scale height of the atmosphere. This produced an altitude array with 692 grid points, with the maximum height step at the upper boundary of about 1.5 km.

The initial concentration and average velocity profiles were taken from the final solution of an unpublished simulation using turbulent diffusion coefficients one third smaller than those shown in Figure 2. A discussion of a method for establishing initial concentrations on all the species is given in Keneshea et al.<sup>8</sup> for a situation where no previous information is available on the vertical distribution of the various species.

The solutions to Eqs. (1) and (18) are started at noon of solution day 1 with the above initial values. Because this is a real time-dependent calculation which takes into account the daily variation of the solar zenith angle, no truly steady state condition on the species concentrations is ever achieved. The calculations are continued, therefore, until all species reproduce their concentrations diurnally at all

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27. Rosenberg, N.W., Golomb, D., Zimmerman, S.P., Vickery, W.K., and Theon, J.S. (1973) The ALADDIN Experiment-Part I, Dynamics, Space Research XIII, Akademie-Verlag, Berlin, 435-439.

28. Philbrick, C.R., Narcisi, R.S., Good, R.E., Hoffman, H.S., Keneshea, T.J., Macleod, M.A., Zimmerman, S.P., and Reinish, B.W. (1973) The ALADDIN Experiment-Part II, Composition, Space Research XIII, Akademie-Verlag, Berlin, 441-448.

29. Theon, J.S., and Horvath, J.J. (1972) ALADDIN neutral atmosphere measurements, Trans. Am. Geophys. Un. 53:463.

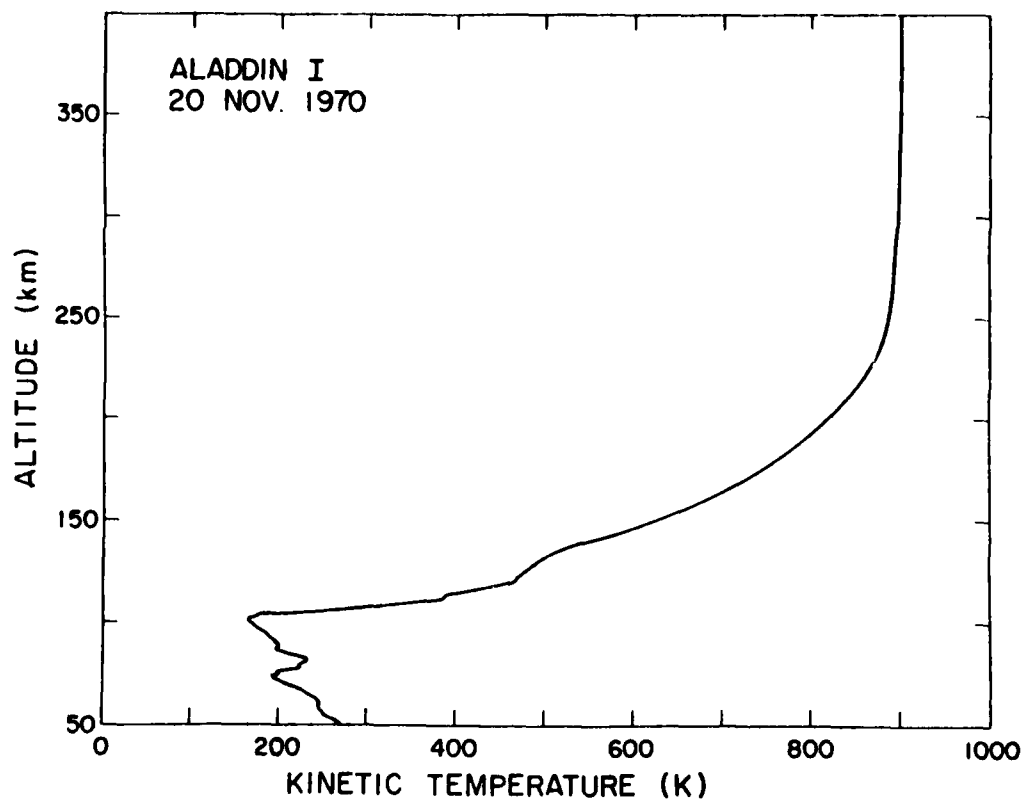


Figure 1. The Static Temperature Profile

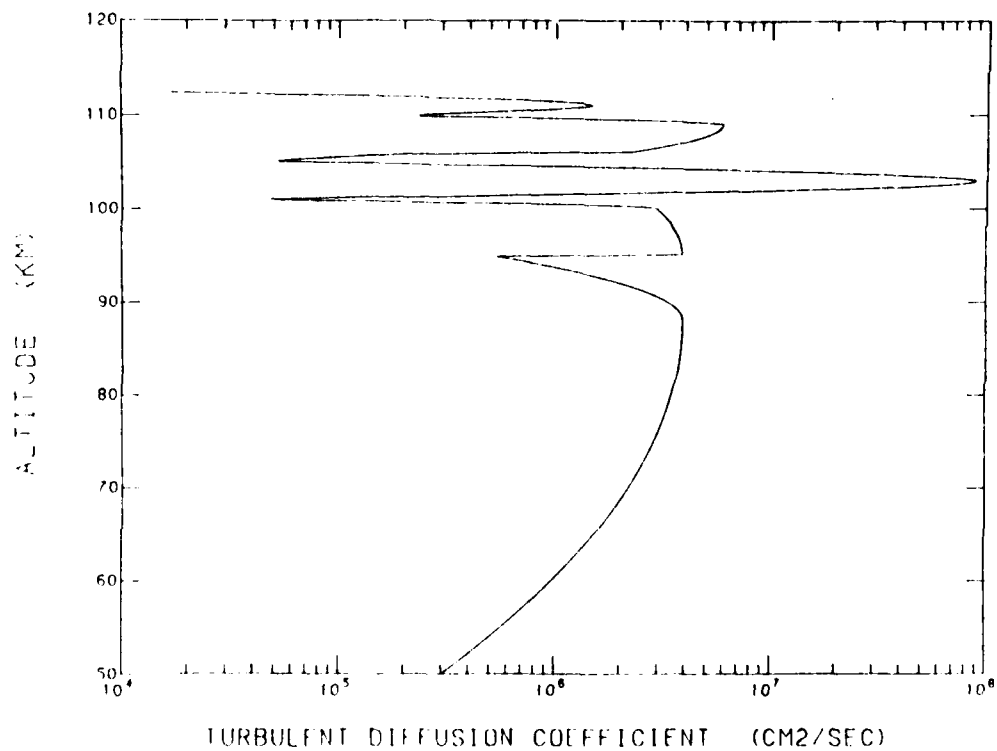


Figure 2. The Turbulent Diffusion Coefficients as Determined From the Chemical Release Data Obtained From the ALADDIN I Experiments

altitudes to within 1 percent. This condition of diurnal reproducibility is generally arrived at after about 20 solution days.

## 7.2 Thermospheric Results

The results to be discussed here were taken from the final diurnal cycle of the calculations when the major and most of the minor species at all altitudes were varying by no more than 1 percent from values achieved 24 hours earlier. The vertical distribution of the major species  $N_2$ ,  $O_2$ ,  $O$ , and argon are shown in Figure 3. In this one-dimensional temperature-independent calculation,  $N_2$ ,  $O_2$ , and argon show no diurnal change, having arrived at an equilibrium with the invariant temperature given in Figure 1. Also displayed in Figure 3 is the fixed profile of helium used in these calculations.

Because of the constant temperature profile used here, atomic oxygen also shows no diurnal variation in the thermosphere down to about 120 km. Below this altitude, the chemistry dominates the production (dissociation of  $O_2$ ) and loss of this species.<sup>7</sup> Thus, we observe in Figures 3 and 4 large diurnal variations of atomic oxygen in the mesosphere.

Presented in Figure 5 are the mesosphere and lower thermosphere noontime profiles of the remaining important neutral species. Carbon dioxide is invariant in the mesosphere and lower thermosphere up to about 140 km. Above this altitude, the diurnal variation of the photodissociation process becomes important in the determination of the carbon dioxide concentrations. The variation of the  $CO_2/Ar$  ratio calculated here is shown in Figure 6 and compares well to that determined from atmospheric measurements of Trinks and Fricke.<sup>30</sup>

Isodensity contour plots of the minor neutral species that exhibit a large diurnal variation are shown in Figures 7 to 11. The numbers in all the isodensity plots presented here are the common logarithms of the concentrations. These species, for the most part, are important in the determination of the electron density throughout the atmosphere. Above about 100 km, the charge distribution is dominated by  $NO^+$ ,  $O_2^+$ ,  $O^+$ ,  $He^+$ , and  $H^+$ . Thus, the resultant thermospheric charge balance follows the chain created primarily by the time-dependent distributions of the neutral species  $N$ ,  $NO$ , and  $N(^2D)$  as shown in Figures 7, 8, and 9, respectively. The other neutral thermospheric species in the code have little effect in determining the charge distribution.

The ion and electron isodensity contours determined from these neutrals are shown in Figures 12 to 19. As expected, the dominant positive ion in the upper

30. Trinks, H., and Fricke, K.H. (1978) Carbon dioxide concentrations in the lower thermosphere, J. Geophys. Res., 83:3883-3886.

thermosphere is the  $O^+$  ion. The electron density distribution, therefore, follows the distribution of this ion very closely. Also displayed in Figure 19 is the altitude profile of  $f_oF_2$ , the space-time dependence of the peak of the electron density along with the measurements of this parameter by Evans.<sup>31</sup> The correspondence is quite good, clearly demonstrating the midday altitude and amplitude and the night-time transition to higher altitudes and lower amplitudes. No horizontal winds are included in this one-dimensional simulation; yet, we obtain an excellent representation of the  $F_2$  layer maximum.

Our rationale, then, is that the contribution of chemical production and loss coupled to the convergences and divergences created in our calculations are the main mechanisms that control the amplitude and altitude variation of the  $F_2$  layer maximum. The question that arises from this one-dimensional calculation, which apparently gives good agreement with some  $F_2$  layer maximum measurements, is: What is the effect of horizontal winds? The answer to this question may be inferred from measurements of Reinisch,<sup>32</sup> who determined the time dependence of  $f_oF_{max}$  for another period from ionosonde measurements. His results for  $f_oF_{max}$  are shown in Figure 20. We observe a smaller peak ionization amplitude than Reinisch does, but, generally, the time dependence of his  $F_2$  layer maximum follows our calculations quite well. Also observed are the large variations that presumably arise from local winds that show multireversals during the measuring period. The point we wish to stress is that ionization calculated from internally determined neutral species distributions does result in an internally consistent  $F_2$  layer ionization behavior that compares well with some of the observed ionic behavior. An example of this is the recent work of Sethia et al.,<sup>33</sup> who have performed calculations similar to ours but include the effects of horizontal winds. They determine the distributions along magnetic field lines, while we calculate in the vertical direction with the magnetic field entering by way of the Larmor frequency and the magnetic dip angle. They input the neutral atmosphere, while we calculate it as an internally consistent integral part of the model.

In Figure 21, we have superimposed upon our calculation of the total electron content that taken from Figure 3, model 4 (no winds) of Sethia et al.<sup>33</sup> We observe that the shapes of the distributions are almost identical between the two one-dimensional models. The differences in magnitude can be attributed to the

31. Evans, J.V. (1971) Observations of F-region vertical velocities at Millstone Hill-I. Evidence for drifts due to expansion, contraction, and winds, Radio Sci. 6:609-626.

32. Reinisch, B. (1983) Private communication.

33. Sethia, G.C., Bailey, G.J., Moffett, R.J., and Hargreaves, J.K. (1983) The effects of neutral air winds on the electron content of the mid-latitude ionosphere and protonosphere in summer, Planet. Space Sci. 31:377-387.

different conditions under which the models were computed. We also compare (Figure 22) the total electron content to some measurements taken at Boulder by Sethia et al<sup>33</sup> as shown in their Figure 8 (July 2, no wind, and July 5, with wind). Again, the shape of our distribution compares well with the measured profiles. For those cases where the wind amplitude is not very large, the contribution of the  $\vec{v} \times \vec{B}$  mechanism is very much smaller than that of the chemistry. We make another comparison with the work of Poulter et al<sup>34</sup> shown in Figure 23. Here we examine the total electron content for measurements at Boulder and Lancaster (Figure 5 of Poulter et al), and again quite good agreement is seen between the shape of the distributions from the chemical-transport one-dimensional model and the measurements. The observed differences between the Boulder and the Lancaster curves result from the differences in the raypath geometries. Comparison is also quite good between our calculations and the  $f_oF_2$  measured by Kohl et al<sup>35</sup> and discussed by Rishbeth.<sup>36</sup>

We reiterate the point we wish to stress (see also Rush et al<sup>37</sup>): A comprehensive, one-dimensional, time-dependent ion-neutral model demonstrates excellent agreement with measurements of electron densities. The inclusion of the effects of winds is necessary, however, to explain the deviation of the ions and/or electrons from their equilibrium distributions, which significantly vary over the diurnal cycle.

### 7.3 Mesospheric Results

The ionization in the mesosphere is much more complex than the ionization in the thermosphere. Ablating meteorites create long-lived atomic ions from the metallic species present in the atmosphere. These metallic ions are significant and are observed to be the dominant ions in sporadic E layers. Their chemistry, however, is not well known. For this reason and because large amounts of additional computer memory and time would be required for their inclusion in the transport mode, they have been omitted from the calculations presented here. This omission might explain why our electron density is somewhat low in the 90 to 110 km

34. Poulter, E.M., Hargreaves, J.K., Bailey, G.J., and Moffet, R.J. (1981) Electron content modelling: The significance of protonospheric contents, Planet. Space Sci. 29:869-883.
35. Kohl, H., King, J.W., and Eccles, D. (1969) An explanation of the magnetic declination effect in the ionospheric F-layer, J. Atmos. Terr. Phys. 31:1011-1016.
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37. Rush, C.M., Kempner, M.P., Anderson, D.N., Stewart, F.G., and Perry, J. (1983) Improving ionospheric maps using theoretically derived values, Radio Sci. 18:95-107.



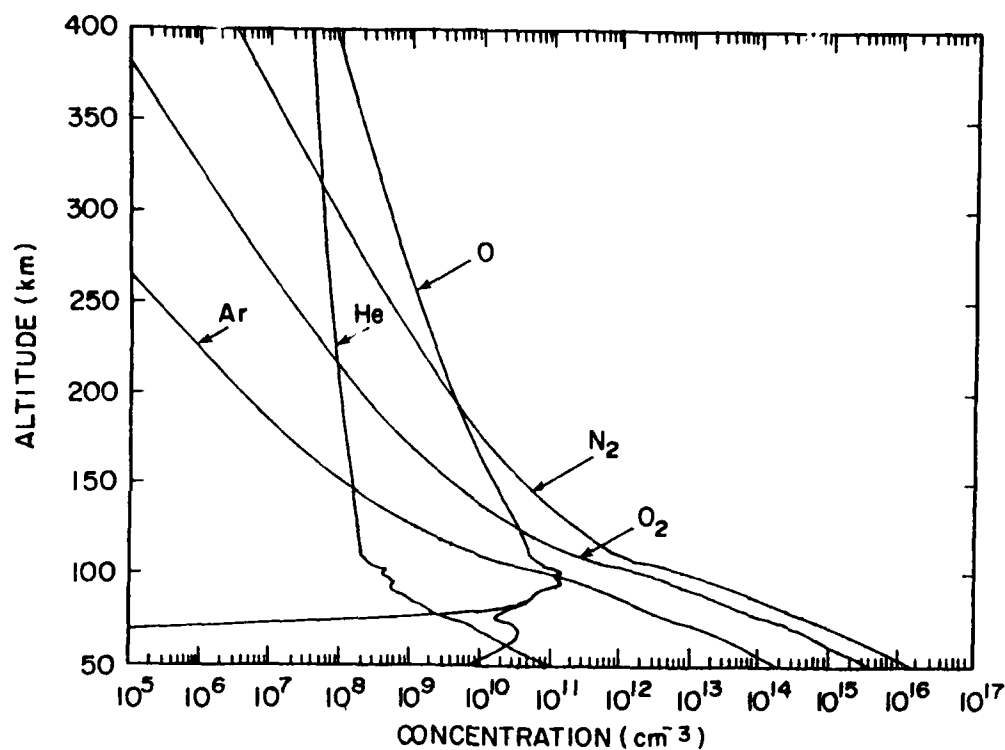


Figure 3. The Time Invariant Height Profiles of  $N_2$ ,  $O_2$ , Helium, and Argon. Above about 100 km, atomic oxygen is also invariant. Below 100 km, the noon and midnight profiles of atomic oxygen are shown

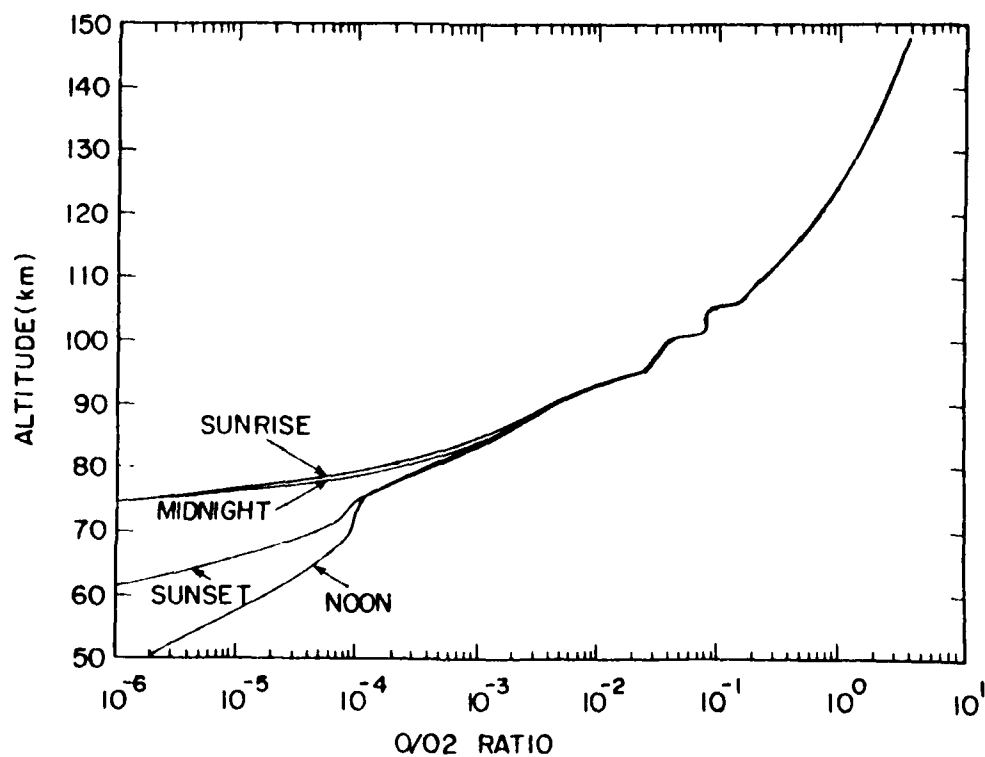


Figure 4. The Ratio of Atomic to Molecular Oxygen at Four Different Times During the Day. These curves reflect the diurnal variations of atomic oxygen in the mesosphere

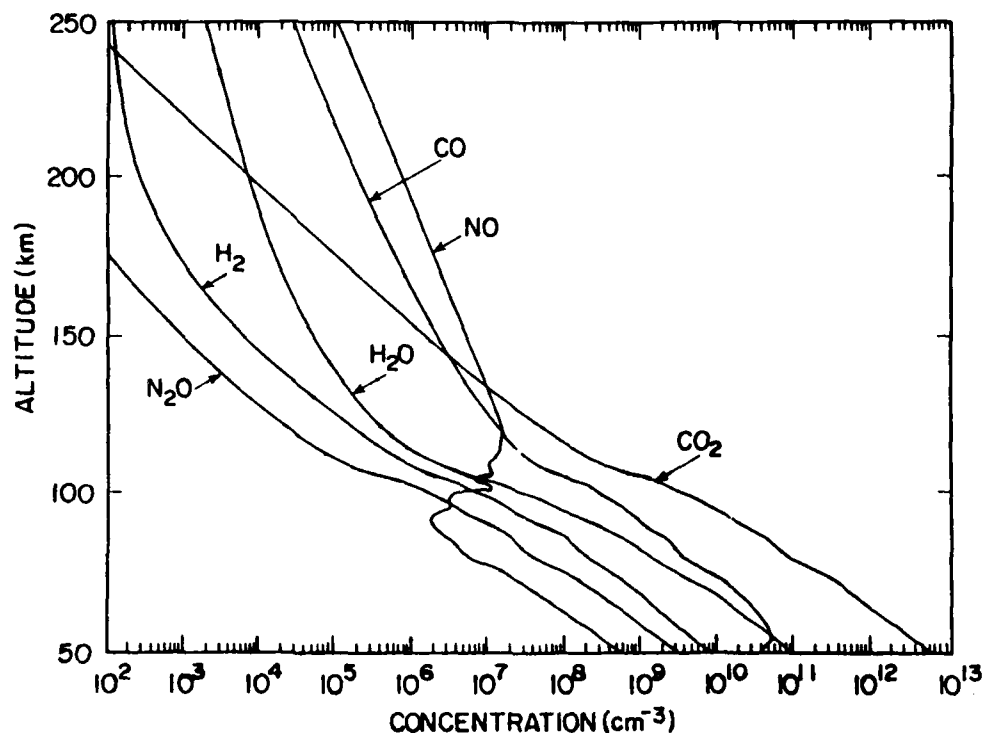


Figure 5. The Noontime Profiles of H<sub>2</sub>, H<sub>2</sub>O, NO, N<sub>2</sub>O, CO, and CO<sub>2</sub> in the Mesosphere and Lower Thermosphere

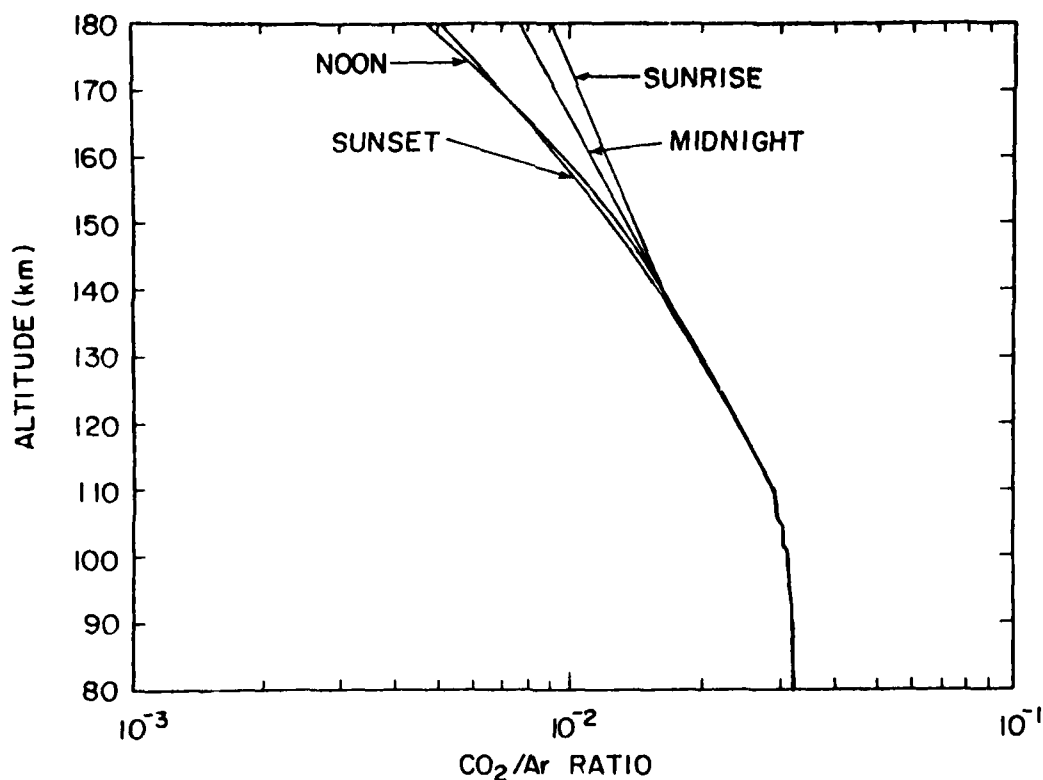


Figure 6. The Ratio of Carbon Dioxide to Argon at Four Different Times During the Day. The curves show the diurnal variation of carbon dioxide in the lower thermosphere

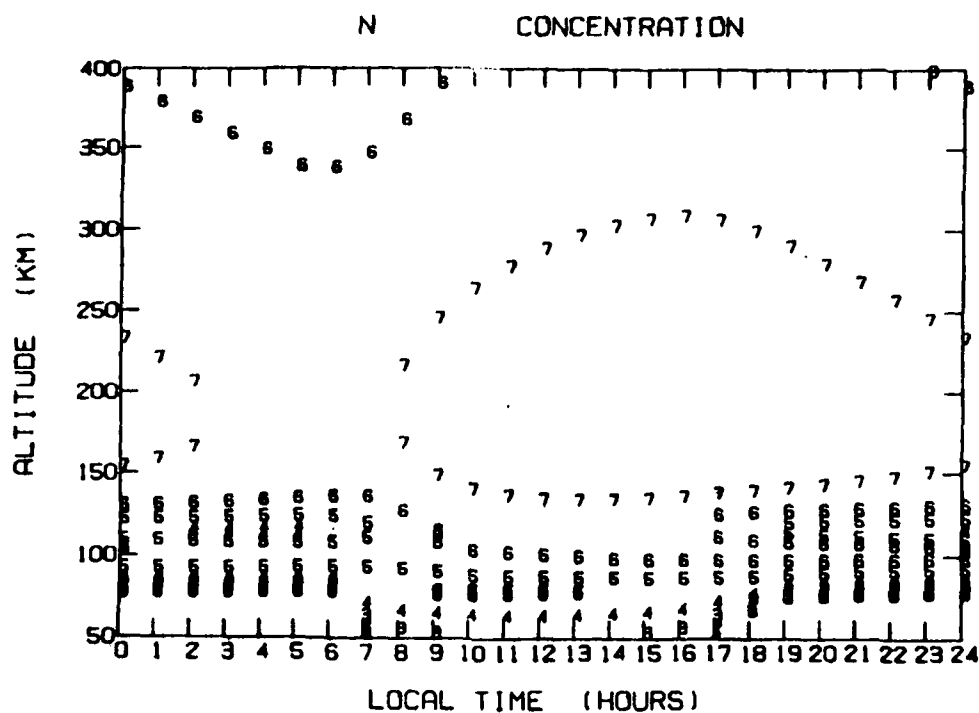


Figure 7. The Iso-Density Contours for Atomic Nitrogen

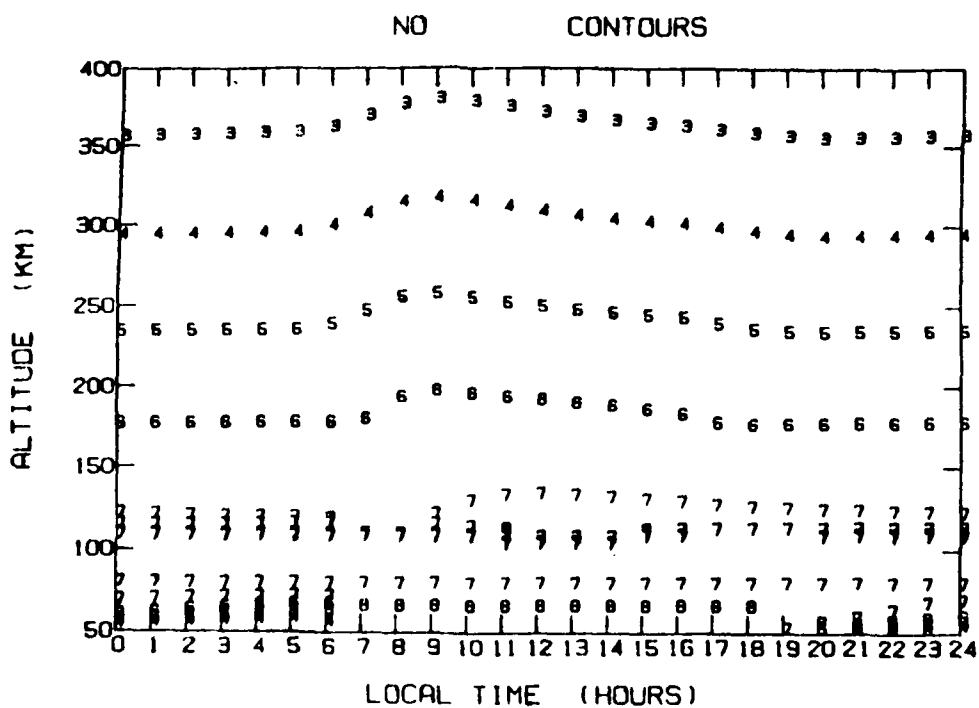


Figure 8. The Iso-Density Contours for Nitric Oxide

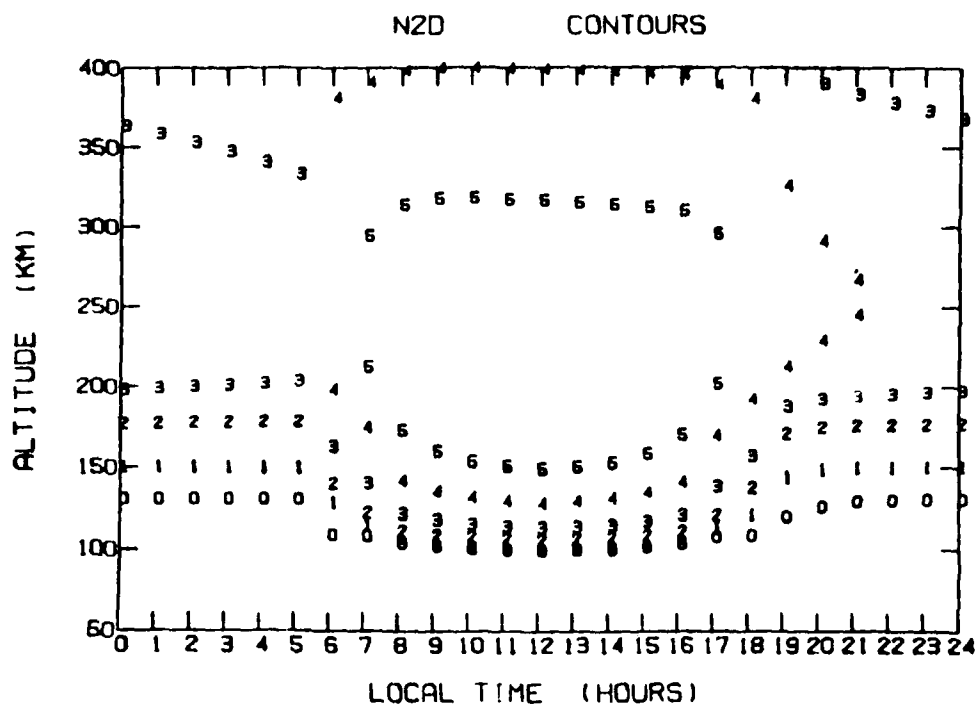


Figure 9. The Iso-Density Contours for N<sub>2</sub>D

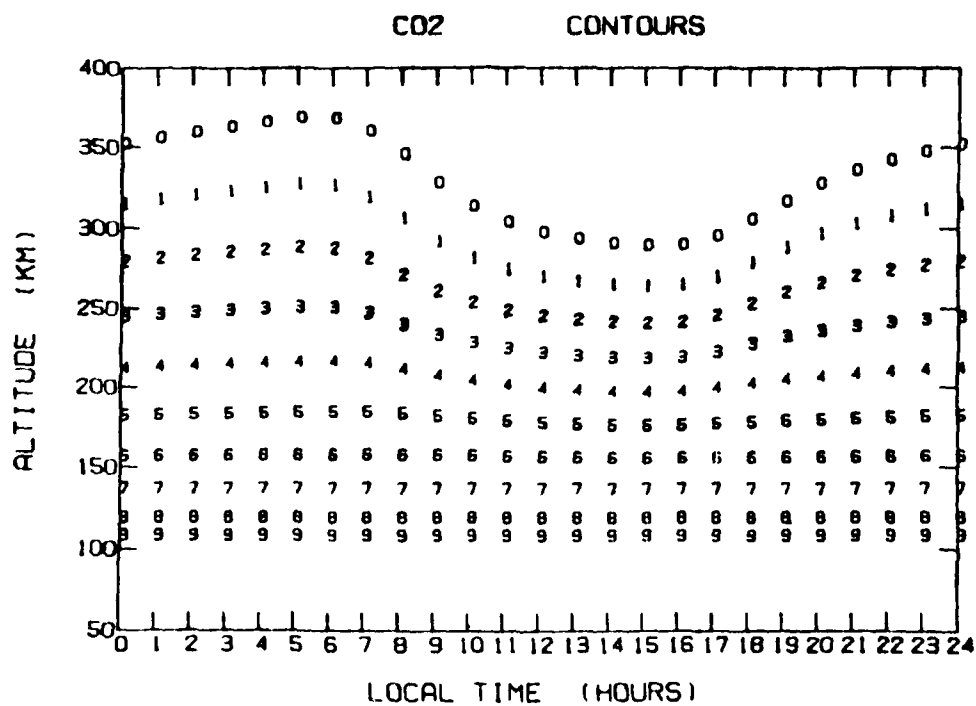


Figure 10. The Iso-Density Contours for Carbon Dioxide. The contours indicate a lack of any diurnal variation for this species below 150 km

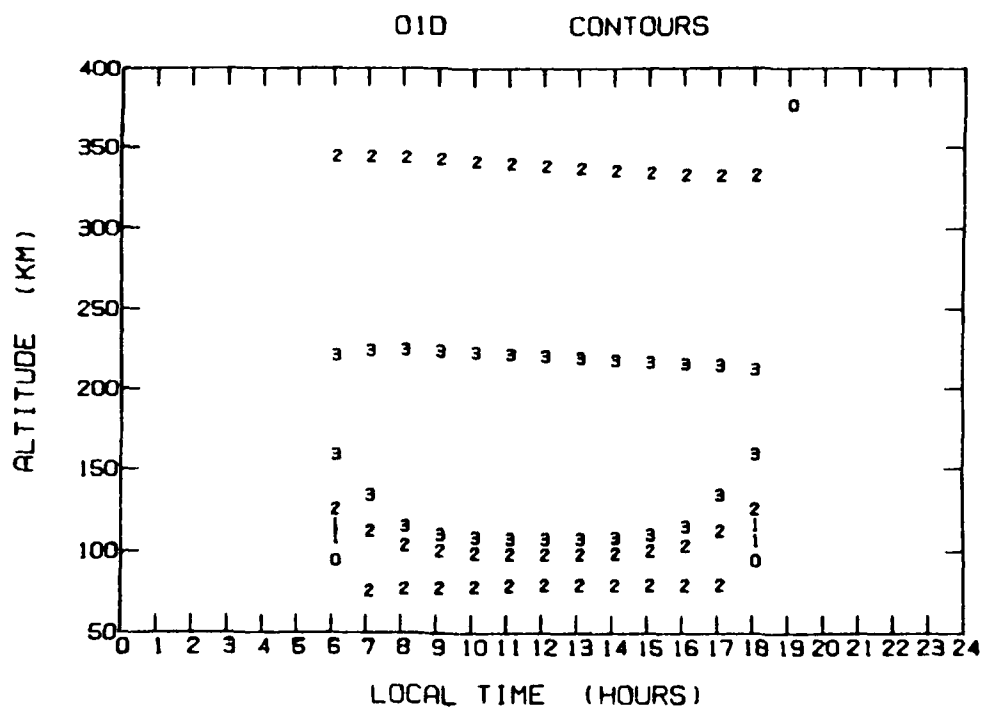


Figure 11. The Iso-Density Contours for  $O^1D$

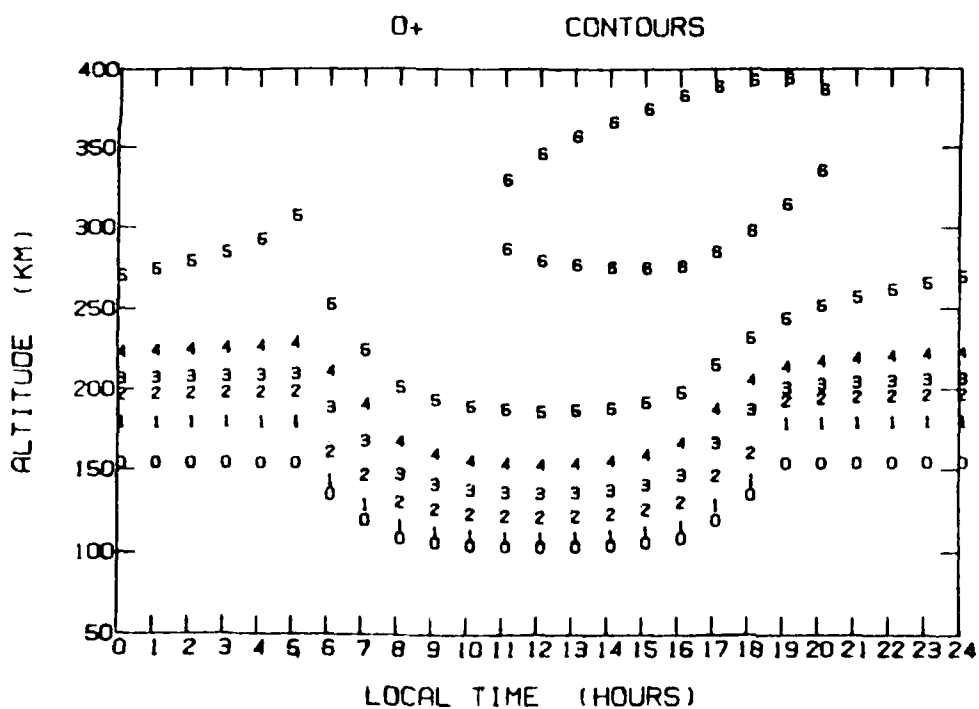


Figure 12. The Iso-Density Contours for  $O^+$ . The contours show the daytime F-layer peak ionization in excess of  $10^6 \text{ cm}^{-3}$

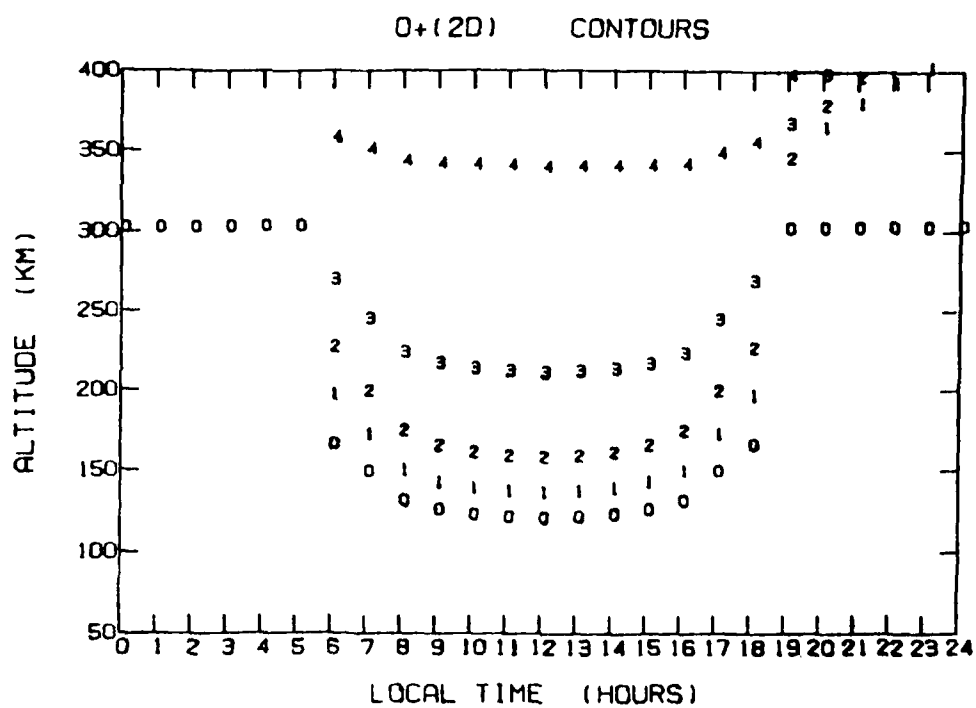


Figure 13. The Iso-Density Contours for O<sup>+</sup>(<sup>2</sup>D)

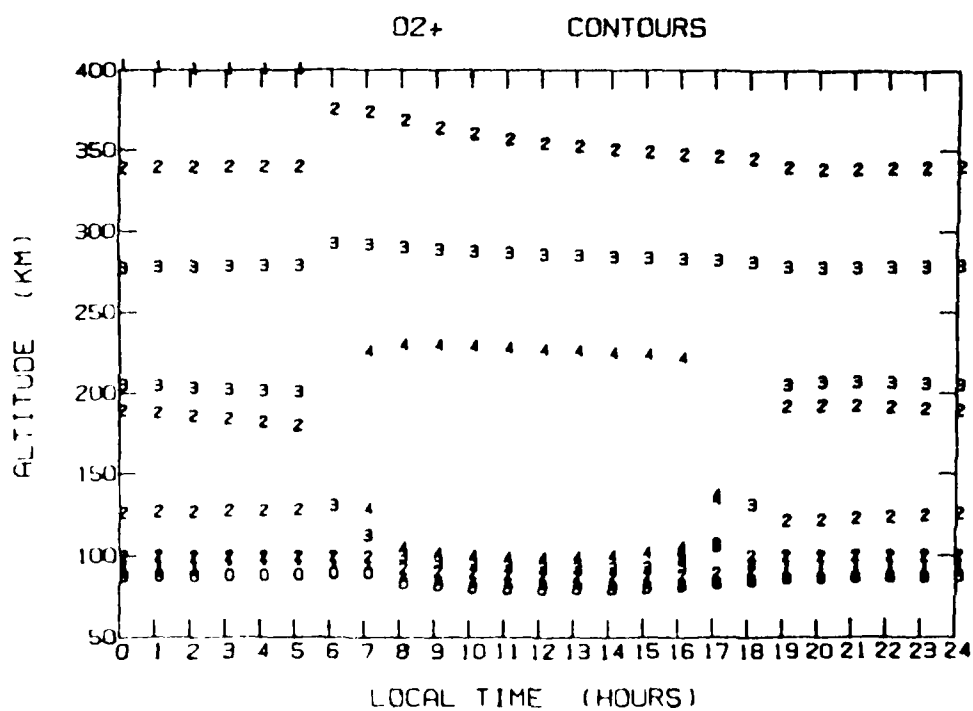


Figure 14. The Iso-Density Contours for O<sub>2</sub><sup>+</sup>

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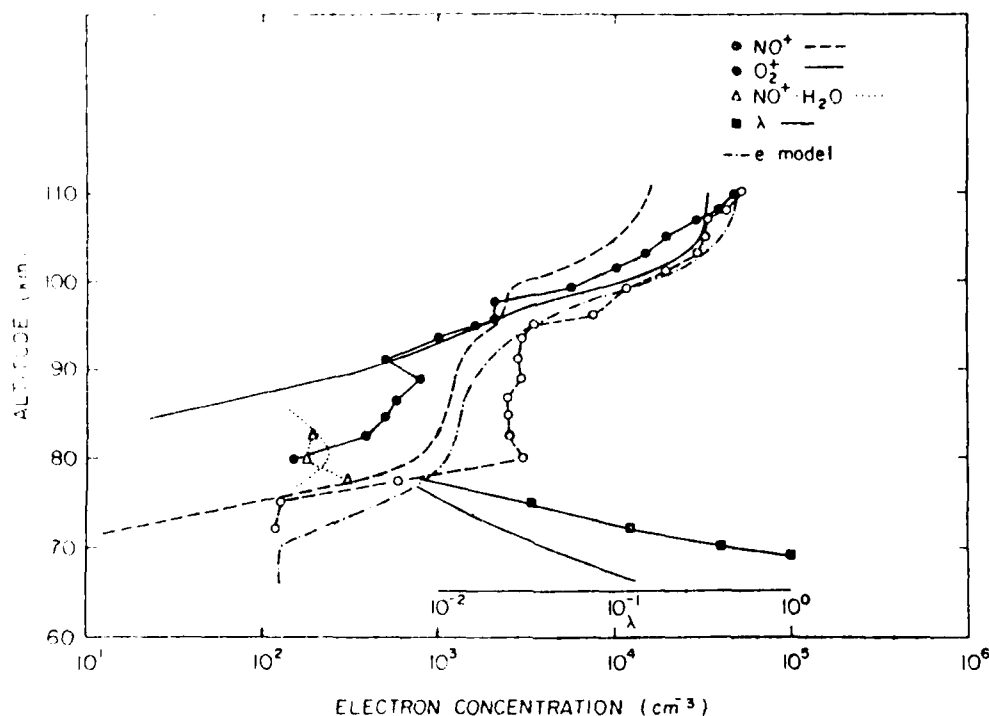
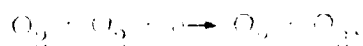


Figure 35. Altitude Profiles of  $\text{NO}_2^+$ ,  $\text{O}^+$ ,  $\text{NO}^+\cdot\text{H}_2\text{O}$ , Electrons and  $\lambda$ , the Ratio of Negative Ions to Electrons. The curves with symbols are the measurements reported by Torkar and Freidrich.<sup>40</sup> The curves without symbols are from this model

ions than the distribution determined in the Winter Anomaly campaign. However, there is a key reaction in the production of  $\text{O}_2^-$  in the early part of the negative ion chemistry scheme used by Viggiano et al,<sup>43</sup> namely



They used a rate coefficient of about  $1 \times 10^{-29} \text{ cm}^3 \text{ sec}^{-1}$  for this reaction. Phelps,<sup>41</sup> however, cites a rate coefficient of  $1.4 \times 10^{-29} (300/T) \exp(-600/T)$  for this reaction. This value would result in a theoretical altitude distribution of the negative ions similar to that in our calculations. Therefore, these data of Arnold et al<sup>41</sup> still are unexplained by theory and leave us with D-region negative ions that are still largely not understood.

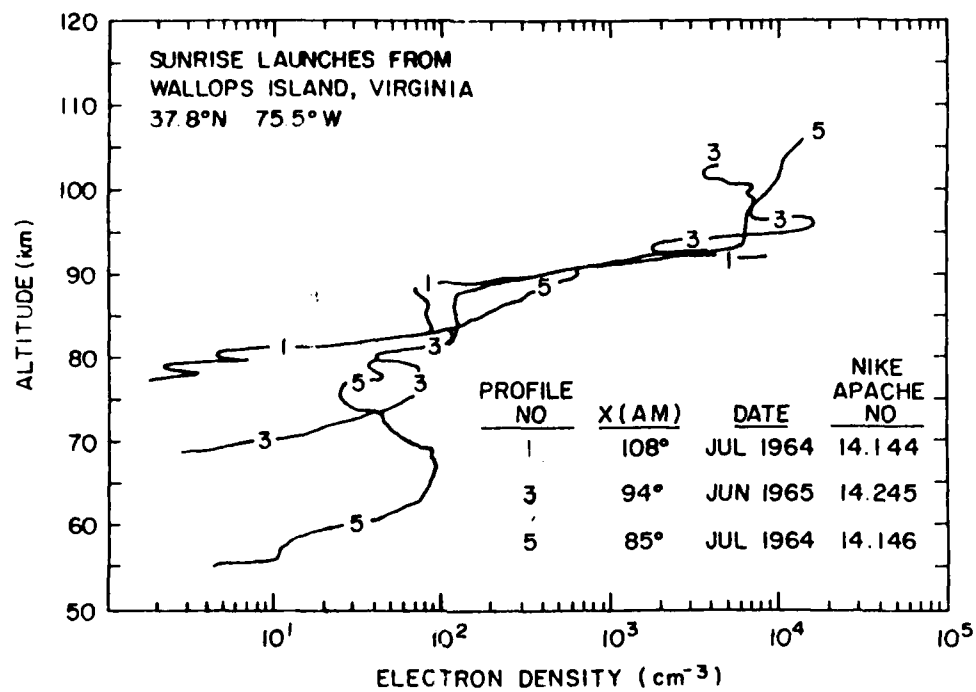


Figure 33. Altitude Profiles of Electron Density From Three Rocket Experiments at Wallops Island by Mechtly and Smith<sup>39</sup>

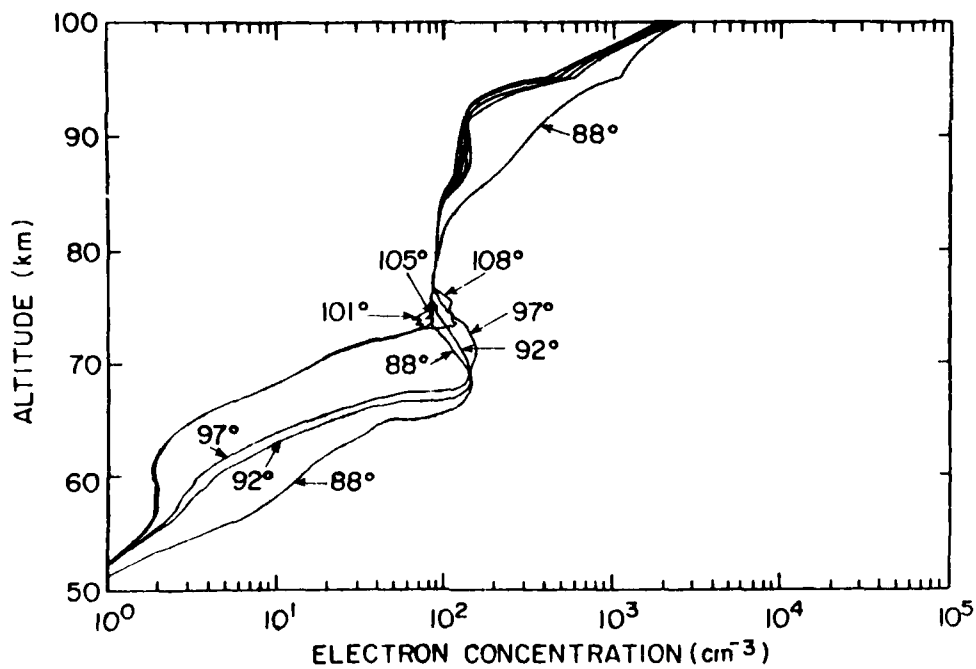


Figure 34. Altitude Profiles of the Electron Concentration From This Model at Several Zenith Angles During Sunrise

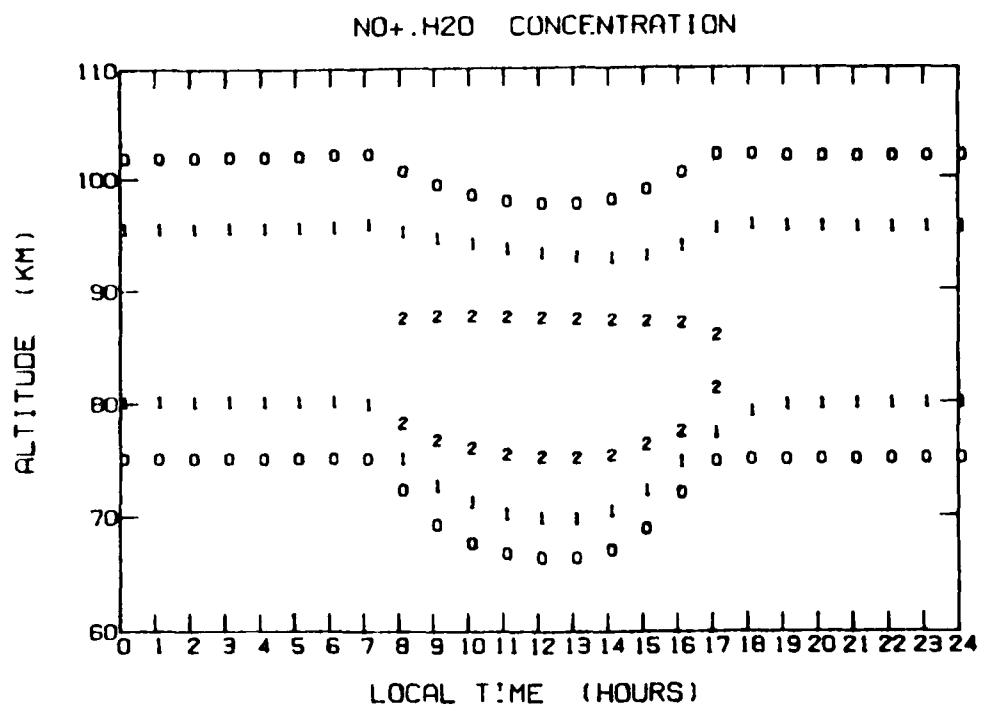


Figure 31. The Iso-Density Contours for  $\text{NO}^+ \cdot \text{H}_2\text{O}$  in the Mesosphere

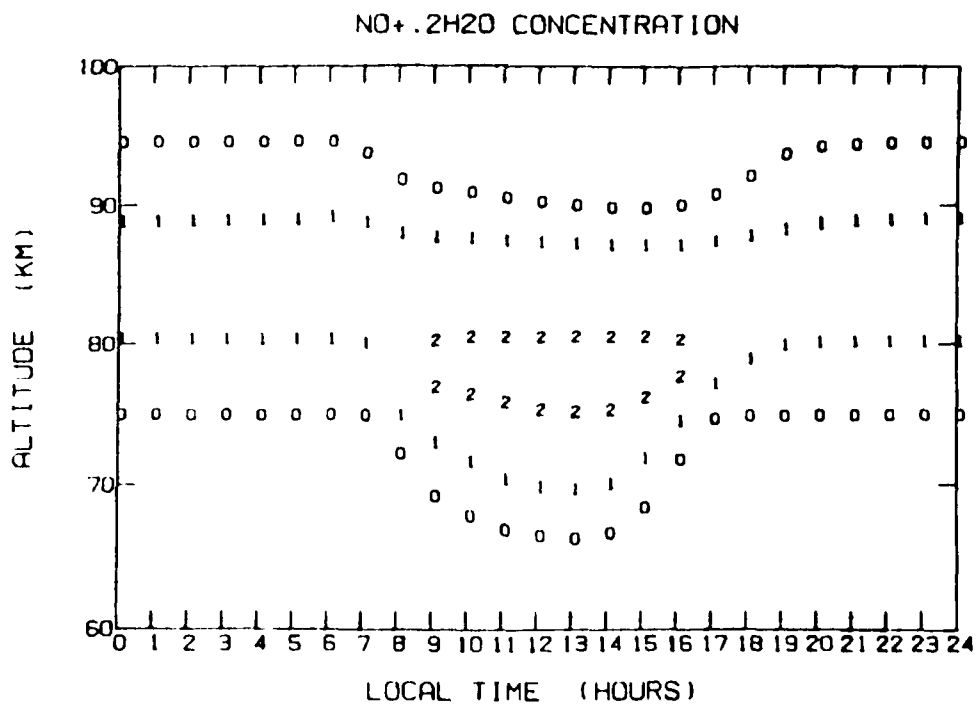


Figure 32. The Iso-Density Contours for  $\text{NO}^+ \cdot (\text{H}_2\text{O})_2$  in the Mesosphere

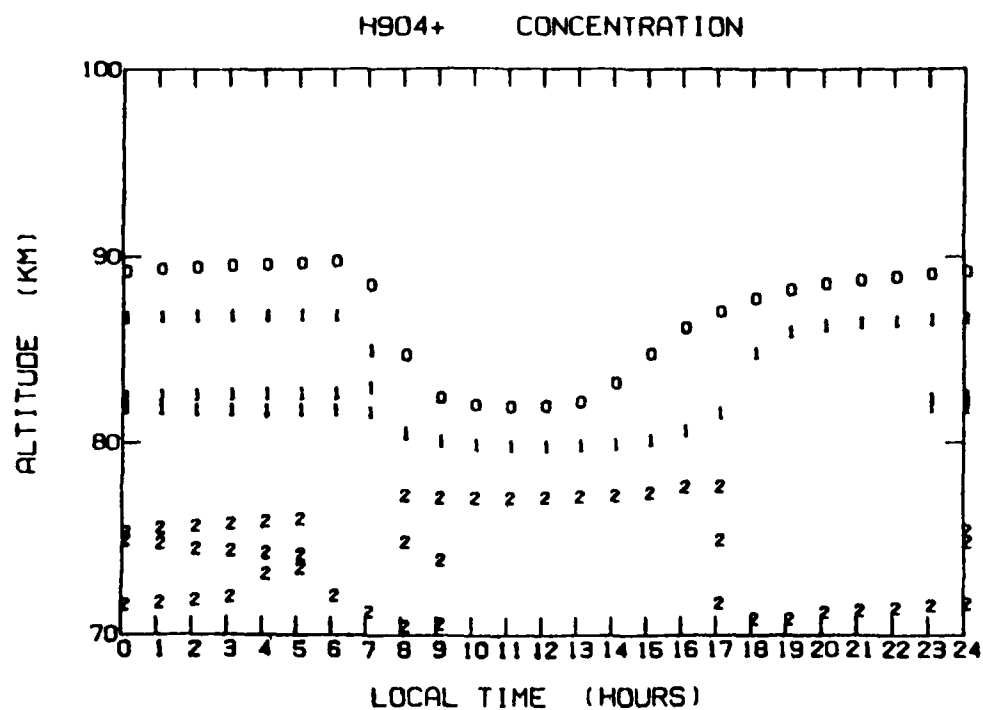


Figure 29. The Iso-Density Contours for  $\text{H}_9\text{O}_4^+$  in the Mesosphere

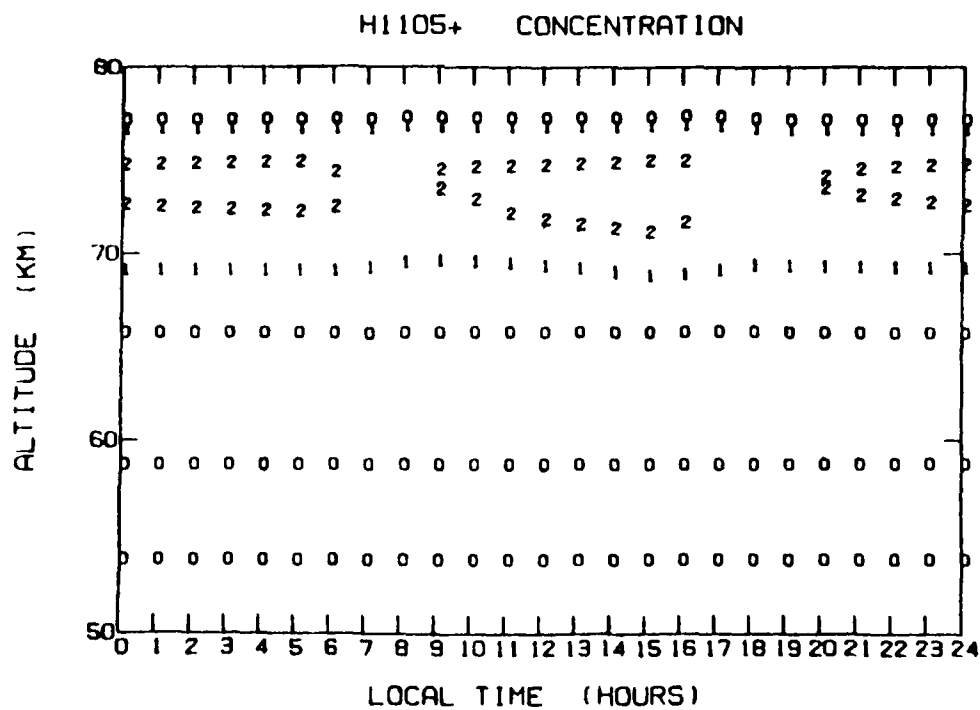


Figure 30. The Iso-Density Contours for  $\text{H}_{11}\text{O}_5^+$  in the Mesosphere

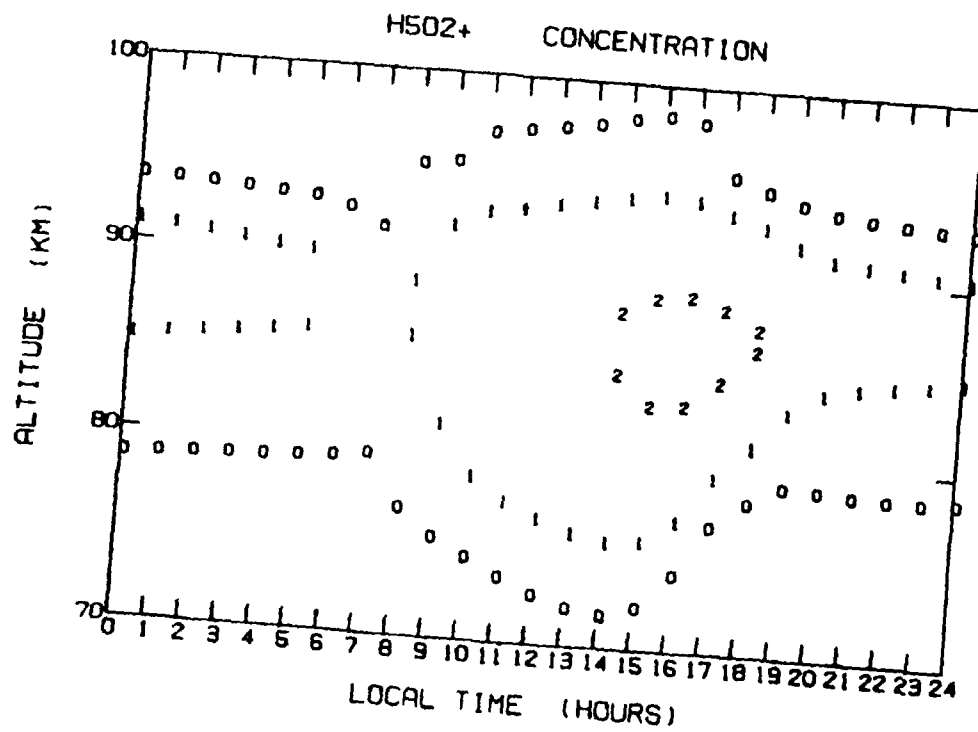


Figure 27. The Iso-Density Contours for  $H_5O_2^+$  in the Mesosphere

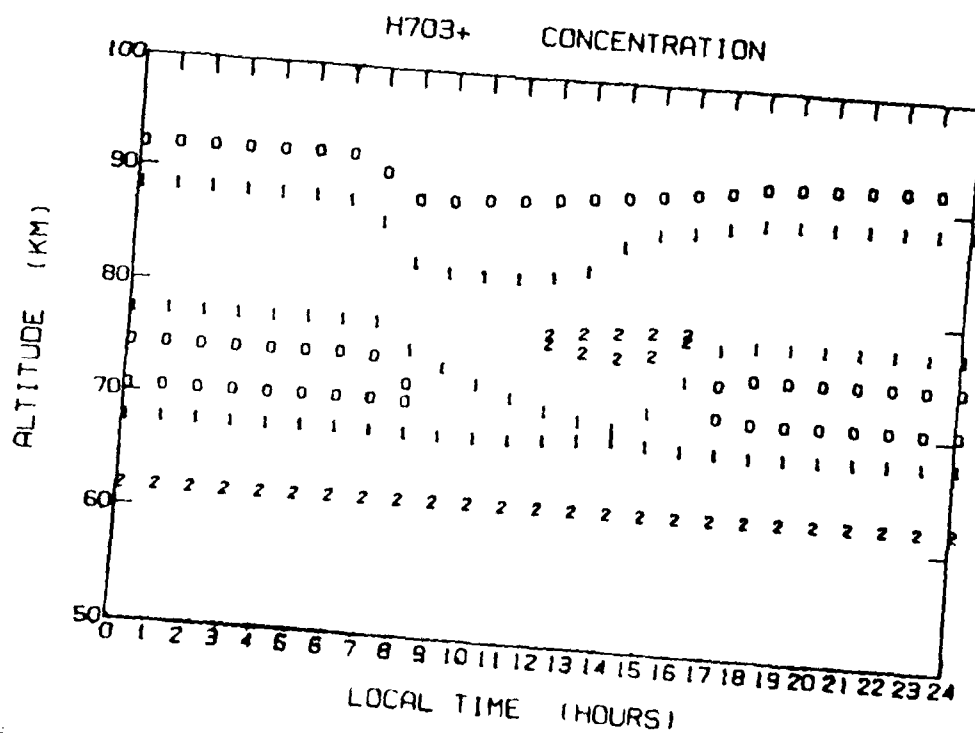


Figure 28. The Iso-Density Contours for  $H_7O_3^+$  in the Mesosphere

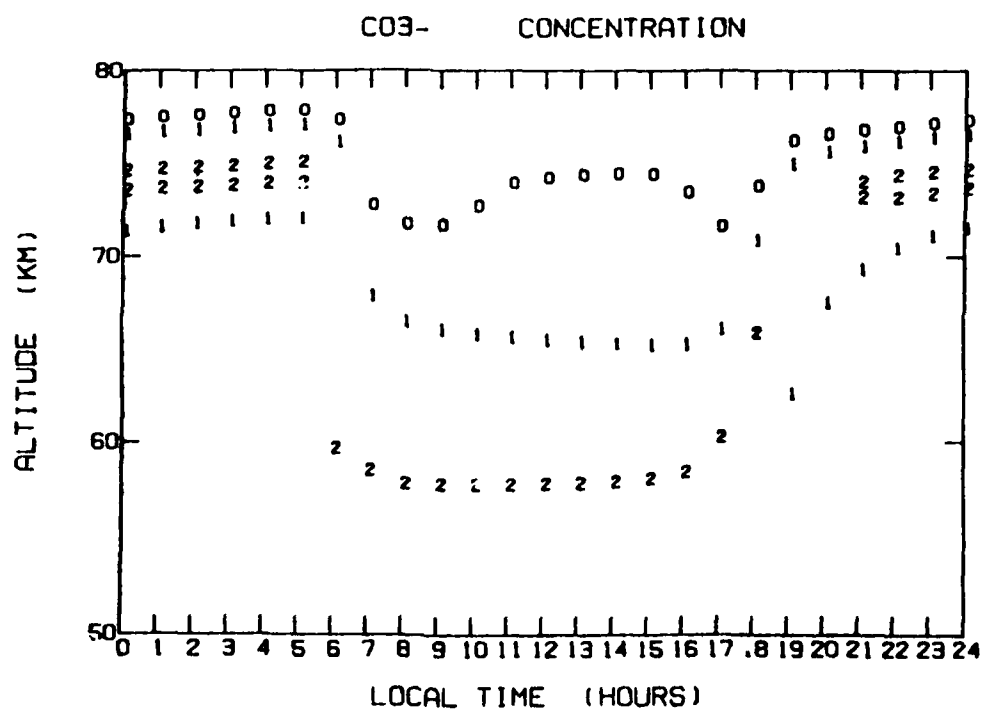


Figure 25. The Iso-Density Contours for  $\text{CO}_3^-$  in the Mesosphere

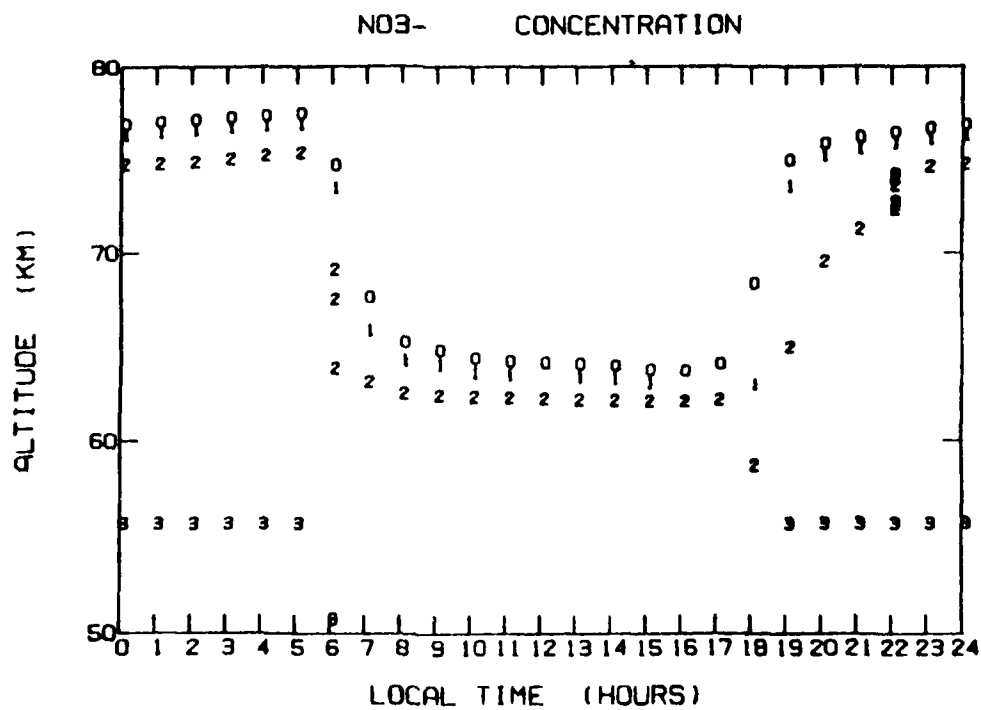


Figure 26. The Iso-Density Contours for  $\text{NO}_3^-$  in the Mesosphere

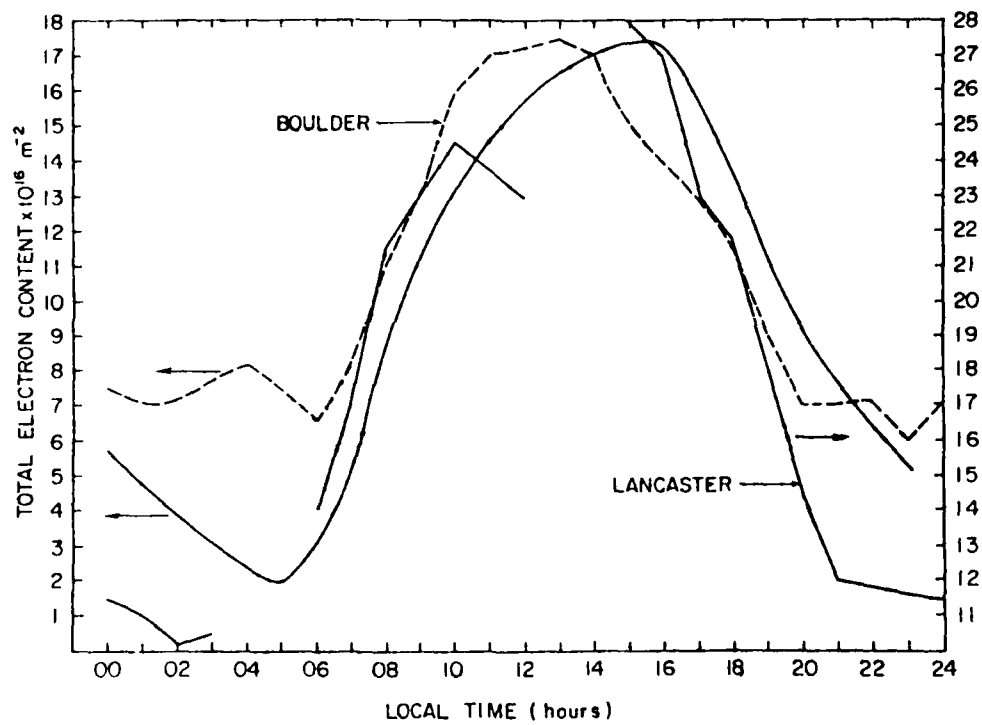


Figure 23. The Total Electron Content. The continuous curve is for this model. The dashed and broken curves are the measurements of Pouiter et al.<sup>34</sup>

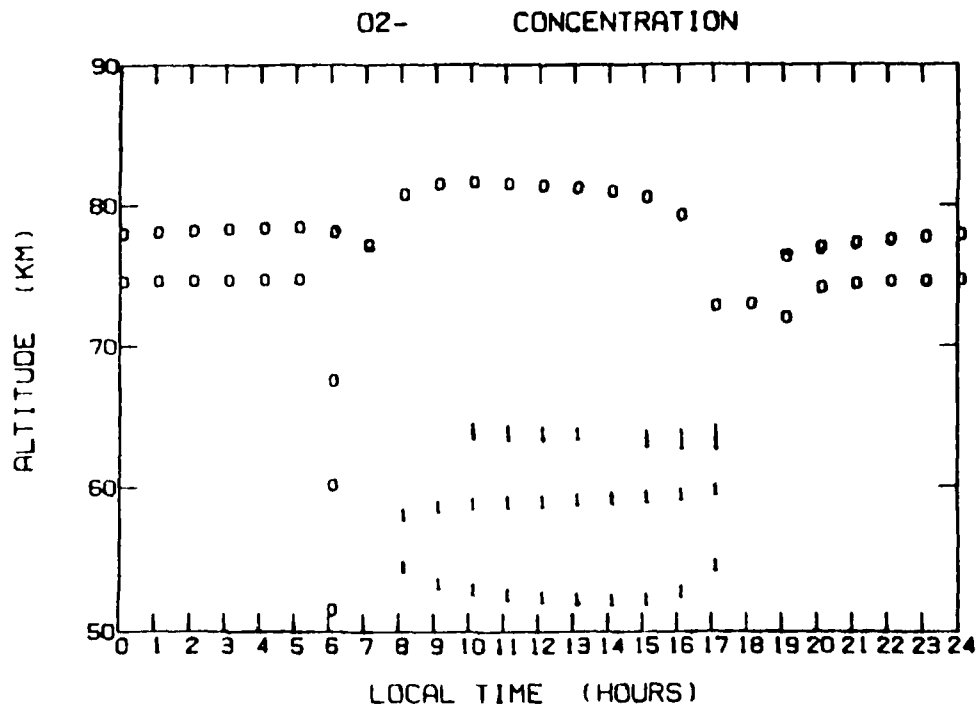


Figure 24. The Iso-Density Contours for  $O_2^-$  in the Mesosphere

region (Figure 19) compared to the work of Solomon et al.<sup>38</sup> Below 90 km, the cluster and negative ions change the effective electron density to a point where it disappears completely between 60 and 70 km.

The isodensity contours for the negative ions and the positive water cluster ions for the chemistry given in Appendix A are displayed in Figures 24 to 32. Isodensity plots for the remaining positive and negative mesospheric ions are not presented here because these ions never achieve a concentration greater than  $1 \text{ cm}^{-3}$  at any time during the diurnal cycle. Of course, the dominant negative ions in the mesosphere are apparently the cluster ions. Because their chemistry is still not fully understood, they have not been included in this work.

Particular emphasis is given to the sunrise period and a comparison of our electron density profiles with sequential measurements made at Wallops Island by Mechtly and Smith.<sup>39</sup> For clarity, the measured profiles are displayed in Figure 33, and our calculated profiles are shown in Figure 34. In some instances, the comparison of theory with experiment is fairly good. Substantial differences, however, do exist. These are, in part, a result of the differences in the seasons (summer for the measurement and winter for the model).

In explaining the D and lower E regions of the ionosphere, there is a question, still not completely answered, of the distribution of the positive and negative ions. To exemplify the puzzle, we cite two works. First, there is the report by Torkar and Freidrich<sup>40</sup> of the measurements taken during the "Winter Anomaly" campaign in Spain. The comparison between our calculations and those measurements, shown in Figure 35, is surprisingly good. In contrast are the measurements of Arnold et al.<sup>41</sup> and Viggiano and Arnold.<sup>42</sup> These measurements, supposedly explained by Viggiano et al.,<sup>43</sup> show an extremely different distribution of the negative

- 
38. Solomon, S., Reid, G.C., Roble, R.G., and Crutzen, P.J. (1982) Photochemical coupling between the thermosphere and the lower atmosphere, 2. D region ion chemistry and the winter anomaly, J. Geophys. Res. 87:7221-7227.
  39. Mechtly, E.A., and Smith, L.G. (1968) Growth of the D-region at sunrise, J. Atmos. Terr. Phys. 30:363-369.
  40. Torkar, K.M., and Friedrich, M. (1983) Tests of an ion-chemical model of the D- and lower E-region, J. Atmos. Terr. Phys. 45:369-385.
  41. Arnold, F., Viggiano, A.A., and Ferguson, E.E. (1982) Combined mass spectrometer composition measurements of positive and negative ions in the lower ionosphere-II. Negative ions, Planet. Space Sci. 30:1307-1314.
  42. Viggiano, A.A., and Arnold, F. (1981) The first height measurements of the negative ion composition of the stratosphere, Planet. Space Sci. 29:895-906.
  43. Viggiano, A.A., Arnold, F., Fahey, D.W., Fehsenfeld, F.C., and Ferguson, E.E. (1982) Silicon negative ion chemistry in the atmosphere--in situ and laboratory measurements, Planet. Space Sci. 30:499-506.



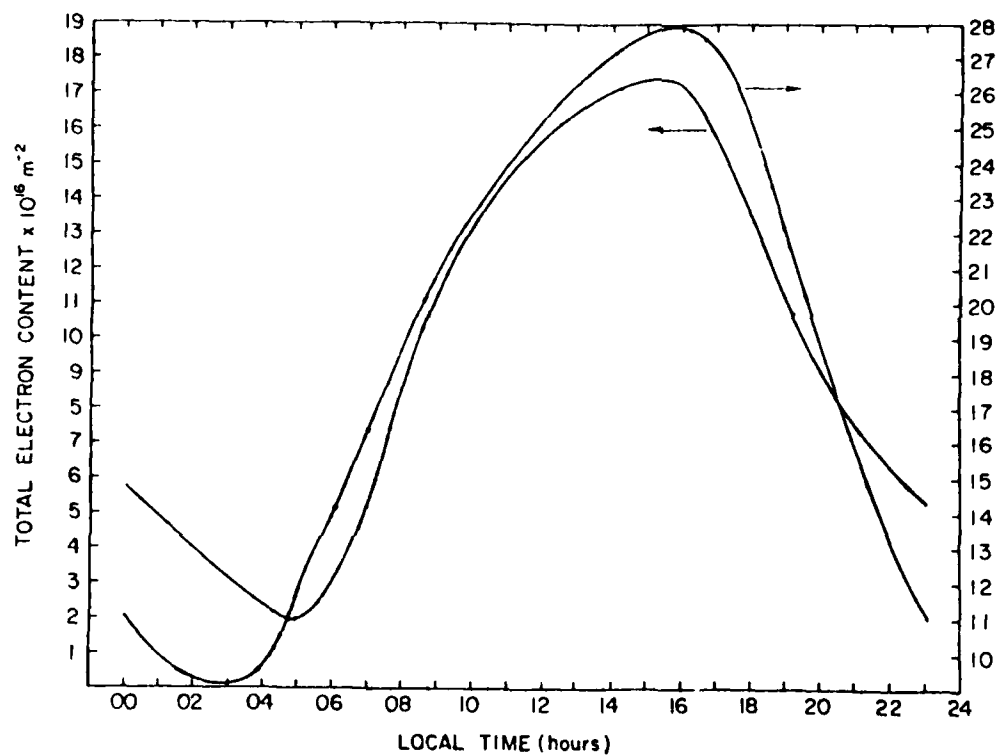


Figure 21. The Total Electron Content. The left-hand scale is for this model. The right-hand scale is for the calculations of Sethia et al<sup>33</sup>

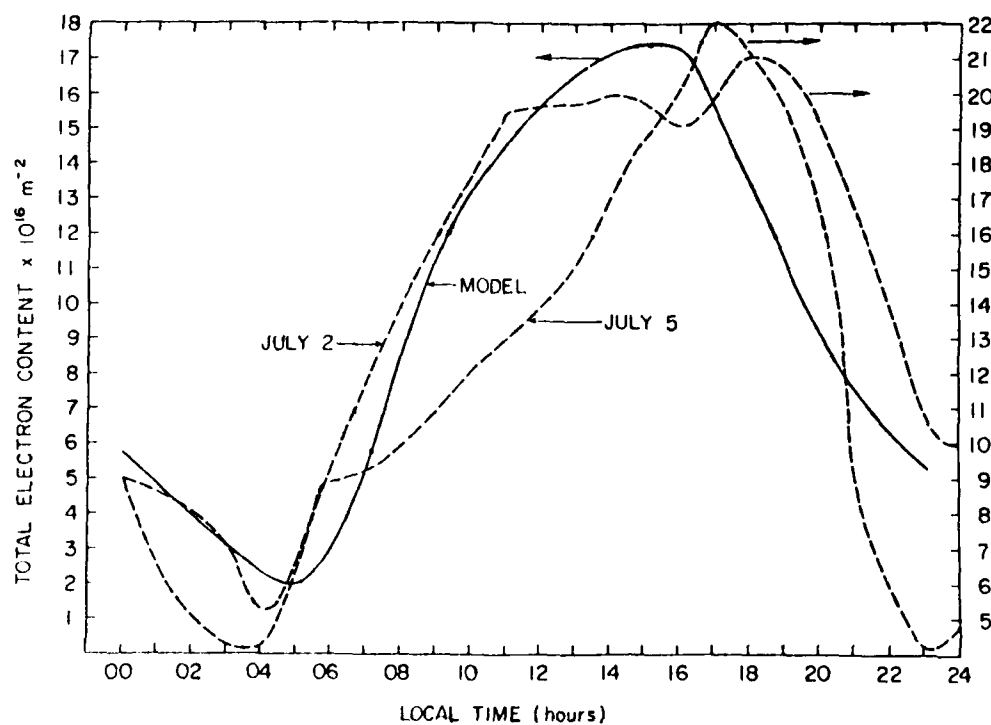


Figure 22. The Total Electron Content. The solid curve is for this model. The dashed curves are the measurements of Sethia et al<sup>33</sup>

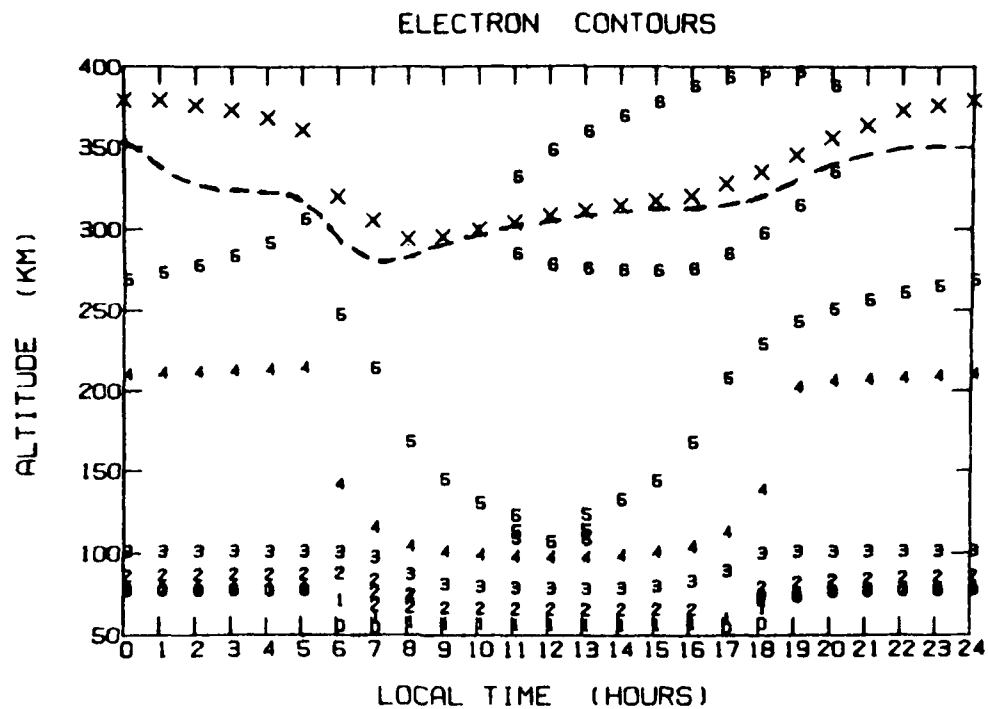


Figure 19. The Iso-Density Contours for the Electrons. The crosses show the diurnal change in the altitude of the peak electron concentration in the model. The dashed curve indicates the measurement of this parameter by Evans<sup>31</sup>

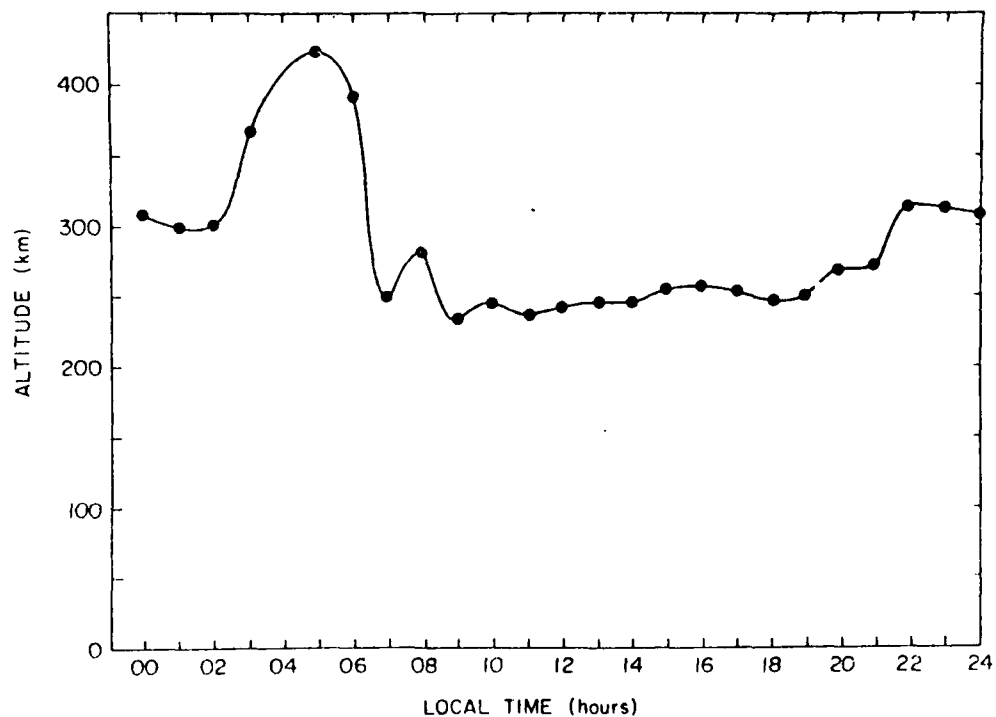


Figure 20. Measurements of Reinisch<sup>32</sup> of the Height of the F-Layer Peak at Eglin AFB, Fla., on 20/21 November 1970

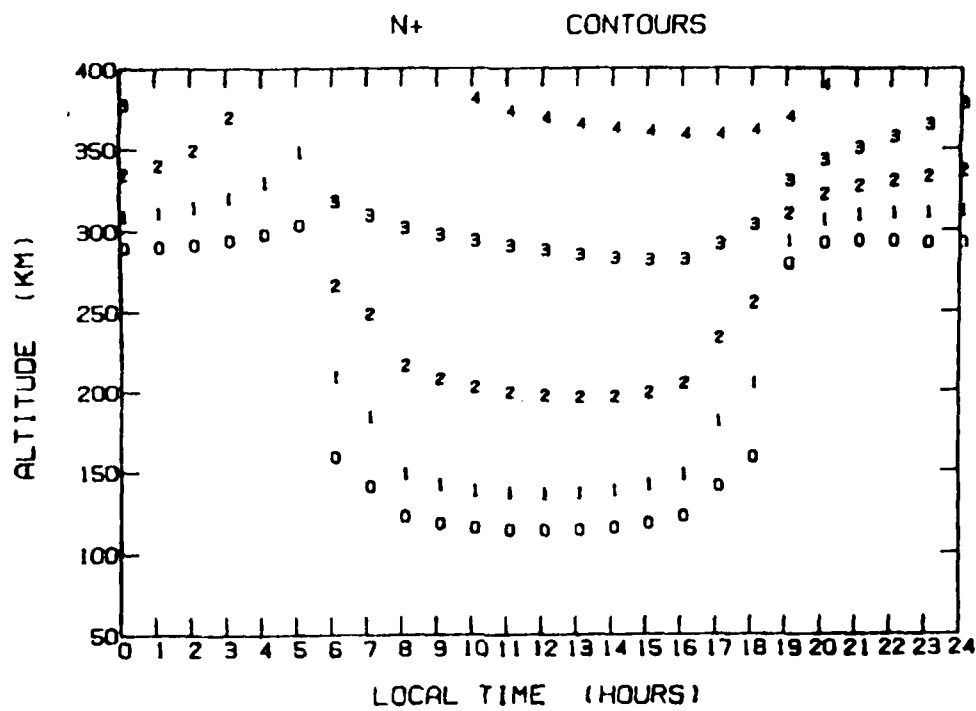


Figure 17. The Iso-Density Contours for N<sup>+</sup>

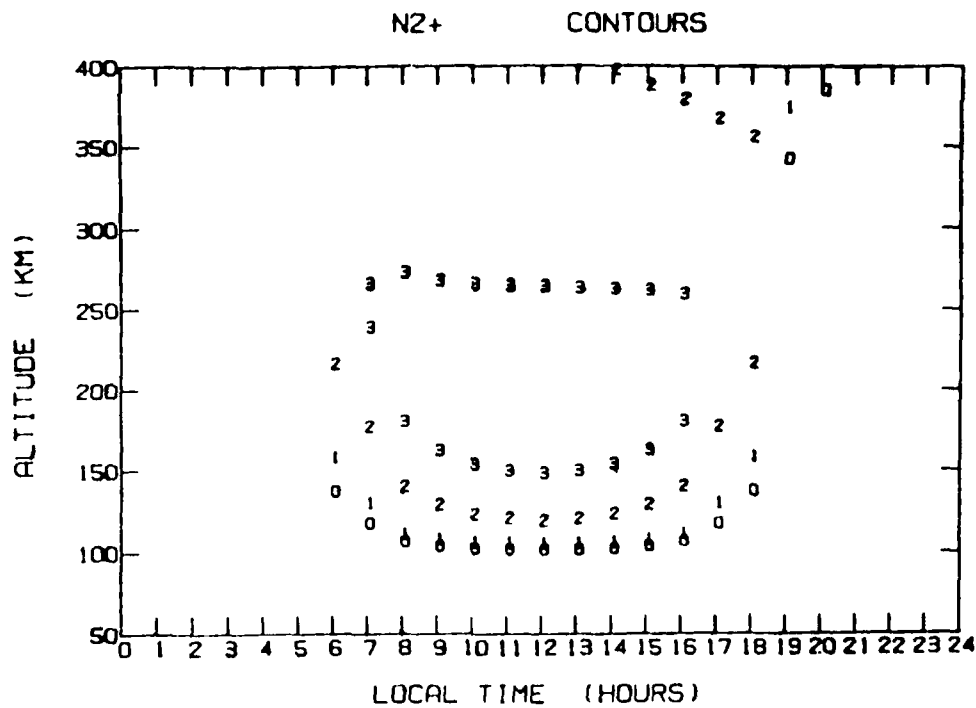


Figure 18. The Iso-Density Contours for N<sub>2</sub><sup>+</sup>. At night, the concentration of N<sub>2</sub><sup>+</sup> falls below 1 cm<sup>-3</sup> at all altitudes

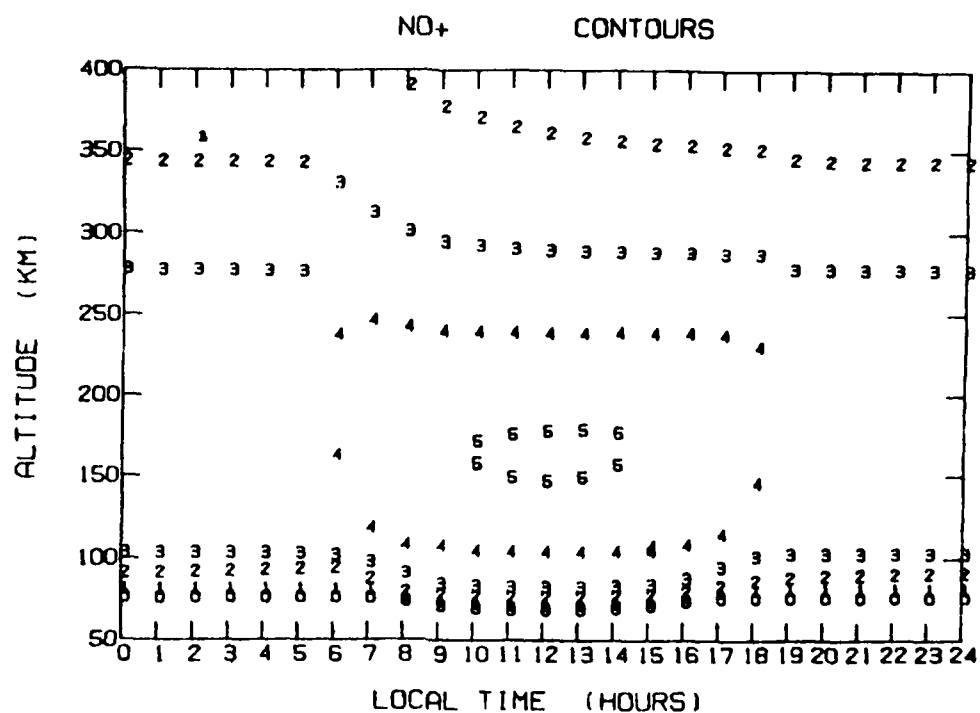


Figure 15. The Iso-Density Contours for NO<sup>+</sup>

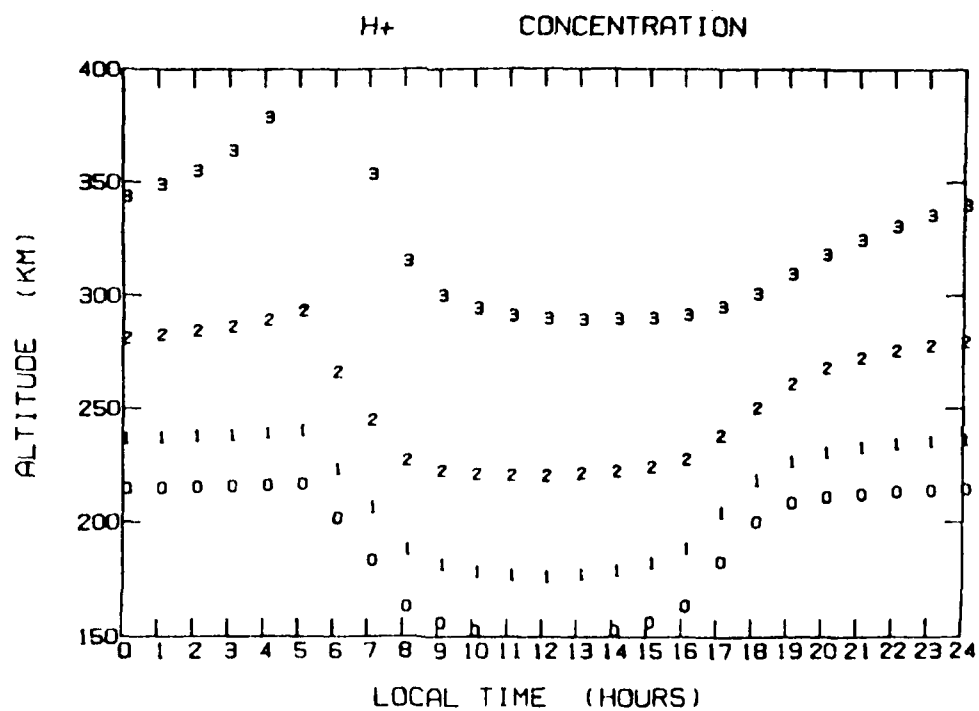


Figure 16. The Iso-Density Contours for H<sup>+</sup>

34. Poulter, E.M., Hargreaves, J.K., Bailey, G.J., and Moffet, R.J. (1981) Electron content modelling: The significance of protonospheric contents, Planet. Space Sci. 29:869-883.
35. Kohl, H., King, J.W., and Eccles, D. (1969) An explanation of the magnetic declination effect in the ionospheric F-layer, J. Atmos. Terr. Phys. 31:1011-1016.
36. Rishbeth, H. (1972) Thermospheric winds and the F-region: A review, J. Atmos. Terr. Phys. 34:1-47.
37. Rush, C.M., Kempner, M.P., Anderson, D.N., Stewart, F.G., and Perry, J. (1983) Improving ionospheric maps using theoretically derived values, Radio Sci. 18:95-107.
38. Solomon, S., Reid, G.C., Roble, R.G., and Crutzen, P.J. (1982) Photochemical coupling between the thermosphere and the lower atmosphere, 2. D region ion chemistry and the winter anomaly, J. Geophys. Res. 87:7221-7227.
39. Mechtly, E.A., and Smith, L.G. (1968) Growth of the D-region at sunrise, J. Atmos. Terr. Phys. 30:363-369.
40. Torkar, K.M., and Friedrich, M. (1983) Tests of an ion-chemical model of the D- and lower E-region, J. Atmos. Terr. Phys. 45:369-385.
41. Arnold, F., Viggiano, A.A., and Ferguson, E.E. (1982) Combined mass spectrometer composition measurements of positive and negative ions in the lower ionosphere—II. Negative ions, Planet. Space Sci. 30:1307-1314.
42. Viggiano, A.A., and Arnold, F. (1981) The first height measurements of the negative ion composition of the stratosphere, Planet. Space Sci. 29:895-906.
43. Viggiano, A.A., Arnold, F., Fahey, D.W., Fehsenfeld, F.C., and Ferguson, E.E. (1982) Silicon negative ion chemistry in the atmosphere—in situ and laboratory measurements, Planet. Space Sci. 30:499-506.

## Appendix A

### The Chemical Reactions

Table A1 lists the complete set of chemical reactions used in this report. Reactions 1 through 127 have temperature invariant rate coefficients that are listed after each reaction along with the source from which the rate coefficient was taken. Reactions 128 through 184 are temperature dependent. The rate coefficients for these reactions are of the form

$$k(z) = A \left( \frac{T(z)}{300} \right)^B \exp \left( \frac{C}{T(z)} \right) \quad (A1)$$

where the A's, B's, and C's are listed in that order after each reaction and  $T(z)$  is the temperature at altitude  $z$ . Reactions 185 through 207 are the photo-reactions, and are functions of the wavelength of the solar radiation and the local solar flux. Reactions 208 through 215 are the energetic electron processes. Some of the rate coefficients in the list of reactions have not been measured in the laboratory. Therefore, these rate coefficients are given as estimates.

Table A1. Chemical Reaction Scheme

NO.	CHEMICAL REACTION	A	B	C	REFERENCE
1	O	1.00E-12	0.00	0.	A1 DAVENPORT ET AL (1976)
2	O	2.20E-11	0.00	0.	A2 BAULCH ET AL (1972)
3	O	1.00E-11	0.00	0.	A3 KAUFMAN (1964)
4	O	9.10E-12	0.00	0.	A4 DAVIS ET AL (1973)
5	H	1.40E-11	0.00	0.	A2 BAULCH ET AL (1972)
6	H	1.00E-11	0.00	0.	A5 KAUFMAN (1964)
7	H	2.60E-11	0.00	0.	A5 PHILLIPS AND SCHIFF (1962B)
8	N	5.70E-13	0.00	0.	A6 PHILLIPS AND SCHIFF (1962A)
9	N	8.00E-12	0.00	0.	A7 PHILLIPS AND SCHIFF (1965)
10	N	6.00E-12	0.00	0.	A7 PHILLIPS AND SCHIFF (1965)
11	N	4.00E-12	0.00	0.	A7 PHILLIPS AND SCHIFF (1965)
12	OH	2.00E-12	0.00	0.	A5 KAUFMAN (1969)
13	OH	2.00E-10	0.00	0.	A7 HOCHANDEL ET AL (1972)
14	N2	6.00E-12	0.00	0.	A10 LIN AND KAUFMAN (1971)
15	O1D	2.10E-10	0.00	0.	A11 DAVIDSON ET AL (1976)
16	O1D	3.00E-11	0.00	0.	A11 DAVIDSON ET AL (1976)
17	O1D	1.30E-10	0.00	0.	A11 DAVIDSON ET AL (1976)
18	O21D	4.40E-19	0.00	0.	A12 CLARK AND WAYNE (1969)
19	O21D	2.58E-04	0.00	0.	A13 BADGER ET AL (1965)
20	HNO2	1.00E-15	0.00	0.	A14 KAISER AND JAPER (1978)
21	HNO2	6.60E-12	0.00	0.	A15 COX ET AL (1976)
22	N2+	1.50E-07	0.00	0.	A16 BIONDI (1969)
23	N2+	1.50E-07	0.00	0.	A16 BIONDI (1969)
24	H3O+	2.00E-06	0.00	0.	A17 BIONDI (1973)
25	H5O2+	1.00E-06	0.00	0.	A17 BIONDI (1973)
26	H7O3+	4.00E-06	0.00	0.	A17 BIONDI (1973)
27	H9O4+	5.00E-06	0.00	0.	A17 BIONDI (1973)
28	H11O5+	7.50E-06	0.00	0.	A17 BIONDI (1973)
29	H3O+.OH	2.00E-06	0.00	0.	ESTIMATED
30	H5O2+.CO2+	2.00E-06	0.00	0.	ESTIMATED
31	O	1.30E-15	0.00	0.	ESTIMATED
32	O2	1.00E-31	0.00	0.	A18 BRANSCOMB (1964)
33	O2+	6.00E-10	0.00	0.	A19 PHELPS (1989)
34	O2+	1.80E-10	0.00	0.	A20 FERGUSON (1973)
35	O2+	6.60E-10	0.00	0.	A21 GOLDAN ET AL (1966)
36	O4+	3.00E-10	0.00	0.	A22 FENSFELD ET AL (1973)
37	O4+	1.50E-09	0.00	0.	A23 FERGUSON (1973)
38	N2+	7.50E-11	0.00	0.	A23 HOWARD ET AL (1972)
39	N2+	7.50E-11	0.00	0.	A24 FERGUSON (1974)
40	O+	6.00E-10	0.00	0.	A24 FERGUSON (1974)
41	H+	4.00E-10	0.00	0.	A24 FERGUSON (1974)
42	N+	6.00E-10	0.00	0.	A24 FERGUSON (1974)
43	N+	6.00E-10	0.00	0.	A25 DUNKIN ET AL (1968)
44	N+	2.00E-10	0.00	0.	A24 FERGUSON (1974)
45	HE+	1.50E-09	0.00	0.	A24 FERGUSON (1974)
46	HE+	2.00E-10	0.00	0.	A24 FERGUSON (1974)
47	HE+	1.50E-09	0.00	0.	A24 FERGUSON (1974)

Table A1. Chemical Reaction Scheme (Contd)

NO.	CHEMICAL REACTION	A	B	C	REFERENCE
48	HE+ + N2	3.50E-10	0.00	0.	A24 FERGUSON (1974)
49	HE+ + NO	1.50E-09	0.00	0.	A26 FEHSENFELD ET AL (1966)
50	NO2+ + NO	2.90E-10	0.00	0.	A26 FEHSENFELD ET AL (1969A)
51	H502+ + CO2	3.00E-30	0.00	0.	ESTIMATED
52	H904+ + H2O	1.00E-27	0.00	0.	ESTIMATED
53	O2+ + H2O	1.00E-09	0.00	0.	A23 HOWARD ET AL (1972)
54	O2+ + H2O	2.00E-10	0.00	0.	A23 HOWARD ET AL (1972)
55	NO+ + 3H2O	1.00E-11	0.00	0.	A25 PUCKETT AND TEAGUE (1971)
56	NO+ + CO2	1.00E-09	0.00	0.	ESTIMATED
57	H30+ + N2	1.00E-10	0.00	0.	ESTIMATED
58	H30+ + CO2	1.00E-27	0.00	0.	ESTIMATED
59	H502+ + CO2	1.00E-10	0.00	0.	ESTIMATED
60	H30+ + CO2	1.00E-10	0.00	0.	ESTIMATED
61	H30+ + OH	1.40E-09	0.00	0.	A23 HOWARD ET AL (1972)
62	H30+ + NO2	6.00E-08	0.00	0.	ESTIMATED
63	H30+ + NO3	6.00E-08	0.00	0.	ESTIMATED
64	H30+ + CO3	6.00E-08	0.00	0.	ESTIMATED
65	H502+ + O2	6.00E-08	0.00	0.	ESTIMATED
66	H502+ + NO2	6.00E-08	0.00	0.	ESTIMATED
67	H502+ + NO3	6.00E-08	0.00	0.	ESTIMATED
68	H502+ + CO3	6.00E-08	0.00	0.	ESTIMATED
69	H502+ + CO4	6.00E-08	0.00	0.	ESTIMATED
70	H703+ + NO2	6.00E-08	0.00	0.	ESTIMATED
71	H703+ + NO3	6.00E-08	0.00	0.	ESTIMATED
72	H703+ + CO3	6.00E-08	0.00	0.	ESTIMATED
73	H703+ + CO4	6.00E-08	0.00	0.	ESTIMATED
74	H904+ + NO2	6.00E-08	0.00	0.	ESTIMATED
75	H904+ + NO3	6.00E-08	0.00	0.	ESTIMATED
76	H904+ + CO3	6.00E-08	0.00	0.	ESTIMATED
77	H904+ + CO4	6.00E-08	0.00	0.	ESTIMATED
78	H1105+ + NO2	6.00E-08	0.00	0.	ESTIMATED
79	H1105+ + NO3	6.00E-08	0.00	0.	ESTIMATED
80	H1105+ + CO3	6.00E-08	0.00	0.	ESTIMATED
81	H1105+ + CO4	6.00E-08	0.00	0.	ESTIMATED
82	NO+ + H2O	6.00E-08	0.00	0.	ESTIMATED
83	NO+ + H2O	6.00E-08	0.00	0.	ESTIMATED
84	NO+ + H2O	6.00E-08	0.00	0.	ESTIMATED
85	NO+ + 2H2O	6.00E-08	0.00	0.	ESTIMATED
86	NO+ + 2H2O	6.00E-08	0.00	0.	ESTIMATED
87	NO+ + 2H2O	6.00E-08	0.00	0.	ESTIMATED
88	NO+ + 3H2O	6.00E-08	0.00	0.	ESTIMATED
89	NO+ + 3H2O	6.00E-08	0.00	0.	ESTIMATED
90	NO+ + 3H2O	6.00E-08	0.00	0.	ESTIMATED
91	H30+ + CO2	6.00E-08	0.00	0.	ESTIMATED
92	H30+ + CO2	6.00E-08	0.00	0.	ESTIMATED
93	H30+ + CO2	6.00E-08	0.00	0.	ESTIMATED
94	H502+ + CO2 + CO3	6.00E-08	0.00	0.	ESTIMATED



Table A1. Chemical Reaction Scheme (Contd)

NO.	CHEMICAL REACTION	2H2O	+ H2O	A	B	C	REFERENCE
95	H2O2 + CO2 → CO4- + HV	+ E		6.00E-08	0.00	0.	ESTIMATED
96	O- → O	+ E		1.40E+00	0.00	0.	A30 BRANSCOMB ET AL (1958)
97	O- → O3	+ E		2.00E-10	0.00	0.	A31 FEHSENFELD ET AL (1967)
98	O- → O3	+ E		5.30E-10	0.00	0.	A31 FEHSENFELD ET AL (1967)
99	O2- → O3	+ E		3.30E-01	0.00	0.	A32 WOO ET AL (1969)
100	O2- → O3	+ E		1.50E-10	0.00	0.	A33 FEHSENFELD ET AL (1969C)
101	O2- → O3	+ O2		1.50E-10	0.00	0.	A34 BORTNER AND BAURER (1979)
102	O2- → O3	+ O2		4.00E-10	0.00	0.	A31 FEHSENFELD ET AL (1967B)
103	O2- → O3	+ O2		2.00E-10	0.00	0.	A31 FEHSENFELD ET AL (1969C)
104	O3- → O3	+ E		7.00E-02	0.00	0.	A35 WONG ET AL (1972)
105	O3- → O3	+ O2		5.00E-01	0.00	0.	A36 PETERSON (1976)
106	O3- → O3	+ O2		3.20E-10	0.00	0.	A34 BORTNER AND BAURER (1979)
107	O4- → O3	+ O2		3.00E-10	0.00	0.	A37 FEHSENFELD ET AL (1969B)
108	O4- → O3	+ O2		1.00E-10	0.00	0.	A37 FEHSENFELD ET AL (1969B)
109	O4- → O3	+ O2		4.30E-10	0.00	0.	A38 ADAMS ET AL (1970)
110	CO3- → CO4-	+ CO2		2.00E-01	0.00	0.	A36 PETERSON (1976)
111	CO3- → CO4-	+ CO2		8.00E-11	0.00	0.	A34 FERGUSON (1974)
112	CO3- → CO4-	+ CO2		2.00E-10	0.00	0.	A39 FEHSENFELD AND FERGUSON (1974)
113	CO4- → CO4-	+ CO2		1.40E-02	0.00	0.	A34 BORTNER AND BAURER (1979)
114	CO4- → CO4-	+ O2		3.00E-01	0.00	0.	A35 WONG ET AL (1972)
115	CO4- → CO4-	+ O2		1.50E-10	0.00	0.	A37 FEHSENFELD ET AL (1969B)
116	CO4- → CO4-	+ O3		1.30E-10	0.00	0.	A37 FEHSENFELD AND FERGUSON (1974)
117	CO4- → CO4-	+ NO		4.80E-11	0.00	0.	A37 FEHSENFELD ET AL (1969B)
118	NO2- → NO2	+ E		3.00E-02	0.00	0.	A34 BORTNER AND BAURER (1979)
119	NO2- → NO2	+ O2		1.80E-11	0.00	0.	A40 FEHSENFELD AND FERGUSON (1968)
120	NO3- → NO3	+ O		3.00E-02	0.00	0.	A34 BORTNER AND BAURER (1979)
121	NO3- → NO3	+ O2		1.00E-12	0.00	0.	A37 FEHSENFELD ET AL (1969B)
122	NO3- → NO3	+ NO2		2.00E-11	0.00	0.	A44 GRAHAM AND JOHNSTON (1978)
123	NO3- → NO3	+ HV		2.00E-02	0.00	0.	A34 BORTNER AND BAURER (1979)
124	O- → O3	+ O2		4.40E-10	0.00	0.	A34 BORTNER AND BAURER (1976)
125	O+ (2D) → O2	+ O2		3.00E-10	0.00	0.	A42 STEBBINGS ET AL (1966)
126	O+ (2D) → O2	+ O2		3.00E-10	0.00	0.	A42 STEBBINGS ET AL (1966)
127	O+ → O2	+ CO		1.00E-09	0.00	0.	A43 LINDBERGER ET AL (1974)
128	O → O2	+ M		4.80E-33	-2.00	0.	A44 CAMPBELL AND GRAY (1973)
129	O → O2	+ M		5.50E-34	-2.60	0.	A45 KAUFMAN AND KELSO (1964)
130	O → O2	+ O2		1.20E-11	0.00	-2.00E+03	A46 SCHIFF (1969)
131	O → O2	+ H		7.00E-11	0.00	-5.10E+03	A47 WONG AND POTTER (1965)
132	O → O2	+ H2O2		1.20E-12	0.00	-2.20E+03	A48 DAVIS ET AL (1974A)
133	O → O2	+ H2O2		1.80E-12	0.00	-2.20E+03	A48 DAVIS ET AL (1974A)
134	H → H2O2	+ H2O2		2.30E-12	0.00	-1.40E+03	A49 KLEMM ET AL (1975)
135	H → H2O2	+ H2O2		2.90E-12	0.00	-1.40E+03	A49 KLEMM ET AL (1975)
136	H → O2	+ M		4.40E-33	0.00	5.00E+02	A2 BAULCH ET AL (1972)
137	N → O2	+ NO		5.50E-12	0.00	-3.22E+03	A50 BECKER ET AL (1969)
138	N → O2	+ N2		8.20E-11	0.00	-4.10E+02	A51 CLYNE AND MCDERMID (1975)
139	N → O2	+ M		1.80E-31	-1.50	0.	A52 BAULCH ET AL (1973)
140	OH → O3	+ H2O2		1.30E-12	0.00	-9.50E+02	A53 ANDERSON AND KAUFMAN (1973)
141	OH → H2O2	+ H2O2		1.00E-11	0.00	-7.50E+02	A54 BORTNER AND BAURER (1979)

Table A1. Chemical Reaction Scheme (Contd)

NO.	CHEMICAL REACTION	A	B	C	REFERENCE
142 NO	+ O <sub>3</sub>	1.70E-12	0.00	-1.31E+03 A52	BAULCH ET AL (1973)
143 NO	+ O	1.55E-32	0.00	-5.84E+02 A57	MYTLOCK ET AL (1976)
144 NO <sub>2</sub>	+ NO <sub>2</sub>	7.55E-12	0.00	-5.00E+02 A34	BORTNER AND BAURER (1979)
145 NO <sub>2</sub>	+ O <sub>3</sub>	1.00E-13	0.00	-1.25E+03 A53	GARVIN (1973)
146 NO <sub>2</sub>	+ H	4.80E-10	0.00	-4.00E+02 A52	CLYNE AND MONKHOUSE (1977)
147 CO	+ OH	2.20E-13	6.00	-8.00E+01 A57	DAVIS ET AL (1974B)
148 CO	+ O	6.50E-33	0.00	-2.18E+03 A57	BAULCH ET AL (1976)
149 NO <sub>2</sub>	+ E	3.20E-10	-8.00	0.	BORTNER AND BAURER (1978)
150 NO <sub>2</sub>	+ E	2.00E-07	-1.00	0.	BIONDI (1973)
151 NO <sub>2</sub>	+ E	2.00E-07	-1.00	0.	BIONDI (1973)
152 O <sub>2</sub>	+ E	2.00E-07	-1.00	0.	BIONDI (1973)
153 O <sub>2</sub>	+ E	3.50E-12	-7.70	0.	BORTNER AND BAURER (1979)
154 N <sub>2</sub>	+ E	3.50E-12	-7.70	0.	BORTNER AND BAURER (1979)
155 N <sub>2</sub>	+ E	3.50E-12	-7.70	0.	BORTNER AND BAURER (1979)
156 NO <sub>2</sub>	+ E	3.00E-07	-5.50	0.	BORTNER AND BAURER (1979)
157 NO <sub>2</sub>	+ E	1.50E-06	-2.20	0.	BORTNER AND BAURER (1979)
158 NO <sub>2</sub>	+ E	2.00E-06	-2.20	0.	BORTNER AND BAURER (1979)
159 NO <sub>2</sub>	+ E	3.00E-06	-2.20	0.	BORTNER AND BAURER (1979)
160 O <sub>2</sub>	+ O <sub>2</sub>	1.40E-29	-1.00	-6.00E+02 A54	PHILIPS (1969)
161 O <sub>3</sub>	+ E	9.00E-12	1.50	0.	STELMAN ET AL (1972)
162 O <sub>2</sub>	+ O <sub>2</sub>	3.90E-30	-3.20	0.	PAYZANT ET AL (1973)
163 O <sub>4</sub>	+ O <sub>2</sub>	2.00E-05	-3.20	-5.40E+03 A54	BORTNER AND BAURER (1978)
164 O <sub>4</sub>	+ O <sub>2</sub>	2.00E-05	-3.20	-5.40E+03 A54	BORTNER AND BAURER (1978)
165 NO <sub>2</sub>	+ NO <sub>2</sub>	3.00E-29	-2.00	0.	BORTNER AND BAURER (1979)
166 NO <sub>2</sub>	+ NO <sub>2</sub>	1.50E-28	-2.00	0.	BORTNER AND BAURER (1979)
167 N <sub>2</sub>	+ O <sub>2</sub>	5.00E-11	-8.00	0.	LINDBERGER ET AL (1974)
168 O <sub>2</sub>	+ O <sub>2</sub>	1.20E-12	-5.50	0.	LINDBERGER ET AL (1974)
169 O <sub>2</sub>	+ O <sub>2</sub>	2.00E-11	-4.00	0.	LINDBERGER ET AL (1974)
170 H <sub>3</sub> O <sup>+</sup>	+ H <sub>2</sub> O	3.50E-27	-4.00	0.	GOOD ET AL (1970)
171 H <sub>3</sub> O <sup>+</sup>	+ N <sub>2</sub>	1.40E-30	-2.00	0.	BORTNER AND BAURER (1979)
172 H <sub>3</sub> O <sup>+</sup>	+ H <sub>2</sub> O	2.20E-27	-2.80	0.	BORTNER AND BAURER (1979)
173 H <sub>3</sub> O <sup>+</sup>	+ H <sub>2</sub> O	2.30E-27	-2.80	0.	BORTNER AND BAURER (1979)
174 H <sub>3</sub> O <sup>+</sup>	+ M	2.50E-03	-4.00	-1.00E+04 A54	BORTNER AND BAURER (1978)
175 H <sub>3</sub> O <sup>+</sup>	+ M	1.20E-01	-4.00	-8.80E+03 A54	BORTNER AND BAURER (1978)
176 H <sub>1</sub> O <sub>5</sub> <sup>+</sup>	+ M	4.00E-01	0.00	-7.67E+03 A54	BORTNER AND BAURER (1978)
177 NO <sub>2</sub>	+ H <sub>2</sub> O	1.10E-27	-4.70	0.	HOWARD ET AL (1971)
178 NO <sub>2</sub>	+ H <sub>2</sub> O	1.10E-27	-4.70	0.	HOWARD ET AL (1971)
179 O <sub>2</sub>	+ O <sub>2</sub>	1.10E-30	-1.00	0.	BORTNER AND BAURER (1979)
180 O <sub>2</sub>	+ O <sub>2</sub>	3.50E-31	-1.00	0.	BORTNER AND BAURER (1979)
181 O <sub>2</sub>	+ O <sub>2</sub>	2.00E-29	-1.00	0.	BORTNER AND BAURER (1979)
182 O <sub>3</sub>	+ CO <sub>2</sub>	5.50E-10	-4.49	0.	BORTNER AND BAURER (1979)
183 O <sub>4</sub>	+ M	2.00E-05	-1.00	-6.30E+03 A54	BORTNER AND BAURER (1979)
184 CO <sub>3</sub>	+ NO	1.10E-11	-1.10	0.	BORTNER AND BAURER (1979)
185 O	+ HV	0.	0.00	0.	
186 O <sub>2</sub>	+ HV	0.	0.00	0.	
187 N <sub>2</sub>	+ HV	0.	0.00	0.	
188 NO	+ HV	0.	0.00	0.	

Wave length dependent (See Text)

Table A1. Chemical Reaction Scheme (Contd)

NO.	CHEMICAL REACTION	A	B	C	REFERENCE
189 N	+ HV	0.	0.00	0.	
190 H	= H+	0.	0.00	0.	
191 HE	= HE+	0.	0.00	0.	
192 O2	= O	0.	0.00	0.	
193 O2	= O1D	0.	0.00	0.	
194 O3	= O2	0.	0.00	0.	
195 O3	= O21D	0.	0.00	0.	
196 H2O	= OH	0.	0.00	0.	
197 H2O2	= OH	0.	0.00	0.	
198 H2O2	= O2	0.	0.00	0.	
199 NO	= N	0.	0.00	0.	
200 NO2	= NO	0.	0.00	0.	
201 N2O	= N2	0.	0.00	0.	
202 HNO2	= OH	0.	0.00	0.	
203 CO2	= CO	0.	0.00	0.	
204 CO2	= CO	0.	0.00	0.	
205 NO3	= NO	0.	0.00	0.	
206 O	= O+(2D)	0.	0.00	0.	
207 O21D	= O2+	0.	0.00	0.	
208 E*	= N	+ 2E	0.00	0.	
209 E*	= O	+ 2E	0.00	0.	
210 E*	= O	+ 2E	0.00	0.	
211 E*	= O+(2D)		0.00	0.	
212 E*	= O+(2D)		0.00	0.	
213 E*	= N2+		0.00	0.	
214 E*	= O2+		0.00	0.	
215 E*	= N	+ E	0.00	0.	

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## Appendix B

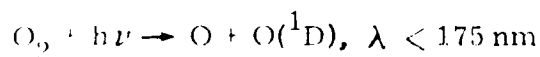
### Photodissociation processes and Their Rate Coefficients

Appendix B contains information on the photodissociation, photoionization, and energetic electron impact reactions. Table B1 lists the solar fluxes in the wavelength region 116.2 to 730.0 nm along with the absorption cross sections for  $O_2$ ,  $O_3$ ,  $H_2O$ ,  $H_2O_2$ ,  $NO_2$ ,  $NO_3$ , and  $N_2O$ . Table B2 contains the absorption cross sections for  $N_2O_5$ ,  $HNO_2$ ,  $HNO_3$ ,  $CH_4$ ,  $CO_2$ ,  $CH_2O$ , and  $HO_2$ .

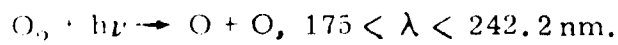
Table B3 lists the photodissociation processes along with their total photodissociation rate coefficient. The units of all the rate coefficients presented in this table and in all the tables that follow (Tables B4-B23) are  $\text{sec}^{-1}$ . The constants in Table B3 were computed from Eq. (52) using the entire unattenuated solar flux. The values listed here are indications of the maximum rate coefficient that each process can attain.

#### B1. MOLECULAR OXYGEN

Two distinct processes for  $O_2$  photodissociation are considered,



and

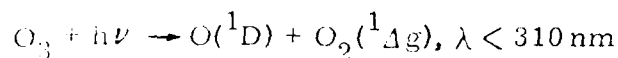




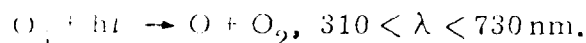
The cross sections for this molecule are taken from the compilation of Ackerman<sup>16</sup> with the exception of those wavelengths in the Schumann Range bands. The photodissociation rate coefficients for the first process above are listed in Table B4, and those for the second process are listed in Table B5. The column densities given in these and all the other tables that follow (Tables B6- B23) are in units of  $\text{cm}^{-2}$  column.

## B2. OZONE

For ozone, two processes are also considered,



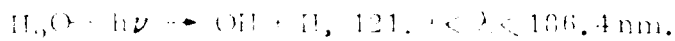
and



The absorption cross sections for ozone are also taken from the compilation of Ackerman.<sup>16</sup> The photodissociation rate coefficients for the process with the excited products are listed in Table B6, and those for the process with the ground state products are listed in Table B7.

## B3. WATER VAPOR

Water vapor is photodissociated primarily through the process

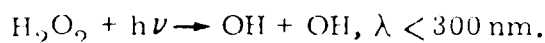


The absorption cross sections for this molecule are taken from Watanabe and Zelikoff.<sup>17</sup> The photodissociation rate coefficients for this process are tabulated in Table B8.

17. Watanabe, K., and Zelikoff, M.J. (1953) Absorption coefficients of water vapor in the vacuum ultraviolet, J. Opt. Soc. Am. 43:753-755.

## B1. HYDROGEN PEROXIDE

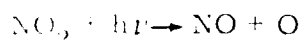
According to Urey et al.<sup>B2</sup> and Holt et al.,<sup>B3</sup> the photodissociation process for hydrogen peroxide is probably



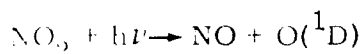
The absorption cross sections above 225 nm are from Urey et al., and those below 225 nm are from Holt et al. The photodissociation rate coefficients for this molecule are presented in Table B9.

## B5. NITROGEN DIOXIDE

The primary quantum yield for nitrogen dioxide is unity for the process



for wavelengths from 308 to 244 nm. The process



has unity primary quantum yield from 244 to 190 nm. For these computations, however, all of the photodissociation of  $\text{NO}_2$  is assumed to take place according to the later process. The absorption cross sections for this molecule are taken from Nakayama et al.<sup>B4</sup> and from Hall and Blacet.<sup>B5</sup> The photodissociation rate coefficients for this process are listed in Table B10.

## B6. THE $\text{NO}_3$ RADICAL

According to Johnston and Graham,<sup>13</sup> the photolysis of  $\text{NO}_3$  can proceed as

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B2. Urey, H.C., Dawsey, L.H., and Rice, F.O. (1929) The absorption spectrum and decomposition of hydrogen peroxide by light, J. Am. Chem. Soc., 51:1371-1383.

B3. Holt, R.B., McLave, C.K., and Oldenberg, O. (1948) Ultraviolet absorption spectrum of hydrogen peroxide, J. Chem. Phys., 16:225-229.

B4. Nakayama, T., Kitamura, M.V., and Watanabe, K. (1959) Ionization potential and absorption coefficients of nitrogen dioxide, J. Chem. Phys., 30:1133-1136.

B5. Hall, T.C., and Blacet, F.E. (1952) Separation of the absorption spectra of  $\text{NO}_2$  and  $\text{N}_2\text{O}_4$  in the range 2400-5000 Å, J. Chem. Phys., 20:1745-1747.

Table B7. Total Photoionization Rate Coefficients for the Process  $O_2 + h\nu \rightarrow O + O(^1D)$  for the Wavelengths Below 1.0  $\mu m$  (Contd)

O3 COLUMN DENSITY

	2.0E+15	5.0E+15	1.0E+16	2.0E+16	5.0E+16	1.0E+17	2.0E+17	5.0E+17	1.0E+18	2.0E+18
1.0E+13	1.66806E-06	1.65171E-06	1.62513E-06	1.57431E-06	1.43824E-06	1.25387E-06	9.88396E-07	5.71980E-07	2.94155E-07	1.02772E-07
2.0E+13	1.66793E-06	1.65158E-06	1.62500E-06	1.57419E-06	1.43814E-06	1.25378E-06	9.88334E-07	5.71953E-07	2.94145E-07	1.02770E-07
5.0E+13	1.66754E-06	1.65119E-06	1.62462E-06	1.57383E-06	1.43783E-06	1.25351E-06	9.88149E-07	5.71873E-07	2.94115E-07	1.02762E-07
1.0E+14	1.66686E-06	1.65055E-06	1.62399E-06	1.57322E-06	1.43728E-06	1.25307E-06	9.87839E-07	5.71740E-07	2.94066E-07	1.02750E-07
2.0E+14	1.66559E-06	1.64926E-06	1.62273E-06	1.57201E-06	1.43621E-06	1.25219E-06	9.87221E-07	5.71474E-07	2.93967E-07	1.02725E-07
5.0E+14	1.66167E-06	1.64540E-06	1.61895E-06	1.56839E-06	1.43302E-06	1.24956E-06	9.85369E-07	5.70676E-07	2.93670E-07	1.02651E-07
1.0E+15	1.65518E-06	1.63899E-06	1.61268E-06	1.56238E-06	1.42771E-06	1.24519E-06	9.82294E-07	5.69351E-07	2.93177E-07	1.02528E-07
2.0E+15	1.64230E-06	1.62629E-06	1.60024E-06	1.55047E-06	1.41718E-06	1.23652E-06	9.76187E-07	5.66715E-07	2.92195E-07	1.02282E-07
5.0E+15	1.60450E-06	1.58897E-06	1.56372E-06	1.51546E-06	1.38623E-06	1.21102E-06	9.58212E-07	5.58929E-07	2.89283E-07	1.01550E-07
1.0E+16	1.54414E-06	1.52939E-06	1.50540E-06	1.45956E-06	1.33677E-06	1.17020E-06	9.29361E-07	5.46341E-07	2.84538E-07	1.00349E-07
2.0E+16	1.43268E-06	1.41934E-06	1.39766E-06	1.35621E-06	1.24522E-06	1.09445E-06	8.75550E-07	5.22546E-07	2.75441E-07	9.80170E-08
5.0E+16	1.16040E-06	1.15043E-06	1.13421E-06	1.10323E-06	1.02023E-06	9.07081E-07	7.40652E-07	4.60789E-07	2.50972E-07	9.15433E-08
1.0E+17	8.54413E-07	8.47991E-07	8.37554E-07	8.17620E-07	7.64191E-07	6.90938E-07	5.80801E-07	3.82530E-07	2.17829E-07	8.22435E-08
2.0E+17	5.36645E-07	5.33460E-07	5.28291E-07	5.18431E-07	4.92011E-07	4.55440E-07	3.98265E-07	2.82798E-07	1.70978E-07	6.78314E-08
5.0E+17	2.54983E-07	2.53852E-07	2.52020E-07	2.48539E-07	2.39264E-07	2.26352E-07	2.05261E-07	1.56698E-07	1.01221E-07	4.28533E-08
1.0E+18	1.36289E-07	1.35699E-07	1.34746E-07	1.32943E-07	1.28181E-07	1.21616E-07	1.10911E-07	8.58955E-08	5.64943E-08	2.44971E-08
2.0E+18	6.00193E-08	5.97393E-08	5.92891E-08	5.84436E-08	5.62472E-08	5.32901E-08	4.85643E-08	3.76423E-08	2.48191E-08	1.08074E-08
5.0E+18	1.13865E-08	1.13204E-08	1.12151E-08	1.10204E-08	1.05331E-08	9.91549E-09	8.98713E-09	6.92906E-09	4.54883E-09	1.96587E-09
1.0E+19	1.66447E-09	1.65246E-09	1.63346E-09	1.59880E-09	1.51493E-09	1.41452E-09	1.27268E-09	9.73832E-10	6.36991E-10	2.74164E-10
2.0E+19	9.58961E-11	9.48877E-11	9.32951E-11	9.04033E-11	8.35107E-11	7.55905E-11	6.54293E-11	4.79128E-11	3.10048E-11	1.33560E-11
5.0E+19	1.95990E-12	1.91295E-12	1.83731E-12	1.69528E-12	1.33423E-12	9.00690E-13	4.20783E-13	5.68626E-14	9.60753E-15	3.42372E-15
1.0E+20	4.57705E-13	4.46221E-13	4.27722E-13	3.93016E-13	3.05030E-13	2.00223E-13	8.67228E-14	7.32785E-15	1.33288E-16	7.01975E-16
2.0E+20	4.61935E-14	4.50798E-14	4.32836E-14	3.99043E-14	3.12770E-14	2.08583E-14	9.30490E-15	6.43112E-16	1.61428E-17	6.38520E-17
5.0E+20	9.31927E-17	9.10317E-17	8.75410E-17	8.09560E-17	6.40283E-17	4.33116E-17	1.98226E-17	1.90290E-18	3.84043E-20	1.57073E-20
1.0E+21	4.18059E-21	4.08390E-21	3.92769E-21	3.63297E-21	2.87498E-21	1.94652E-21	8.92285E-22	8.59497E-23	1.73975E-24	7.12828E-28
2.0E+21	8.61614E-30	8.41687E-30	8.04933E-30	7.48752E-30	5.92534E-30	4.01179E-30	1.83903E-30	1.77149E-31	3.58584E-33	1.46924E-36
5.0E+21	7.54474E-56	7.37024E-56	7.08833E-56	6.53036E-56	5.18853E-56	3.51293E-56	1.61035E-56	1.55121E-57	3.13995E-59	1.28655E-62
1.0E+22	2.80670E-99	2.74178E-99	2.63691E-99	2.43905E-99	1.93017E-99	1.30684E-99	5.99062E-100	5.77062E-101	1.16808E-102	4.78605E-106

O2 COLUMN DENSITY

Table B4. Total Photoionization Rate Coefficients for the Process  $O_2 + h\nu \rightarrow O + O(^1D)$  for the Wavelengths Below 175 nm

	O3 COLUMN DENSITY									
	1.0E+12	2.0E+12	5.0E+12	1.0E+13	2.0E+13	5.0E+13	1.0E+14	2.0E+14	5.0E+14	1.0E+15
1.0E+13	1.67913E-06	1.67912E-06	1.67911E-06	1.67908E-06	1.67902E-06	1.67885E-06	1.67858E-06	1.67802E-06	1.67635E-06	1.67358E-06
2.0E+13	1.67900E-06	1.67899E-06	1.67897E-06	1.67893E-06	1.67889E-06	1.67872E-06	1.67844E-06	1.67789E-06	1.67622E-06	1.67345E-06
5.0E+13	1.67860E-06	1.67859E-06	1.67858E-06	1.67855E-06	1.67849E-06	1.67833E-06	1.67805E-06	1.67749E-06	1.67583E-06	1.67305E-06
1.0E+14	1.67794E-06	1.67793E-06	1.67791E-06	1.67789E-06	1.67783E-06	1.67767E-06	1.67739E-06	1.67683E-06	1.67517E-06	1.67240E-06
2.0E+14	1.67762E-06	1.67760E-06	1.67758E-06	1.67756E-06	1.67752E-06	1.67735E-06	1.67707E-06	1.67652E-06	1.67485E-06	1.67208E-06
5.0E+14	1.67268E-06	1.67267E-06	1.67266E-06	1.67263E-06	1.67257E-06	1.67241E-06	1.67213E-06	1.67158E-06	1.66992E-06	1.66716E-06
1.0E+15	1.66613E-06	1.66613E-06	1.66611E-06	1.66608E-06	1.66603E-06	1.66586E-06	1.66558E-06	1.66503E-06	1.66338E-06	1.66064E-06
2.0E+15	1.65314E-06	1.65314E-06	1.65312E-06	1.65309E-06	1.65304E-06	1.65288E-06	1.65260E-06	1.65206E-06	1.65042E-06	1.64771E-06
5.0E+15	1.61501E-06	1.61501E-06	1.61499E-06	1.61496E-06	1.61491E-06	1.61475E-06	1.61449E-06	1.61396E-06	1.61237E-06	1.60974E-06
1.0E+16	1.55435E-06	1.55435E-06	1.55431E-06	1.55409E-06	1.55404E-06	1.55388E-06	1.55363E-06	1.55313E-06	1.55163E-06	1.54912E-06
2.0E+16	1.44170E-06	1.44170E-06	1.44168E-06	1.44162E-06	1.44162E-06	1.44148E-06	1.44125E-06	1.44080E-06	1.43944E-06	1.43718E-06
5.0E+16	1.16715E-06	1.16715E-06	1.16714E-06	1.16712E-06	1.16709E-06	1.16699E-06	1.16682E-06	1.16648E-06	1.16546E-06	1.16377E-06
1.0E+17	8.58763E-07	8.58761E-07	8.58754E-07	8.58743E-07	8.58721E-07	8.58656E-07	8.58546E-07	8.58327E-07	8.57872E-07	8.56582E-07
2.0E+17	5.38802E-07	5.38800E-07	5.38797E-07	5.38791E-07	5.38781E-07	5.38748E-07	5.38694E-07	5.38585E-07	5.38260E-07	5.37720E-07
5.0E+17	2.55751E-07	2.55751E-07	2.55750E-07	2.55749E-07	2.55744E-07	2.55732E-07	2.55713E-07	2.55674E-07	2.55556E-07	2.55366E-07
1.0E+18	1.35650E-07	1.35650E-07	1.35650E-07	1.35650E-07	1.35650E-07	1.35686E-07	1.36680E-07	1.36670E-07	1.36590E-07	1.36489E-07
2.0E+18	6.02101E-08	6.02098E-08	6.02093E-08	6.02083E-08	6.02055E-08	6.02055E-08	6.02006E-08	6.01910E-08	6.01622E-08	6.01143E-08
5.0E+18	1.14317E-08	1.14317E-08	1.14316E-08	1.14315E-08	1.14313E-08	1.14306E-08	1.14295E-08	1.14272E-08	1.14203E-08	1.14090E-08
1.0E+19	1.67274E-09	1.67273E-09	1.67272E-09	1.67270E-09	1.67266E-09	1.67253E-09	1.67232E-09	1.67190E-09	1.67165E-09	1.66858E-09
2.0E+19	9.65914E-11	9.65911E-11	9.65900E-11	9.65883E-11	9.65847E-11	9.65742E-11	9.65565E-11	9.65213E-11	9.64160E-11	9.62415E-11
5.0E+19	1.99185E-12	1.99183E-12	1.99179E-12	1.99170E-12	1.99154E-12	1.99106E-12	1.99025E-12	1.98864E-12	1.98382E-12	1.97581E-12
1.0E+20	4.65523E-13	4.65519E-13	4.65508E-13	4.65488E-13	4.65446E-13	4.65330E-13	4.65133E-13	4.64739E-13	4.63559E-13	4.61600E-13
2.0E+20	4.69508E-14	4.69504E-14	4.69493E-14	4.69474E-14	4.69436E-14	4.69321E-14	4.69130E-14	4.68749E-14	4.67606E-14	4.65708E-14
5.0E+20	9.46611E-17	9.46603E-17	9.46581E-17	9.46544E-17	9.46470E-17	9.46248E-17	9.45878E-17	9.45139E-17	9.42924E-17	9.39244E-17
1.0E+21	4.24629E-21	4.24626E-21	4.24616E-21	4.24599E-21	4.24566E-21	4.24467E-21	4.24301E-21	4.23971E-21	4.22980E-21	4.21333E-21
2.0E+21	8.75154E-30	8.75147E-30	8.75127E-30	8.75093E-30	8.75024E-30	8.74820E-30	8.74479E-30	8.73797E-30	8.71754E-30	8.68361E-30
5.0E+21	7.66330E-56	7.66324E-56	7.66306E-56	7.66276E-56	7.66216E-56	7.66037E-56	7.65738E-56	7.65141E-56	7.63535E-56	7.60381E-56
1.0E+22	2.85080E-99	2.85078E-99	2.85072E-99	2.85060E-99	2.85038E-99	2.84972E-99	2.84860E-99	2.84638E-99	2.83973E-99	2.82868E-99

Table B3. Total Photodissociation Rate  
Coefficients for Unattenuated Solar Flux

$O_2 + HV = O + O^1D$	1.67927E-06 SEC-1
$O_2 + HV = O + O$	8.36798E-08 SEC-1
$O_3 + HV = O^1D + O^2^1D$	9.72665E-03 SEC-1
$O_3 + HV = O + O_2$	4.17996E-04 SEC-1
$H_2O + HV = OH + H$	7.39662E-06 SEC-1
$H_2O_2 + HV = OH + OH$	1.59387E-04 SEC-1
$NO_2 + HV = NO + O^1D$	1.51039E-02 SEC-1
$NO_3 + HV = NO + O_2$	7.04137E-02 SEC-1
$N_2O + HV = N_2 + O^1D$	7.76688E-07 SEC-1
$N_2O_5 + HV = NO_2 + NO_2$	6.92337E-04 SEC-1
$HNO_2 + HV = OH + NO$	5.84756E-04 SEC-1
$HNO_3 + HV = OH + NO_2$	1.16540E-04 SEC-1
$CH_4 + HV = CH_3 + H$	9.08606E-06 SEC-1
$CO_2 + HV = CO + O^1D$	8.84043E-08 SEC-1
$CO_2 + HV = CO + O$	8.24894E-09 SEC-1
$CH_2O + HV = CHO + H$	2.58902E-04 SEC-1
$HO_2 + HV = O_2 + H$	1.13657E-03 SEC-1

Table B2. Absorption Cross Sections for  $N_2O_5$ ,  $HNO_2$ ,  $HNO_3$ ,  $CH_4$ ,  $CO_2$ ,  $CH_2O$ , and  $HO_2$  (Contd)

WAVELENGTH BAND ANGSTROMS	CROSS SECTIONS (CM <sup>2</sup> )						
	N2O5	HNO2	HNO3	CH4	CO2	CH2O	HO2
3200.00-3250.00	6.00E-21	2.00E-20	1.00E-22	0.	0.	2.20E-20	0.
3250.00-3300.00	5.00E-21	2.00E-20	0.	0.	0.	3.40E-20	0.
3300.00-3350.00	3.40E-21	3.00E-20	0.	0.	0.	1.50E-20	0.
3350.00-3400.00	3.00E-21	2.80E-20	0.	0.	0.	1.20E-20	0.
3400.00-3450.00	2.40E-21	3.10E-20	0.	0.	0.	2.00E-20	0.
3450.00-3500.00	2.00E-21	3.00E-20	0.	0.	0.	5.00E-21	0.
3500.00-3550.00	1.50E-21	5.00E-20	0.	0.	0.	2.80E-21	0.
3550.00-3600.00	1.20E-21	5.00E-20	0.	0.	0.	1.20E-21	0.
3600.00-3650.00	9.00E-22	2.90E-20	0.	0.	0.	0.	0.
3650.00-3700.00	7.00E-22	8.00E-20	0.	0.	0.	0.	0.
3700.00-3750.00	4.00E-22	4.00E-20	0.	0.	0.	0.	0.
3750.00-3800.00	2.50E-22	2.00E-20	0.	0.	0.	0.	0.
3800.00-3850.00	0.	4.00E-20	0.	0.	0.	0.	0.
3850.00-3900.00	0.	5.00E-20	0.	0.	0.	0.	0.
3900.00-3950.00	0.	0.	0.	0.	0.	0.	0.
3950.00-4000.00	0.	0.	0.	0.	0.	0.	0.
4000.00-4050.00	0.	0.	0.	0.	0.	0.	0.
4050.00-4100.00	0.	0.	0.	0.	0.	0.	0.
4100.00-4150.00	0.	0.	0.	0.	0.	0.	0.
4150.00-4200.00	0.	0.	0.	0.	0.	0.	0.
4200.00-4250.00	0.	0.	0.	0.	0.	0.	0.
4250.00-4300.00	0.	0.	0.	0.	0.	0.	0.
4300.00-4350.00	0.	0.	0.	0.	0.	0.	0.
4350.00-4400.00	0.	0.	0.	0.	0.	0.	0.
4400.00-4450.00	0.	0.	0.	0.	0.	0.	0.
4450.00-4500.00	0.	0.	0.	0.	0.	0.	0.
4500.00-4550.00	0.	0.	0.	0.	0.	0.	0.
4550.00-4600.00	0.	0.	0.	0.	0.	0.	0.
4600.00-4650.00	0.	0.	0.	0.	0.	0.	0.
4650.00-4700.00	0.	0.	0.	0.	0.	0.	0.
4700.00-4750.00	0.	0.	0.	0.	0.	0.	0.
4750.00-4800.00	0.	0.	0.	0.	0.	0.	0.
4800.00-4850.00	0.	0.	0.	0.	0.	0.	0.
4850.00-4900.00	0.	0.	0.	0.	0.	0.	0.
4900.00-4950.00	0.	0.	0.	0.	0.	0.	0.
4950.00-5000.00	0.	0.	0.	0.	0.	0.	0.
5000.00-5050.00	0.	0.	0.	0.	0.	0.	0.
5050.00-5100.00	0.	0.	0.	0.	0.	0.	0.
5100.00-5150.00	0.	0.	0.	0.	0.	0.	0.
5150.00-5200.00	0.	0.	0.	0.	0.	0.	0.
5200.00-5250.00	0.	0.	0.	0.	0.	0.	0.
5250.00-5300.00	0.	0.	0.	0.	0.	0.	0.
5300.00-5350.00	0.	0.	0.	0.	0.	0.	0.
5350.00-5400.00	0.	0.	0.	0.	0.	0.	0.
5400.00-5450.00	0.	0.	0.	0.	0.	0.	0.
5450.00-5500.00	0.	0.	0.	0.	0.	0.	0.
5500.00-5550.00	0.	0.	0.	0.	0.	0.	0.
5550.00-5600.00	0.	0.	0.	0.	0.	0.	0.
5600.00-5650.00	0.	0.	0.	0.	0.	0.	0.
5650.00-5700.00	0.	0.	0.	0.	0.	0.	0.

Table B2. Absorption Cross Sections for  $N_2O_5$ ,  $HNO_2$ ,  $HNO_3$ ,  $CH_4$ ,  $CO_2$ ,  $CH_2O$ , and  $HO_2$  (Contd)

WAVELENGTH BAND ANGSTROMS	CROSS SECTIONS (CM2)						HO2
	N2O5	HNO2	HNO3	CH4	CO2	CH2O	
1792.60-1803.60	0.	0.	0.	0.	1.30E-21	0.	5.50E-18
1803.60-1816.40	0.	0.	0.	0.	1.00E-21	0.	5.50E-18
1816.40-1830.60	0.	0.	0.	0.	6.00E-22	0.	5.50E-18
1830.60-1846.20	0.	0.	0.	0.	4.00E-22	0.	5.50E-18
1846.20-1863.40	0.	0.	0.	0.	3.00E-22	0.	5.60E-18
1863.40-1882.20	0.	0.	0.	0.	1.50E-22	0.	5.70E-18
1882.20-1902.40	0.	0.	0.	0.	8.00E-23	0.	5.80E-18
1902.40-1924.00	0.	0.	0.	0.	3.00E-23	0.	5.80E-18
1924.00-1947.00	0.	0.	0.	0.	2.00E-23	0.	5.80E-18
1947.00-1971.80	0.	0.	0.	0.	1.00E-23	0.	5.80E-18
1971.80-1985.00	0.	0.	8.00E-18	0.	8.00E-24	0.	5.80E-18
1985.00-2000.00	0.	0.	7.00E-18	0.	5.50E-24	0.	5.90E-18
2000.00-2025.00	0.	0.	5.00E-18	0.	4.00E-24	0.	5.90E-18
2025.00-2050.00	0.	0.	3.80E-18	0.	3.20E-24	0.	5.90E-18
2050.00-2061.86	0.	0.	3.00E-18	0.	3.00E-24	0.	5.90E-18
2061.86-2083.33	0.	0.	2.40E-18	0.	3.00E-24	0.	6.00E-18
2083.33-2105.26	0.	0.	1.70E-18	0.	2.80E-24	0.	6.00E-18
2105.26-2127.66	5.00E-18	0.	6.00E-19	0.	2.40E-24	0.	6.00E-18
2127.66-2150.54	4.00E-18	0.	4.60E-19	0.	2.00E-24	0.	6.00E-18
2150.54-2173.91	3.30E-18	0.	3.40E-19	0.	0.	0.	5.80E-18
2173.91-2197.80	2.80E-18	0.	2.40E-19	0.	0.	0.	5.50E-18
2197.80-2222.22	2.20E-18	0.	1.50E-19	0.	0.	0.	5.00E-18
2222.22-2247.19	2.00E-18	0.	1.10E-19	0.	0.	0.	4.50E-18
2247.19-2272.73	1.50E-18	0.	9.00E-20	0.	0.	0.	4.00E-18
2272.73-2298.85	1.10E-18	0.	8.00E-20	0.	0.	0.	3.70E-18
2298.85-2325.58	1.00E-18	0.	5.50E-20	0.	0.	0.	3.00E-18
2325.58-2352.94	9.00E-19	0.	4.50E-20	0.	0.	0.	2.70E-18
2352.94-2380.95	8.00E-19	0.	3.80E-20	0.	0.	0.	2.30E-18
2380.95-2409.64	7.00E-19	0.	3.00E-20	0.	0.	0.	2.10E-18
2409.64-2439.02	6.00E-19	0.	2.80E-20	0.	0.	3.50E-21	1.70E-18
2439.02-2469.14	5.00E-19	0.	2.10E-20	0.	0.	3.80E-21	1.20E-18
2469.14-2500.00	4.00E-19	0.	2.00E-20	0.	0.	4.00E-21	1.00E-18
2500.00-2531.65	3.80E-19	0.	2.00E-20	0.	0.	6.00E-21	5.00E-19
2531.65-2564.10	3.20E-19	0.	2.00E-20	0.	0.	7.00E-21	3.80E-19
2564.10-2597.40	3.00E-19	0.	2.00E-20	0.	0.	8.00E-21	2.60E-19
2597.40-2631.58	2.40E-19	0.	2.00E-20	0.	0.	9.00E-21	1.10E-19
2631.58-2666.67	2.10E-19	0.	2.00E-20	0.	0.	1.00E-20	8.00E-20
2666.67-2702.70	1.80E-19	0.	2.00E-20	0.	0.	1.20E-20	5.00E-20
2702.70-2739.73	1.50E-19	0.	1.80E-20	0.	0.	1.50E-20	2.20E-20
2739.73-2777.78	1.30E-19	0.	1.60E-20	0.	0.	1.70E-20	0.
2777.78-2816.90	1.00E-19	0.	1.20E-20	0.	0.	1.90E-20	0.
2816.90-2857.14	8.00E-20	0.	1.10E-20	0.	0.	2.10E-20	0.
2857.14-2898.55	6.00E-20	0.	9.00E-21	0.	0.	2.50E-20	0.
2898.55-2941.18	4.00E-20	0.	6.50E-21	0.	0.	3.00E-20	0.
2941.18-2985.07	3.30E-20	0.	5.00E-21	0.	0.	3.80E-20	0.
2985.07-3030.30	2.80E-20	7.00E-21	3.20E-21	0.	0.	3.00E-20	0.
3030.30-3076.92	2.10E-20	7.50E-21	2.30E-21	0.	0.	4.00E-20	0.
3076.92-3100.00	1.90E-20	9.00E-21	1.80E-21	0.	0.	3.50E-20	0.
3100.00-3150.00	1.10E-20	1.00E-20	7.00E-22	0.	0.	4.50E-20	0.
3150.00-3200.00	9.00E-21	1.10E-20	3.90E-22	0.	0.	3.00E-20	0.

Table B2. Absorption Cross Sections for  $N_2O_5$ ,  $HNO_2$ ,  $HNO_3$ ,  $CH_4$ ,  $CO_2$ ,  $CH_2O$ , and  $HO_2$

WAVELENGTH BAND ANGSTROMS	CROSS SECTIONS (CM <sup>2</sup> )					
	$N_2O_5$	$HNO_2$	$HNO_3$	$CH_4$	$CO_2$	$CH_2O$ $HO_2$
1215.67-1215.67 0.	0.	0.	0.	2.80E-17	7.30E-20	9.00E-18 0.
1162.79-1169.59 0.	0.	0.	0.	2.80E-17	1.10E-19	0. 0.
1169.59-1176.47 0.	0.	0.	0.	2.80E-17	8.80E-20	0. 0.
1176.47-1183.43 0.	0.	0.	0.	2.80E-17	6.00E-20	0. 0.
1183.43-1190.48 0.	0.	0.	0.	2.80E-17	4.70E-20	0. 0.
1190.48-1197.60 0.	0.	0.	0.	2.80E-17	3.80E-20	0. 0.
1197.60-1204.82 0.	0.	0.	0.	2.80E-17	4.00E-20	0. 0.
1204.82-1212.12 0.	0.	0.	0.	2.80E-17	6.10E-20	0. 0.
1212.12-1219.51 0.	0.	0.	0.	2.80E-17	7.40E-20	0. 0.
1219.51-1226.99 0.	0.	0.	0.	2.80E-17	1.00E-19	0. 0.
1226.99-1234.57 0.	0.	0.	0.	2.80E-17	1.20E-19	0. 0.
1234.57-1242.00 0.	0.	0.	0.	2.80E-17	1.60E-19	0. 0.
1242.24-1250.24 0.	0.	0.	0.	2.80E-17	1.80E-19	0. 0.
1250.00-1257.86 0.	0.	0.	0.	2.80E-17	2.10E-19	0. 0.
1257.86-1265.82 0.	0.	0.	0.	2.80E-17	2.80E-19	0. 0.
1265.82-1273.89 0.	0.	0.	0.	2.80E-17	3.30E-19	0. 0.
1273.89-1282.05 0.	0.	0.	0.	2.80E-17	4.20E-19	0. 0.
1282.05-1290.32 0.	0.	0.	0.	2.80E-17	5.90E-19	0. 0.
1290.32-1298.70 0.	0.	0.	0.	2.80E-17	7.00E-19	0. 0.
1298.70-1307.19 0.	0.	0.	0.	2.47E-17	8.00E-19	0. 0.
1307.19-1315.79 0.	0.	0.	0.	2.24E-17	8.30E-19	0. 0.
1315.79-1324.50 0.	0.	0.	0.	2.07E-17	8.50E-19	0. 0.
1324.50-1333.33 0.	0.	0.	0.	1.57E-17	8.70E-19	0. 0.
1333.33-1342.28 0.	0.	0.	0.	1.33E-17	8.70E-19	0. 0.
1342.28-1351.35 0.	0.	0.	0.	1.20E-17	8.70E-19	0. 0.
1351.35-1360.54 0.	0.	0.	0.	1.00E-17	8.60E-19	0. 0.
1360.54-1369.86 0.	0.	0.	0.	8.40E-18	8.10E-19	0. 0.
1369.86-1379.31 0.	0.	0.	0.	5.90E-18	7.20E-19	0. 0.
1379.31-1388.89 0.	0.	0.	0.	3.93E-18	6.40E-19	0. 0.
1388.89-1408.45 0.	0.	0.	0.	2.24E-18	6.00E-19	0. 0.
1408.45-1428.57 0.	0.	0.	0.	6.72E-19	5.70E-19	1.00E-17 0.
1428.57-1449.28 0.	0.	0.	0.	6.72E-20	5.50E-19	7.00E-18 0.
1449.28-1470.59 0.	0.	0.	0.	1.68E-20	5.70E-19	4.00E-18 0.
1470.59-1492.54 0.	0.	0.	0.	1.12E-20	5.70E-19	5.50E-18 0.
1492.54-1515.15 0.	0.	0.	0.	9.00E-21	5.00E-19	1.20E-17 0.
1515.15-1538.46 0.	0.	0.	0.	5.60E-21	4.00E-19	1.80E-17 0.
1538.46-1562.50 0.	0.	0.	0.	4.48E-21	3.00E-19	9.00E-18 0.
1562.50-1587.30 0.	0.	0.	0.	2.80E-21	2.50E-19	8.00E-19 0.
1587.30-1612.90 0.	0.	0.	0.	1.12E-21	1.60E-19	0. 0.
1612.90-1639.34 0.	0.	0.	0.	8.00E-22	1.00E-19	0. 0.
1639.34-1666.67 0.	0.	0.	0.	0.	7.00E-20	0. 0.
1666.67-1694.92 0.	0.	0.	0.	0.	4.00E-20	1.50E-18 0.
1694.92-1724.14 0.	0.	0.	0.	0.	1.50E-20	1.20E-17 0.
1724.14-1739.13 0.	0.	0.	0.	0.	1.00E-20	6.00E-18 0.
1739.13-1750.00 0.	0.	0.	0.	0.	8.00E-21	1.80E-18 0.
1750.00-1763.20 0.	0.	0.	0.	0.	5.00E-21	0. 0.
1763.20-1768.60 0.	0.	0.	0.	0.	3.50E-21	0. 0.
1768.60-1774.60 0.	0.	0.	0.	0.	3.00E-21	0. 0.
1774.60-1782.60 0.	0.	0.	0.	0.	2.00E-21	0. 0.
1782.60-1792.60 0.	0.	0.	0.	0.	1.50E-21	0. 0.



Table B1. Solar Fluxes and Absorption Cross Sections for O<sub>2</sub>, O<sub>3</sub>, H<sub>2</sub>O, H<sub>2</sub>O<sub>2</sub>, NO<sub>2</sub>, NO<sub>3</sub>, and N<sub>2</sub>O (Contd)

WAVELENGTH BAND ANGSTROMS	FLUX PH/CM <sup>2</sup> /S/A	CROSS SECTIONS (CM <sup>2</sup> )					
		O <sub>2</sub>	O <sub>3</sub>	H <sub>2</sub> O	H <sub>2</sub> O <sub>2</sub>	NO <sub>2</sub>	NO <sub>3</sub> N <sub>2</sub> O
5700.00-5750.00	5.38E+13 0.		4.75E-21 0.	0.	0.		6.00E-19 0.
5750.00-5800.00	5.42E+13 0.		4.55E-21 0.	0.	0.		7.00E-19 0.
5800.00-5850.00	5.42E+13 0.		4.35E-21 0.	0.	0.		7.00E-19 0.
5850.00-5900.00	5.42E+13 0.		4.42E-21 0.	0.	0.		9.00E-19 0.
5900.00-5950.00	5.44E+13 0.		4.61E-21 0.	0.	0.		1.00E-18 0.
5950.00-6000.00	5.44E+13 0.		4.89E-21 0.	0.	0.		9.00E-19 0.
6000.00-6050.00	5.42E+13 0.		4.84E-21 0.	0.	0.		8.00E-19 0.
6050.00-6100.00	5.40E+13 0.		4.54E-21 0.	0.	0.		7.00E-19 0.
6100.00-6150.00	5.40E+13 0.		4.24E-21 0.	0.	0.		5.00E-19 0.
6150.00-6200.00	5.40E+13 0.		3.90E-21 0.	0.	0.		4.00E-19 0.
6200.00-6250.00	5.38E+13 0.		3.60E-21 0.	0.	0.		2.00E-18 0.
6250.00-6300.00	5.36E+13 0.		3.43E-21 0.	0.	0.		1.80E-18 0.
6300.00-6350.00	5.34E+13 0.		3.17E-21 0.	0.	0.		6.00E-19 0.
6350.00-6400.00	5.32E+13 0.		2.74E-21 0.	0.	0.		4.00E-19 0.
6400.00-6450.00	5.30E+13 0.		2.61E-21 0.	0.	0.		2.20E-19 0.
6450.00-6500.00	7.90E+13 0.		2.40E-21 0.	0.	0.		2.00E-19 0.
6500.00-6600.00	5.22E+13 0.		2.07E-21 0.	0.	0.		3.00E-19 0.
6600.00-6700.00	5.18E+13 0.		1.72E-21 0.	0.	0.		2.00E-18 0.
6700.00-6800.00	5.14E+13 0.		1.37E-21 0.	0.	0.		2.00E-19 0.
6800.00-6900.00	5.09E+13 0.		1.11E-21 0.	0.	0.		0. 0.
6900.00-7000.00	5.04E+13 0.		9.13E-22 0.	0.	0.		0. 0.
7000.00-7100.00	4.99E+13 0.		7.93E-22 0.	0.	0.		0. 0.
7100.00-7200.00	4.94E+13 0.		6.40E-22 0.	0.	0.		0. 0.
7200.00-7300.00	4.90E+13 0.		5.14E-22 0.	0.	0.		0. 0.

Table B1. Solar Fluxes and Absorption Cross Sections for O<sub>2</sub>, O<sub>3</sub>, H<sub>2</sub>O, H<sub>2</sub>O<sub>2</sub>, NO<sub>2</sub>, NO<sub>3</sub>, and N<sub>2</sub>O (Contd)

WAVELENGTH BAND ANGSTROMS	FLUX PH/CM <sup>2</sup> /S, Å	CROSS SECTIONS (CM <sup>2</sup> )				
		O <sub>2</sub>	O <sub>3</sub>	H <sub>2</sub> O	H <sub>2</sub> O <sub>2</sub>	NO <sub>2</sub>
3200.00-3250.00	1.62E+13 0.		1.50E-20 0.	0.	2.94E-19 0.	0.
3250.00-3300.00	1.94E+13 0.		7.78E-21 0.	0.	3.38E-19 0.	0.
3300.00-3350.00	1.79E+13 0.		3.72E-21 0.	0.	3.61E-19 0.	0.
3350.00-3400.00	1.89E+13 0.		1.71E-21 0.	0.	4.17E-19 0.	0.
3400.00-3450.00	2.02E+13 0.		7.46E-22 0.	0.	4.30E-19 0.	0.
3450.00-3500.00	2.06E+13 0.		2.66E-22 0.	0.	4.48E-19 0.	0.
3500.00-3550.00	2.06E+13 0.		1.09E-22 0.	0.	5.53E-19 0.	0.
3550.00-3600.00	2.08E+13 0.		5.49E-23 0.	0.	4.96E-19 0.	0.
3600.00-3650.00	2.36E+13 0.		0.	0.	5.84E-19 0.	0.
3650.00-3700.00	2.46E+13 0.		0.	0.	5.70E-19 0.	0.
3700.00-3750.00	2.48E+13 0.		0.	0.	5.74E-19 0.	0.
3750.00-3800.00	2.34E+13 0.		0.	0.	6.52E-19 0.	0.
3800.00-3850.00	2.22E+13 0.		0.	0.	6.45E-19 0.	0.
3850.00-3900.00	2.18E+13 0.		0.	0.	6.51E-19 0.	0.
3900.00-3950.00	2.38E+13 0.		0.	0.	6.08E-19 0.	0.
3950.00-4000.00	3.08E+13 0.		0.	0.	6.68E-19 0.	0.
4000.00-4050.00	3.80E+13 0.		0.	0.	6.52E-19 0.	0.
4050.00-4100.00	3.98E+13 0.		2.91E-23 0.	0.	6.59E-19 0.	0.
4100.00-4150.00	3.98E+13 0.		3.14E-23 0.	0.	6.03E-19 0.	0.
4150.00-4200.00	4.04E+13 0.		3.99E-23 0.	0.	6.24E-19 0.	0.
4200.00-4250.00	4.02E+13 0.		6.54E-23 0.	0.	0.	0.
4250.00-4300.00	3.88E+13 0.		6.83E-23 0.	0.	0.	0.
4300.00-4350.00	3.96E+13 0.		8.66E-23 0.	0.	0.	0.
4350.00-4400.00	4.50E+13 0.		1.25E-22 0.	0.	0.	0.
4400.00-4450.00	4.78E+13 0.		1.49E-22 0.	0.	0.	0.
4450.00-4500.00	4.96E+13 0.		1.71E-22 0.	0.	0.	0.
4500.00-4550.00	4.98E+13 0.		2.12E-22 0.	0.	0.	6.00E-20 0.
4550.00-4600.00	4.96E+13 0.		3.57E-22 0.	0.	0.	1.00E-19 0.
4600.00-4650.00	5.00E+13 0.		3.68E-22 0.	0.	0.	8.00E-20 0.
4650.00-4700.00	5.10E+13 0.		4.06E-22 0.	0.	0.	1.20E-19 0.
4700.00-4750.00	5.22E+13 0.		4.89E-22 0.	0.	0.	1.80E-19 0.
4750.00-4800.00	5.18E+13 0.		7.11E-22 0.	0.	0.	2.40E-19 0.
4800.00-4850.00	4.92E+13 0.		8.43E-22 0.	0.	0.	2.10E-19 0.
4850.00-4900.00	4.88E+13 0.		8.28E-22 0.	0.	0.	2.40E-19 0.
4900.00-4950.00	5.06E+13 0.		9.09E-22 0.	0.	0.	2.40E-19 0.
4950.00-5000.00	4.96E+13 0.		1.22E-21 0.	0.	0.	3.00E-19 0.
5000.00-5050.00	4.98E+13 0.		1.62E-21 0.	0.	0.	3.00E-19 0.
5050.00-5100.00	5.00E+13 0.		1.58E-21 0.	0.	0.	4.00E-19 0.
5100.00-5150.00	4.86E+13 0.		1.60E-21 0.	0.	0.	4.50E-19 0.
5150.00-5200.00	4.86E+13 0.		1.78E-21 0.	0.	0.	5.00E-19 0.
5200.00-5250.00	5.04E+13 0.		2.07E-21 0.	0.	0.	5.00E-19 0.
5250.00-5300.00	5.16E+13 0.		2.55E-21 0.	0.	0.	6.00E-19 0.
5300.00-5350.00	5.28E+13 0.		2.74E-21 0.	0.	0.	6.00E-19 0.
5350.00-5400.00	5.34E+13 0.		2.88E-21 0.	0.	0.	5.00E-19 0.
5400.00-5450.00	5.40E+13 0.		3.07E-21 0.	0.	0.	4.00E-19 0.
5450.00-5500.00	5.36E+13 0.		3.17E-21 0.	0.	0.	6.00E-19 0.
5500.00-5550.00	5.32E+13 0.		3.36E-21 0.	0.	0.	6.50E-19 0.
5550.00-5600.00	5.32E+13 0.		3.88E-21 0.	0.	0.	7.00E-19 0.
5600.00-5650.00	5.34E+13 0.		4.31E-21 0.	0.	0.	6.00E-19 0.
5650.00-5700.00	5.34E+13 0.		4.67E-21 0.	0.	0.	6.00E-19 0.

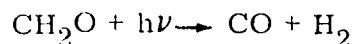
Table B1. Solar Fluxes and Absorption Cross Sections for O<sub>2</sub>, O<sub>3</sub>, H<sub>2</sub>O, H<sub>2</sub>O<sub>2</sub>, NO<sub>2</sub>, NO<sub>3</sub>, and N<sub>2</sub>O (Contd)

WAVELENGTH BAND ANGSTROMS	FLUX PH/CM2/S/A	CROSS SECTIONS (CM2)						
		O2	O3	H2O	H2O2	NO2	NO3	N2O
1792.60-1803.60	1.01E+10 0.		7.77E-19	1.02E-18 0.	0.	0.	0.	0.
1803.60-1816.40	1.27E+10 0.		7.60E-19	6.98E-19 0.	0.	0.	0.	0.
1816.40-1830.60	1.42E+10 0.		7.33E-19	3.64E-19 0.	0.	0.	0.	0.
1830.60-1846.20	1.29E+10 0.		6.99E-19	1.80E-19 0.	0.	0.	0.	0.
1846.20-1863.40	1.31E+10 0.		6.56E-19	6.51E-20 0.	0.	0.	0.	0.
1863.40-1882.20	1.63E+10 0.		6.06E-19 0.	0.	0.	0.	0.	0.
1882.20-1902.40	1.92E+10 0.		5.45E-19 0.	9.79E-19 0.	0.	0.	0.	0.
1902.40-1924.00	2.29E+10 0.		4.86E-19 0.	8.10E-19	5.25E-19 0.	0.	1.26E-19	
1924.00-1947.00	3.61E+10 0.		4.36E-19 0.	7.03E-19	4.83E-19 0.	0.	9.00E-20	
1947.00-1971.80	4.68E+10 0.		4.01E-19 0.	6.15E-19	4.00E-19 0.	0.	8.00E-20	
1971.80-1985.00	6.21E+10 0.		3.42E-19 0.	5.64E-19	3.50E-19 0.	0.	7.00E-20	
1985.00-2000.00	6.85E+10 0.		3.28E-19 0.	5.43E-19	3.30E-19 0.	0.	5.50E-20	
2000.00-2025.00	7.33E+10 0.		3.26E-19 0.	5.16E-19	3.50E-19 0.	0.	4.00E-20	
2025.00-2050.00	8.74E+10 0.		3.28E-19 0.	4.79E-19	4.00E-19 0.	0.	2.50E-20	
2050.00-2061.86	1.10E+11 1.05E-23		3.51E-19 0.	4.66E-19	4.20E-19 0.	0.	2.00E-20	
2061.86-2083.33	1.96E+11 1.00E-23		4.11E-19 0.	4.42E-19	4.30E-19 0.	0.	1.70E-20	
2083.33-2105.26	3.33E+11 9.55E-24		4.84E-19 0.	4.22E-19	4.40E-19 0.	0.	1.10E-20	
2105.26-2127.66	4.21E+11 8.93E-24		6.26E-19 0.	3.92E-19	4.54E-19 0.	0.	4.00E-21	
2127.66-2150.54	4.63E+11 8.28E-24		8.57E-19 0.	3.63E-19	4.58E-19 0.	0.	2.00E-21	
2150.54-2173.91	5.73E+11 7.60E-24		1.17E-18 0.	3.40E-19	4.62E-19 0.	0.	1.10E-21	
2173.91-2197.80	5.53E+11 6.92E-24		1.52E-18 0.	3.19E-19	4.50E-19 0.	0.	1.00E-21	
2197.80-2222.22	7.08E+11 6.28E-24		1.97E-18 0.	2.98E-19	4.25E-19 0.	0.	4.00E-22	
2222.22-2247.19	7.21E+11 5.65E-24		2.55E-18 0.	2.67E-19	4.00E-19 0.	0.	2.80E-22	
2247.19-2272.73	7.13E+11 5.03E-24		3.24E-18 0.	2.49E-19	3.50E-19 0.	0.	2.00E-22	
2272.73-2298.85	8.65E+11 4.40E-24		4.00E-18 0.	2.36E-19	3.00E-19 0.	0.	1.20E-22	
2298.85-2325.58	8.98E+11 3.76E-24		4.83E-18 0.	2.16E-19	2.50E-19 0.	0.	7.00E-23	
2325.58-2352.94	8.22E+11 3.09E-24		5.79E-18 0.	1.99E-19	2.00E-19 0.	0.	5.00E-23	
2352.94-2380.95	7.89E+11 2.44E-24		6.86E-18 0.	1.81E-19	1.18E-19 0.	0.	3.00E-23	
2380.95-2409.64	8.09E+11 1.75E-24		7.97E-18 0.	1.66E-19	1.00E-19 0.	0.	2.00E-23	
2409.64-2439.02	8.51E+11 6.74E-25		9.00E-18 0.	1.48E-19	7.00E-20 0.	0.	1.10E-23	
2439.02-2469.14	9.07E+11 0.		1.00E-17 0.	1.30E-19	5.00E-20 0.	0.	9.00E-24	
2469.14-2500.00	9.33E+11 0.		1.07E-17 0.	1.22E-19	3.60E-20 0.	0.	8.00E-24	
2500.00-2531.65	9.54E+11 0.		1.11E-17 0.	1.08E-19	2.50E-20 0.	0.	7.00E-24	
2531.65-2564.10	1.22E+12 0.		1.12E-17 0.	9.30E-20	1.50E-20 0.	0.	6.00E-24	
2564.10-2597.40	2.14E+12 0.		1.11E-17 0.	8.43E-20	1.70E-20 0.	0.	5.00E-24	
2597.40-2631.58	1.28E+12 0.		1.03E-17 0.	7.49E-20	1.90E-20 0.	0.	5.00E-24	
2631.58-2666.67	3.19E+12 0.		9.43E-18 0.	6.39E-20	2.10E-20 0.	0.	5.00E-24	
2666.67-2702.70	3.47E+12 0.		8.23E-18 0.	5.64E-20	2.90E-20 0.	0.	5.00E-24	
2702.70-2739.73	3.13E+12 0.		6.81E-18 0.	5.00E-20	3.70E-20 0.	0.	5.20E-24	
2739.73-2777.78	3.13E+12 0.		5.31E-18 0.	4.33E-20	4.20E-20 0.	0.	5.90E-24	
2777.78-2816.90	3.53E+12 0.		3.99E-18 0.	3.62E-20	5.00E-20 0.	0.	6.00E-24	
2816.90-2857.14	4.22E+12 0.		2.84E-18 0.	3.27E-20	6.50E-20 0.	0.	5.40E-24	
2857.14-2898.55	5.94E+12 0.		1.92E-18 0.	2.91E-20	8.00E-20 0.	0.	5.20E-24	
2898.55-2941.18	9.15E+12 0.		1.14E-18 0.	2.53E-20	9.00E-20 0.	0.	5.00E-24	
2941.18-2985.07	9.09E+12 0.		6.60E-19 0.	2.15E-20	1.20E-19 0.	0.	5.10E-24	
2985.07-3030.30	6.53E+12 0.		3.63E-19 0.	1.75E-20	1.33E-19 0.	0.	5.00E-24	
3030.30-3076.92	1.09E+13 0.		1.97E-19 0.	0.	1.65E-19 0.	0.	4.20E-24	
3076.92-3110.00	2.57E+13 0.		1.05E-19 0.	0.	1.97E-19 0.	0.	3.40E-24	
3110.00-3140.00	1.21E+13 0.		5.23E-20 0.	0.	2.24E-19 0.	0.	1.70E-24	
3140.00-3200.00	1.39E+13 0.		2.91E-20 0.	0.	2.61E-19 0.	0.	0.	

Table B1. Solar Fluxes and Absorption Cross Sections for O<sub>2</sub>, O<sub>3</sub>, H<sub>2</sub>O, H<sub>2</sub>O<sub>2</sub>, NO<sub>2</sub>, NO<sub>3</sub>, and N<sub>2</sub>O

WAVELENGTH BAND ANGSTROMS	FLUX PH/CM2/S/A	CROSS SECTIONS (CM2)							
		O2	O3	H2O	H2O2	NO2	NO3	N2O	
1215.67-1215.67	3.00E+11	1.00E-20	2.32E-17	0.	0.	0.	0.	0.	
1162.79-1169.59	1.51E+07	2.00E-20	7.80E-18	0.	0.	0.	0.	0.	
1169.59-1176.47	3.87E+07	1.25E-18	7.97E-18	0.	0.	0.	0.	0.	
1176.47-1183.43	1.61E+07	2.55E-19	8.66E-18	0.	0.	0.	0.	0.	
1183.43-1190.48	1.76E+07	3.00E-20	9.51E-18	0.	0.	0.	0.	0.	
1190.48-1197.60	2.55E+07	3.75E-19	1.25E-17	0.	0.	0.	0.	0.	
1197.60-1204.82	2.57E+07	4.45E-18	1.84E-17	0.	0.	0.	0.	0.	
1204.82-1212.12	1.01E+08	8.35E-18	2.19E-17	0.	0.	0.	0.	0.	
1212.12-1219.51	3.08E+08	6.00E-19	2.30E-17	0.	0.	0.	0.	0.	
1219.51-1226.99	4.91E+08	2.35E-19	2.26E-17	1.99E-17	0.	0.	0.	0.	
1226.99-1234.57	1.80E+08	4.50E-19	2.06E-17	6.15E-18	0.	0.	0.	0.	
1234.57-1242.24	1.51E+08	3.35E-19	1.30E-17	5.16E-18	0.	0.	0.	0.	
1242.24-1250.00	9.69E+07	1.75E-17	8.91E-18	1.10E-17	0.	0.	0.	0.	
1250.00-1257.86	1.05E+08	8.95E-19	7.24E-18	6.39E-18	0.	0.	0.	0.	
1257.86-1265.82	1.19E+08	4.30E-19	6.09E-18	7.13E-18	0.	0.	0.	0.	
1265.82-1273.89	1.03E+08	1.10E-19	5.66E-18	7.84E-18	0.	0.	0.	0.	
1273.89-1282.05	7.96E+07	2.05E-19	5.87E-18	7.48E-18	0.	0.	0.	0.	
1282.05-1290.32	5.71E+07	4.43E-19	6.47E-18	7.82E-18	0.	0.	0.	0.	
1290.32-1298.70	7.16E+07	5.55E-19	8.14E-18	7.64E-18	0.	0.	0.	0.	
1298.70-1307.19	3.89E+08	4.20E-19	1.24E-17	6.71E-18	0.	0.	0.	0.	
1307.19-1315.79	2.06E+08	6.85E-19	1.52E-17	6.75E-18	0.	0.	0.	0.	
1315.79-1324.50	8.68E+07	1.45E-18	1.47E-17	5.67E-18	0.	0.	0.	0.	
1324.50-1333.33	1.73E+08	2.25E-18	1.51E-17	4.93E-18	0.	0.	0.	0.	
1333.33-1342.28	2.79E+08	2.30E-18	1.51E-17	5.00E-18	0.	0.	0.	0.	
1342.28-1351.35	1.03E+08	4.55E-18	1.65E-17	3.69E-18	0.	0.	0.	0.	
1351.35-1360.54	1.62E+08	7.23E-18	1.54E-17	3.36E-18	0.	0.	0.	0.	
1360.54-1369.86	1.23E+08	9.50E-18	1.35E-17	2.42E-18	0.	0.	0.	0.	
1369.86-1379.31	1.37E+08	1.23E-17	1.05E-17	1.80E-18	0.	0.	0.	0.	
1379.31-1388.89	1.20E+08	1.32E-17	7.97E-18	1.60E-18	0.	0.	0.	0.	
1388.89-1408.45	2.93E+08	1.36E-17	7.17E-18	1.19E-18	0.	0.	0.	0.	
1408.45-1428.57	2.10E+08	1.40E-17	6.28E-18	7.00E-19	0.	0.	0.	0.	
1428.57-1449.28	2.49E+08	1.48E-17	5.66E-18	5.03E-19	0.	0.	0.	0.	
1449.28-1470.59	2.94E+08	1.41E-17	5.23E-18	4.96E-19	0.	0.	0.	0.	
1470.59-1492.54	4.06E+08	1.29E-17	4.47E-18	6.87E-19	0.	0.	0.	0.	
1492.54-1515.15	4.55E+08	1.15E-17	3.69E-18	9.45E-19	0.	0.	0.	0.	
1515.15-1538.46	5.96E+08	9.91E-18	2.93E-18	1.38E-18	0.	0.	0.	0.	
1538.46-1562.50	9.36E+08	8.24E-18	2.19E-18	1.84E-18	0.	0.	0.	0.	
1562.50-1587.30	8.59E+09	6.58E-18	1.63E-18	2.44E-18	0.	0.	0.	0.	
1587.30-1612.90	8.05E+08	4.97E-18	1.20E-18	3.20E-18	0.	0.	0.	0.	
1612.90-1639.34	1.29E+09	3.45E-18	9.77E-19	3.91E-18	0.	0.	0.	0.	
1639.34-1665.67	2.06E+09	2.08E-18	8.66E-19	4.64E-18	0.	0.	0.	0.	
1665.67-1694.92	2.84E+09	1.23E-18	9.14E-19	4.57E-18	0.	0.	0.	0.	
1694.92-1724.14	4.72E+09	7.22E-19	8.17E-19	4.35E-18	0.	0.	0.	0.	
1724.14-1759.13	4.93E+09	4.58E-19	8.57E-19	3.57E-18	0.	0.	0.	0.	
1759.13-1790.00	5.49E+09	2.74E-19	8.40E-19	2.64E-18	0.	0.	0.	0.	
1790.00-1822.20	6.25E+09	0.	8.18E-19	2.64E-18	0.	0.	0.	0.	
1822.20-1859.60	1.60E+09	0.	8.04E-19	2.22E-18	0.	0.	0.	0.	
1859.60-1904.60	8.14E+09	0.	8.00E-19	2.04E-18	0.	0.	0.	0.	
1904.60-1959.60	8.41E+09	0.	7.95E-19	1.80E-18	0.	0.	0.	0.	
1959.60-2022.60	6.86E+09	0.	7.89E-19	1.42E-18	0.	0.	0.	0.	

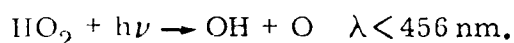
and



for wavelengths from 240 to 360 nm. The absorption cross sections for this molecule are taken from McQuigg and Calvert<sup>B14</sup> and Calvert et al.<sup>B15</sup> These authors also give the quantum efficiencies for these processes. Table B19 lists the total photodissociation rate coefficients for formaldehyde. If both of the above processes are considered to occur for this molecule, then the values presented in Table B19 must be multiplied by the relative efficiencies as given by McQuigg and Calvert<sup>B14</sup> and Calvert et al.<sup>B15</sup> for each of these reactions.

#### B14. THE HYDROPEROXYL RADICAL

The primary photodissociation process for the hydroperoxyl radical is



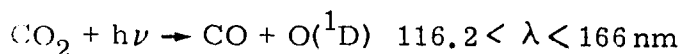
The absorption cross sections used for  $\text{HO}_2$  are a composite of the measurements of Hochanadel et al.<sup>B16</sup> and Paukert and Johnston.<sup>B17</sup> The photodissociation rate coefficients for this radical are listed in Table B20.

- 
- B14. McQuigg, R.D., and Calvert, J.G. (1969) The photodecomposition of  $\text{CH}_2\text{O}$ ,  $\text{CD}_2\text{O}$ ,  $\text{CHDO}$  and  $\text{CH}_2\text{O}-\text{CD}_2\text{O}$  mixtures at xenon flash lamp intensities, J. Am. Chem. Soc. **91**:1590-1599.
- B15. Calvert, J.G., Kerr, J.A., Demerjian, K.L., and McQuigg, R.D. (1972) Photolysis of formaldehyde as a hydrogen atom source in the lower atmosphere, Science **175**:751-752.
- B16. Hochanadel, C.J., Ghormley, A., and Ogren, P.J. (1972) Absorption spectrum and reaction kinetics of the  $\text{HO}_2$  radical in the gas phase, J. Chem. Phys. **56**:4426-4432.
- B17. Paukert, T.T., and Johnston, A.S. (1972) Spectra and kinetics of the hydroperoxyl free radical in the gas phase, J. Chem. Phys. **56**:2824-2838.

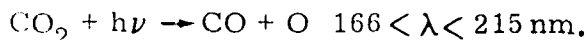
for wavelengths from 116 to 164 nm. Most of the  $\text{CH}_4$  photodissociation occurs at the Lyman  $\alpha$  line 121.6 nm. The values listed in Table B16 are the total photodissociation rate coefficients for methane. If the above processes have equal efficiencies, then each process would have rate coefficients equal to half of the values shown in the table. The absorption cross sections for this molecule are taken from Watanabe et al.<sup>B10</sup>

## B12. CARBON DIOXIDE

The photolysis of carbon dioxide can be proceed by two different processes:



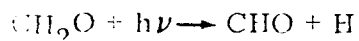
and



The absorption cross sections for this molecule are taken from Inn et al.<sup>B11</sup> Heimerl,<sup>B12</sup> and Ogawa.<sup>B13</sup> The photodissociation rate coefficients for the process yielding excited atomic oxygen are listed in Table B17, and those for the process yielding ground state atomic oxygen are listed in Table B18.

## B13. FORMALDEHYDE

Although formaldehyde can be photodissociated in several ways, the primary photolytic processes are

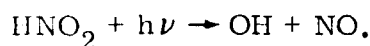


1. Watanabe, K., Zelickoff, M., and Inn, E.C.Y. (1953) Absorption Coefficient of Several Atmospheric Gases, Geophys. Res. Paper, 21, Tech Rpt. AFCRL-53-23.
2. Inn, E.C.Y., Watanabe, K., and Zelickoff, M. (1953) Absorption coefficients of gases in the vacuum ultraviolet. Part III.  $\text{CO}_2$ , J. Chem. Phys. 21:1648-1651.
3. Heimerl, J. (1970)  $\text{CO}_2$  absorption coefficient 1655-1825 A, J. Geophys. Res. 75:5574-5575.
4. Ogawa, M. (1971) Absorption cross sections of  $\text{O}_2$  and  $\text{CO}_2$  continua in the Schumann and UV regions, J. Chem. Phys. 54:2550-2556.

cule are taken from Jones and Wulf<sup>B9</sup> and Johnston and Graham.<sup>13</sup> Its photodissociation rate coefficients are listed in Table B13.

#### B9. NITROUS ACID

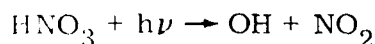
The photodissociation of nitrous acid probably proceeds as



The absorption cross sections for this molecule between 300 and 390 nm are those given by Johnston and Graham.<sup>13</sup> Since  $\text{O}_2$  is not an efficient absorber of radiation in this wavelength interval, the photodissociation rate coefficients for  $\text{HNO}_2$  are listed in Table B14 only as a function of the column density of ozone.

#### B10. NITRIC ACID

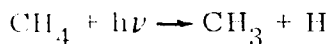
The primary photolytic process for nitric acid is



over the broad wavelength region from 192 to 325 nm. The values for the absorption cross sections for this gas are taken from Johnston and Graham.<sup>13</sup> The nitric acid photodissociation rate coefficients are listed in Table B15.

#### B11. METHANE

The photodissociation processes for methane are

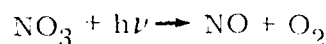


and



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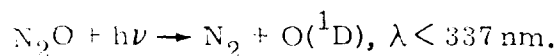
B9. Jones, E.J., and Wulf, O.R. (1937) The absorption coefficient of nitrogen pentoxide in the ultraviolet and the visible absorption spectrum of  $\text{NO}_3$ , J. Chem. Phys. 5:873-877.



for wavelengths longer than 578 nm. For wavelengths below 578 nm, it is not known whether the products are  $\text{NO}_2 + \text{O}$  or  $\text{NO} + \text{O}_2$ . In Table B11, all the photodissociation of this radical is assumed to produce  $\text{NO} + \text{O}_2$ . The absorption cross sections for this molecule are taken from Johnston and Graham.<sup>13</sup> Since molecular oxygen is not an efficient absorber for radiations above 450 nm, the photodissociation rate coefficients for this molecule are given only as a function of the ozone column density.

## B7. NITROUS OXIDE

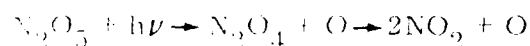
The primary photolytic process for nitrous oxide according to Preston and Barr<sup>B6</sup> is



Below 210 nm, oxygen atoms in the  $^1\text{S}$  state may be produced. For the calculations presented in this report, Table B12 was computed with all of the photodissociation of  $\text{N}_2\text{O}$  producing  $\text{O}(^1\text{D})$ . The absorption cross sections below 205 nm are from Zelikoff et al.<sup>B7</sup> and above 205 nm, from Bates and Hayes.<sup>B8</sup>

## B8. DINITROGEN PENTOXIDE

The primary processes in the photolysis of  $\text{N}_2\text{O}_5$  are not well understood. Jones and Wulf<sup>B9</sup> attribute the photodissociation of this molecule to



for wavelengths from 210 to 330 nm. The absorption cross sections for this molecule

B6. Preston, K.F., and Barr, R.F. (1971) Primary processes in the photolysis of nitrous oxide, J. Chem. Phys., 54,3347-3348.

B7. Zelikoff, M., Watanabe, K., and Imu, E.C.Y. (1953) Absorption coefficients of gases in the vacuum ultraviolet. Part II. Nitrous oxide, J. Chem. Phys., 21,1643-1647.

B8. Bates, D.R., and Hayes, P.B. (1967) Atmospheric nitrous oxide, Planet. Space Sci., 15,139-147.



Table 14. Total Photodissociation Rate Coefficients for the Process  $O_2 + h\nu \rightarrow O(^1D)$  (Contd)

		O3 COLUMN DENSITY					
		5.0E+18	1.0E+19	2.0E+19	5.0E+19	1.0E+20	2.0E+20
1.0E+13	6.79834E-09	9.47067E-11	2.23187E-14	4.24957E-25	7.77344E-43	3.03675E-78	
2.0E+13	6.79822E-09	9.47055E-11	2.23184E-14	4.24953E-25	7.77336E-43	3.03671E-78	
5.0E+13	6.79788E-09	9.47016E-11	2.23177E-14	4.24940E-25	7.77312E-43	3.03662E-78	
1.0E+14	6.79731E-09	9.46952E-11	2.23164E-14	4.24919E-25	7.77273E-43	3.03646E-78	
2.0E+14	6.79618E-09	9.46824E-11	2.23139E-14	4.24876E-25	7.77195E-43	3.03614E-78	
5.0E+14	6.79277E-09	9.46440E-11	2.23062E-14	4.24746E-25	7.76959E-43	3.03519E-78	
1.0E+15	6.78709E-09	9.45800E-11	2.22935E-14	4.24531E-25	7.76567E-43	3.03360E-78	
2.0E+15	6.77575E-09	9.44522E-11	2.22680E-14	4.24101E-25	7.75783E-43	3.03042E-78	
5.0E+15	6.74192E-09	9.40702E-11	2.21919E-14	4.22813E-25	7.73437E-43	3.02091E-78	
1.0E+16	6.68610E-09	9.34384E-11	2.20657E-14	4.20676E-25	7.69544E-43	3.00512E-78	
2.0E+16	6.57656E-09	9.21925E-11	2.18161E-14	4.16438E-25	7.61821E-43	2.97381E-78	
5.0E+16	6.26383E-09	8.85918E-11	2.10884E-14	4.04011E-25	7.39145E-43	2.88193E-78	
1.0E+17	5.79071E-09	8.30145E-11	1.99426E-14	3.84213E-25	7.02941E-43	2.73539E-78	
2.0E+17	4.99391E-09	7.32432E-11	1.78774E-14	3.47802E-25	6.36107E-43	2.46540E-78	
5.0E+17	3.39109E-09	5.19651E-11	1.31032E-14	2.59836E-25	4.73406E-43	1.81176E-78	
1.0E+18	2.01269E-09	3.17454E-11	8.18451E-15	1.63393E-25	2.93529E-43	1.09807E-78	
2.0E+18	8.94428E-10	1.41535E-11	3.62480E-15	6.95328E-26	1.18981E-43	4.23429E-79	
5.0E+18	1.58965E-10	2.41572E-12	5.68530E-16	8.57694E-27	1.14044E-44	3.39320E-80	
1.0E+19	2.18886E-11	3.24585E-13	7.18573E-17	8.26195E-28	6.12377E-46	9.18129E-82	
2.0E+19	1.07208E-12	1.60175E-14	3.57869E-18	4.01515E-29	2.29144E-47	8.03806E-84	
5.0E+19	2.75090E-16	4.12506E-18	9.27565E-22	1.05462E-32	6.06327E-51	2.00427E-87	
1.0E+20	3.08714E-22	4.62933E-24	1.04099E-27	1.18365E-38	6.80543E-57	2.24967E-93	
2.0E+20	4.49203E-31	5.83243E-36	1.31152E-39	1.49127E-50	8.57407E-69	2.83433E-105	
5.0E+20	1.08004E-33	1.24725E-50	2.62283E-75	2.98228E-86	1.71467E-104	5.66818E-141	
1.0E+21	4.90335E-38	5.66250E-55	7.55159E-89	9.46683E-146	5.44298E-164	1.79928E-200	
2.0E+21	1.01066E-48	1.16713E-63	1.55650E-97	3.69182E-199	5.48464E-283	0.	
5.0E+21	8.84982E-73	1.02200E-89	1.36295E-123	3.23274E-225	0.	0.	
1.0E+22	3.29220E-116	3.80190E-133	5.97028E-167	1.20260E-268	0.	0.	

O2 COLUMN DENSITY

Table B5. Total Photodissociation Rate Coefficients for the Process  $O_2 + h\nu \rightarrow O + O$  for Wavelengths From 175 to 242.2 nm

O3 COLUMN DENSITY

	1.0E+13	2.0E+13	5.0E+13	1.0E+14	2.0E+14	5.0E+14	1.0E+15	2.0E+15	5.0E+15	1.0E+16
1.0E+17	8.36791E-08	8.36784E-08	8.36764E-08	8.36731E-08	8.36664E-08	8.36464E-08	8.36131E-08	8.35466E-08	8.33473E-08	8.30164E-08
2.0E+17	7.96609E-08	7.96602E-08	7.96583E-08	7.96551E-08	7.96488E-08	7.96298E-08	7.95980E-08	7.95346E-08	7.93448E-08	7.90296E-08
5.0E+17	6.94462E-08	6.94456E-08	6.94400E-08	6.94412E-08	6.94357E-08	6.94190E-08	6.93913E-08	6.93359E-08	6.91701E-08	6.88949E-08
1.0E+18	5.78378E-08	5.78373E-08	5.78359E-08	5.78336E-08	5.78290E-08	5.78151E-08	5.77919E-08	5.77456E-08	5.76070E-08	5.73770E-08
2.0E+18	4.48169E-08	4.48165E-08	4.48154E-08	4.48136E-08	4.48100E-08	4.47991E-08	4.47811E-08	4.47450E-08	4.46369E-08	4.44575E-08
5.0E+18	2.84480E-08	2.84478E-08	2.84471E-08	2.84459E-08	2.84435E-08	2.84365E-08	2.84248E-08	2.84014E-08	2.83314E-08	2.82154E-08
1.0E+19	1.87404E-08	1.87402E-08	1.87397E-08	1.87390E-08	1.87374E-08	1.87326E-08	1.87246E-08	1.87087E-08	1.86612E-08	1.85824E-08
2.0E+19	1.19434E-08	1.19433E-08	1.19429E-08	1.19424E-08	1.19413E-08	1.19381E-08	1.19327E-08	1.19220E-08	1.18898E-08	1.18367E-08
5.0E+19	6.78508E-09	6.78501E-09	6.78490E-09	6.78445E-09	6.78375E-09	6.78166E-09	6.77119E-09	6.75038E-09	6.71603E-09	6.67184E-09
1.0E+20	4.62169E-09	4.62163E-09	4.62147E-09	4.62120E-09	4.62065E-09	4.61901E-09	4.61628E-09	4.61083E-09	4.59459E-09	4.56784E-09
2.0E+20	3.25814E-09	3.25810E-09	3.25796E-09	3.25773E-09	3.25728E-09	3.25592E-09	3.25365E-09	3.24914E-09	3.23568E-09	3.21355E-09
5.0E+20	3.25604E-09	3.25599E-09	3.25586E-09	3.25563E-09	3.25518E-09	3.25382E-09	3.25155E-09	3.24704E-09	3.23359E-09	3.21149E-09
1.0E+21	2.19371E-09	2.19369E-09	2.19356E-09	2.19372E-09	2.19898E-09	2.19783E-09	2.19591E-09	2.19209E-09	2.18071E-09	2.16203E-09
2.0E+21	1.75574E-09	1.75574E-09	1.75563E-09	1.75546E-09	1.75510E-09	1.75403E-09	1.75225E-09	1.74870E-09	1.73815E-09	1.72886E-09
5.0E+21	1.49053E-09	1.49050E-09	1.49040E-09	1.49033E-09	1.48989E-09	1.48897E-09	1.4873E-09	1.48381E-09	1.47379E-09	1.45738E-09
1.0E+22	1.29543E-09	1.29540E-09	1.29530E-09	1.29514E-09	1.29482E-09	1.29385E-09	1.29223E-09	1.28901E-09	1.27944E-09	1.26378E-09
2.0E+22	1.16775E-09	1.16775E-09	1.16766E-09	1.16750E-09	1.16720E-09	1.16627E-09	1.16474E-09	1.16168E-09	1.15259E-09	1.13770E-09
5.0E+22	9.58654E-10	9.58627E-10	9.58546E-10	9.58410E-10	9.58139E-10	9.57328E-10	9.55977E-10	9.53286E-10	9.45287E-10	9.32304E-10
1.0E+23	7.03317E-10	7.03295E-10	7.03229E-10	7.03118E-10	7.02897E-10	7.02234E-10	7.01131E-10	6.98933E-10	6.92405E-10	6.81737E-10
2.0E+23	4.12219E-10	4.12204E-10	4.12158E-10	4.12081E-10	4.11928E-10	4.11471E-10	4.10709E-10	4.09192E-10	4.04690E-10	3.97346E-10
5.0E+23	1.18661E-10	1.18655E-10	1.18636E-10	1.18600E-10	1.18545E-10	1.18362E-10	1.18058E-10	1.17454E-10	1.15664E-10	1.12756E-10
1.0E+24	3.05886E-11	3.05866E-11	3.05807E-11	3.05702E-11	3.05498E-11	3.04886E-11	3.03859E-11	3.01848E-11	2.95873E-11	2.86217E-11
2.0E+24	8.54771E-12	8.54716E-12	8.54551E-12	8.54273E-12	8.53727E-12	8.52922E-12	8.49249E-12	8.43918E-12	8.27895E-12	8.07063E-12
5.0E+24	2.80922E-12	2.80815E-12	2.80794E-12	2.80738E-12	2.80687E-12	2.80473E-12	2.80117E-12	2.79418E-12	2.78318E-12	2.76324E-12
1.0E+25	2.34202E-12	2.34200E-12	2.34193E-12	2.34183E-12	2.34163E-12	2.34101E-12	2.33999E-12	2.33794E-12	2.33181E-12	2.32165E-12
2.0E+25	2.32211E-12	2.32209E-12	2.32204E-12	2.32194E-12	2.32176E-12	2.32120E-12	2.32068E-12	2.31839E-12	2.31275E-12	2.30346E-12

O2 COLUMN DENSITY

Table 15. Total Photoionization Rate Coefficients for the Process  $O_2 + h\nu \rightarrow O + O$  for Wavelengths From 175 to 242.2 nm (Cont'd)

		O3 COLUMN DENSITY									
		2.0E+16	5.0E+16	1.0E+17	2.0E+17	5.0E+17	1.0E+18	2.0E+18	5.0E+18	1.0E+19	2.0E+19
1.0E+17	8.23593E-08	8.04246E-08	7.73159E-08	7.14945E-08	5.66739E-08	3.86203E-08	1.80502E-08	1.93497E-09	6.22227E-11	3.88685E-13	
2.0E+17	7.84037E-08	7.65612E-08	7.36013E-08	6.80606E-08	5.39608E-08	3.67881E-08	1.72141E-08	1.85505E-09	6.05895E-11	3.87938E-13	
5.0E+17	6.83484E-08	6.67403E-08	6.41590E-08	5.93223E-08	4.70661E-08	3.21332E-08	1.50907E-08	1.65214E-09	5.64206E-11	3.85817E-13	
1.0E+18	5.69205E-08	5.55781E-08	5.341E-08	4.94087E-08	3.92220E-08	2.68312E-08	1.26659E-08	1.41812E-09	5.14674E-11	3.82177E-13	
2.0E+18	4.41017E-08	4.30567E-08	4.13851E-08	3.82738E-08	3.04156E-08	2.08730E-08	9.93541E-09	1.15254E-09	4.57406E-11	3.78163E-13	
5.0E+18	2.79853E-08	2.73124E-08	2.62414E-08	2.42635E-08	1.93198E-08	1.33475E-08	6.46744E-09	8.07455E-10	3.77590E-11	3.70179E-13	
1.0E+19	1.84265E-08	1.79722E-08	1.72547E-08	1.59439E-08	1.27178E-08	8.85386E-09	4.38021E-09	5.93023E-10	3.23310E-11	3.62676E-13	
2.0E+19	1.17318E-08	1.14281E-08	1.09541E-08	1.01032E-08	8.06359E-09	5.66293E-09	2.87414E-09	4.28336E-10	2.73964E-11	3.50925E-13	
5.0E+19	6.64656E-09	6.45547E-09	6.16043E-09	5.64812E-09	4.48576E-09	3.17666E-09	1.66625E-09	2.81839E-10	2.18888E-11	3.3017E-13	
1.0E+20	4.51559E-09	4.36707E-09	4.14439E-09	3.76924E-09	2.96396E-09	2.10352E-09	1.12840E-09	2.09148E-10	1.64843E-11	3.110E-13	
2.0E+20	3.17041E-09	3.04920E-09	2.87063E-09	2.57918E-09	1.99268E-09	1.40941E-09	7.70327E-10	1.55452E-10	1.53759E-11	2.8E-13	
5.0E+20	3.16838E-09	3.04728E-09	2.86888E-09	2.57769E-09	1.99168E-09	1.40879E-09	7.70035E-10	1.55397E-10	1.53705E-11	2.7E-13	
1.0E+21	2.12576E-09	2.02486E-09	1.87920E-09	1.65023E-09	1.22740E-09	8.53232E-10	4.72751E-10	1.04948E-10	1.17558E-11	2.5E-13	
2.0E+21	1.68732E-09	1.59453E-09	1.46199E-09	1.25788E-09	9.00217E-10	6.10129E-10	3.36480E-10	7.83265E-11	9.43953E-12	2.14135E-13	
5.0E+21	1.42500E-09	1.33794E-09	1.21157E-09	1.02460E-09	7.05255E-10	4.63424E-10	2.51417E-10	5.99429E-11	7.63448E-12	1.85954E-13	
1.0E+22	1.23347E-09	1.15007E-09	1.03236E-09	8.55318E-10	5.64536E-10	3.56948E-10	1.88097E-10	4.50794E-11	6.02269E-12	1.57677E-13	
2.0E+22	1.10892E-09	1.02987E-09	9.18651E-10	7.52459E-10	4.64043E-10	2.98625E-10	1.54032E-10	3.66700E-11	5.00513E-12	1.36236E-13	
5.0E+22	9.06936E-10	8.37738E-10	7.40991E-10	5.98057E-10	3.73317E-10	2.24810E-10	1.14036E-10	2.71906E-11	3.81188E-12	1.08378E-13	
1.0E+23	6.61173E-10	6.05122E-10	5.27515E-10	4.14905E-10	2.45244E-10	1.40952E-10	6.87819E-11	1.59798E-11	2.25926E-12	6.61797E-14	
2.0E+23	3.83235E-10	3.45100E-10	2.93210E-10	2.20309E-10	1.18551E-10	6.35160E-11	2.96893E-11	6.85088E-12	1.00007E-12	3.07726E-14	
5.0E+23	1.07213E-10	9.25449E-11	7.34312E-11	4.86877E-11	2.03970E-11	9.64924E-12	4.57852E-12	1.21106E-12	2.05296E-13	7.24282E-15	
1.0E+24	2.67951E-11	2.20719E-11	1.62007E-11	9.26161E-12	2.93456E-12	1.29966E-12	5.41249E-13	6.31005E-14	4.84552E-15	1.52144E-16	
2.0E+24	7.53517E-12	6.29823E-12	4.80552E-12	3.12606E-12	1.65148E-12	1.03930E-12	4.63488E-13	4.24045E-14	1.07364E-15	1.33514E-17	
5.0E+24	2.77466E-12	2.60425E-12	2.38066E-12	2.07309E-12	1.55767E-12	1.03654E-12	4.63449E-13	4.24042E-14	1.07363E-15	1.33513E-17	
1.0E+25	2.30156E-12	2.24295E-12	2.15012E-12	1.97922E-12	1.55133E-12	1.03647E-12	4.63449E-13	4.24042E-14	1.07363E-15	1.33513E-17	
2.0E+25	2.28494E-12	2.23026E-12	2.14203E-12	1.97993E-12	1.55111E-12	1.03647E-12	4.63449E-13	4.24042E-14	1.07363E-15	1.33513E-17	

O2 COLUMN DENSITY

Table B5. Total Photodissociation Rate Coefficients for the Process  $O_2 + h\nu \rightarrow O + O$  for Wavelengths From 175 to 242.2 nm (Contd)

O3 COLUMN DENSITY				
	5.0E+19	1.0E+20	2.0E+20	5.0E+20 1.0E+21
1.0E+17	6.73391E-18	5.25966E-25	2.73918E-39	6.48784E-82 7.83393-153
2.0E+17	8.73401E-18	5.25969E-25	2.73918E-39	6.48784E-82 7.83393-153
5.0E+17	8.73431E-18	5.25972E-25	2.73915E-39	6.48771E-82 7.83377-153
1.0E+18	8.70961E-18	5.25049E-25	2.73786E-39	6.48769E-82 7.83385-153
2.0E+18	8.70936E-18	5.25076E-25	2.73786E-39	6.48763E-82 7.83385-153
5.0E+18	8.70805E-18	5.25147E-25	2.73783E-39	6.48732E-82 7.83366-153
1.0E+19	8.68652E-18	5.24339E-25	2.73649E-39	6.48685E-82 7.83351-153
2.0E+19	8.64264E-18	5.22092E-25	2.72619E-39	6.46929E-82 7.82302-153
5.0E+19	8.55010E-18	5.19131E-25	2.72091E-39	6.46673E-82 7.82211-153
1.0E+20	8.43410E-18	5.15784E-25	2.71819E-39	6.47105E-82 7.82488-153
2.0E+20	8.21772E-18	5.09124E-25	2.70931E-39	6.47191E-82 7.82630-153
5.0E+20	8.21654E-18	5.09100E-25	2.70929E-39	6.47191E-82 7.82630-153
1.0E+21	7.75047E-18	4.94050E-25	2.68714E-39	6.46964E-82 7.82824-153
2.0E+21	7.29024E-18	4.77961E-25	2.65499E-39	6.44707E-82 7.81927-153
5.0E+21	6.81167E-18	4.59358E-25	2.60309E-39	6.36972E-82 7.73855-153
1.0E+22	6.22360E-18	4.31292E-25	2.48965E-39	6.13959E-82 7.47824-153
2.0E+22	5.60679E-18	3.94057E-25	2.30204E-39	5.70753E-82 6.97128-153
5.0E+22	4.67258E-18	3.34675E-25	1.97407E-39	4.91590E-82 6.01377-153
1.0E+23	2.96441E-18	2.16146E-25	1.28895E-39	3.23148E-82 3.96684-153
2.0E+23	1.44765E-18	1.07621E-25	6.48120E-40	1.62614E-82 1.98836-153
5.0E+23	3.74534E-19	2.86729E-26	1.74848E-40	4.38425E-83 5.32466-154
1.0E+24	8.08785E-21	6.25749E-28	3.82194E-42	9.39947E-85 1.10288-155
2.0E+24	6.83445E-22	5.20470E-29	3.13298E-43	7.54866E-86 8.60985-157
5.0E+24	6.83445E-22	5.20470E-29	3.13298E-43	7.54866E-86 8.60985-157
1.0E+25	6.83445E-22	5.20470E-29	3.13298E-43	7.54866E-86 8.60985-157
2.0E+25	6.83445E-22	5.20470E-29	3.13298E-43	7.54866E-86 8.60985-157

O2 COLUMN DENSITY

Table Bb. Total Photoionization Rate Coefficients for the Process  $O_3 + h\nu \rightarrow O(^1D) + O_2(^1\Delta g)$  for Wavelengths Below 510 nm

		O3 COLUMN DENSITY									
		1.0E+12	2.0E+12	5.0E+12	1.0E+13	2.0E+13	5.0E+13	1.0E+14	2.0E+14	5.0E+14	1.0E+15
1.0E+15	9.72657E-03	9.72651E-03	9.72631E-03	9.72597E-03	9.72596E-03	9.72530E-03	9.72328E-03	9.71992E-03	9.71321E-03	9.69311E-03	9.65972E-03
2.0E+15	9.72657E-03	9.72650E-03	9.72630E-03	9.72596E-03	9.72596E-03	9.72530E-03	9.72328E-03	9.71992E-03	9.71321E-03	9.69311E-03	9.65972E-03
5.0E+15	9.72655E-03	9.72649E-03	9.72628E-03	9.72595E-03	9.72595E-03	9.72528E-03	9.72326E-03	9.71990E-03	9.71319E-03	9.69309E-03	9.65970E-03
1.0E+16	9.72653E-03	9.72646E-03	9.72626E-03	9.72592E-03	9.72592E-03	9.72525E-03	9.72323E-03	9.71988E-03	9.71316E-03	9.69306E-03	9.65968E-03
2.0E+16	9.72648E-03	9.72641E-03	9.72621E-03	9.72587E-03	9.72587E-03	9.72520E-03	9.72319E-03	9.71983E-03	9.71312E-03	9.69302E-03	9.65963E-03
5.0E+16	9.72636E-03	9.72629E-03	9.72609E-03	9.72576E-03	9.72576E-03	9.72509E-03	9.72307E-03	9.71971E-03	9.71300E-03	9.69290E-03	9.65951E-03
1.0E+17	9.72622E-03	9.72616E-03	9.72596E-03	9.72562E-03	9.72562E-03	9.72495E-03	9.72293E-03	9.71957E-03	9.71266E-03	9.69276E-03	9.65930E-03
2.0E+17	9.72600E-03	9.72600E-03	9.72579E-03	9.72546E-03	9.72546E-03	9.72479E-03	9.72277E-03	9.71941E-03	9.71270E-03	9.69260E-03	9.65922E-03
5.0E+17	9.72585E-03	9.72579E-03	9.72559E-03	9.72526E-03	9.72526E-03	9.72459E-03	9.72257E-03	9.71921E-03	9.71250E-03	9.69240E-03	9.65903E-03
1.0E+18	9.72570E-03	9.72563E-03	9.72543E-03	9.72509E-03	9.72509E-03	9.72442E-03	9.72241E-03	9.71905E-03	9.71234E-03	9.69224E-03	9.65885E-03
2.0E+18	9.72552E-03	9.72545E-03	9.72525E-03	9.72491E-03	9.72491E-03	9.72424E-03	9.72223E-03	9.71887E-03	9.71216E-03	9.69206E-03	9.65867E-03
5.0E+18	9.72528E-03	9.72522E-03	9.72502E-03	9.72468E-03	9.72468E-03	9.72401E-03	9.72199E-03	9.71863E-03	9.71192E-03	9.69182E-03	9.65844E-03
1.0E+19	9.72514E-03	9.72507E-03	9.72487E-03	9.72453E-03	9.72453E-03	9.72386E-03	9.72184E-03	9.71849E-03	9.71178E-03	9.69168E-03	9.65833E-03
2.0E+19	9.72499E-03	9.72492E-03	9.72472E-03	9.72438E-03	9.72438E-03	9.72372E-03	9.72170E-03	9.71834E-03	9.71153E-03	9.69153E-03	9.65815E-03
5.0E+19	9.72474E-03	9.72467E-03	9.72447E-03	9.72413E-03	9.72413E-03	9.72346E-03	9.72145E-03	9.71809E-03	9.71138E-03	9.69128E-03	9.65790E-03
1.0E+20	9.72443E-03	9.72436E-03	9.72416E-03	9.72382E-03	9.72382E-03	9.72315E-03	9.72114E-03	9.71778E-03	9.71107E-03	9.69097E-03	9.65759E-03
2.0E+20	9.72393E-03	9.72387E-03	9.72367E-03	9.72333E-03	9.72333E-03	9.72266E-03	9.72065E-03	9.71729E-03	9.71058E-03	9.69048E-03	9.65710E-03
5.0E+20	9.72295E-03	9.72289E-03	9.72268E-03	9.72234E-03	9.72234E-03	9.72167E-03	9.71966E-03	9.71630E-03	9.70959E-03	9.68950E-03	9.65612E-03
1.0E+21	9.72106E-03	9.72100E-03	9.72080E-03	9.72046E-03	9.72046E-03	9.71979E-03	9.71777E-03	9.71442E-03	9.70771E-03	9.68761E-03	9.65423E-03
2.0E+21	9.71753E-03	9.71752E-03	9.71732E-03	9.71698E-03	9.71698E-03	9.71631E-03	9.71430E-03	9.71094E-03	9.70423E-03	9.68414E-03	9.65078E-03
5.0E+21	9.70753E-03	9.70757E-03	9.70736E-03	9.70703E-03	9.70703E-03	9.70636E-03	9.70434E-03	9.70099E-03	9.69429E-03	9.67421E-03	9.64087E-03
1.0E+22	9.69134E-03	9.69128E-03	9.69108E-03	9.69074E-03	9.69074E-03	9.69007E-03	9.68806E-03	9.68471E-03	9.67801E-03	9.65796E-03	9.62465E-03
2.0E+22	9.66011E-03	9.66005E-03	9.65985E-03	9.65951E-03	9.65951E-03	9.65884E-03	9.65684E-03	9.65349E-03	9.64681E-03	9.62680E-03	9.59356E-03
5.0E+22	9.57430E-03	9.57423E-03	9.57404E-03	9.57370E-03	9.57370E-03	9.57304E-03	9.57104E-03	9.56772E-03	9.56108E-03	9.54119E-03	9.50815E-03
1.0E+23	9.45231E-03	9.45224E-03	9.45205E-03	9.45172E-03	9.45172E-03	9.45106E-03	9.44908E-03	9.44579E-03	9.43921E-03	9.41949E-03	9.38676E-03
2.0E+23	9.26855E-03	9.26850E-03	9.26830E-03	9.26798E-03	9.26798E-03	9.26733E-03	9.26538E-03	9.26213E-03	9.25565E-03	9.23522E-03	9.20395E-03
5.0E+23	8.97590E-03	8.97584E-03	8.97565E-03	8.97534E-03	8.97534E-03	8.97470E-03	8.97281E-03	8.96965E-03	8.96333E-03	8.94443E-03	8.91307E-03
1.0E+24	8.79821E-03	8.79795E-03	8.79776E-03	8.79745E-03	8.79745E-03	8.79683E-03	8.79497E-03	8.79188E-03	8.78569E-03	8.76715E-03	8.73637E-03
2.0E+24	8.69314E-03	8.69308E-03	8.69290E-03	8.69259E-03	8.69259E-03	8.69198E-03	8.69015E-03	8.68709E-03	8.68095E-03	8.66271E-03	8.63235E-03
5.0E+24	8.63538E-03	8.63532E-03	8.63514E-03	8.63483E-03	8.63483E-03	8.63423E-03	8.63241E-03	8.62938E-03	8.62333E-03	8.60520E-03	8.57509E-03
1.0E+25	8.62788E-03	8.62782E-03	8.62763E-03	8.62733E-03	8.62733E-03	8.62673E-03	8.62491E-03	8.62188E-03	8.61584E-03	8.59773E-03	8.56766E-03
2.0E+25	8.62761E-03	8.62755E-03	8.62737E-03	8.62707E-03	8.62707E-03	8.62646E-03	8.62464E-03	8.62162E-03	8.61557E-03	8.59747E-03	8.56739E-03

O3 COLUMN DENSITY

Table Bb. Total Photodissociation Rate Coefficients for the Process  $O_3 + h\nu \rightarrow O(^1D) + O_2(^1\Delta g)$  for Wavelengths Below 310 nm (Contd)

O3 COLUMN DENSITY									
	2.0E+15	5.0E+15	1.0E+16	2.0E+16	5.0E+16	1.0E+17	2.0E+17	5.0E+17	1.0E+18
1.0E+15	9.59335E-03	9.39780E-03	9.08291E-03	8.49245E-03	6.99530E-03	5.19826E-03	3.16694E-03	1.30466E-03	6.63680E-04
2.0E+15	9.59336E-03	9.39779E-03	9.08290E-03	8.49245E-03	6.99530E-03	5.19826E-03	3.16694E-03	1.30466E-03	6.63680E-04
5.0E+15	9.59337E-03	9.39778E-03	9.08289E-03	8.49244E-03	6.99528E-03	5.19825E-03	3.16693E-03	1.30465E-03	6.63679E-04
1.0E+16	9.59338E-03	9.39777E-03	9.08288E-03	8.49243E-03	6.99526E-03	5.19823E-03	3.16692E-03	1.30464E-03	6.63677E-04
2.0E+16	9.59329E-03	9.39770E-03	9.08282E-03	8.49237E-03	6.99523E-03	5.19821E-03	3.16690E-03	1.30465E-03	6.63674E-04
5.0E+16	9.59316E-03	9.39759E-03	9.08271E-03	8.49227E-03	6.99514E-03	5.19814E-03	3.16686E-03	1.30462E-03	6.63665E-04
1.0E+17	9.59304E-03	9.39746E-03	9.08258E-03	8.49214E-03	6.99504E-03	5.19805E-03	3.16680E-03	1.30460E-03	6.63653E-04
2.0E+17	9.59288E-03	9.39730E-03	9.08243E-03	8.49200E-03	6.99492E-03	5.19796E-03	3.16672E-03	1.30456E-03	6.63630E-04
5.0E+17	9.59268E-03	9.39711E-03	9.08224E-03	8.49182E-03	6.99476E-03	5.19783E-03	3.16662E-03	1.30448E-03	6.63587E-04
1.0E+18	9.59252E-03	9.39695E-03	9.08208E-03	8.49168E-03	6.99464E-03	5.19772E-03	3.16653E-03	1.30442E-03	6.63544E-04
2.0E+18	9.59234E-03	9.39677E-03	9.08191E-03	8.49152E-03	6.99450E-03	5.19760E-03	3.16643E-03	1.30434E-03	6.63494E-04
5.0E+18	9.59211E-03	9.39655E-03	9.08170E-03	8.49131E-03	6.99432E-03	5.19745E-03	3.16630E-03	1.30425E-03	6.63429E-04
1.0E+19	9.59197E-03	9.39640E-03	9.08156E-03	8.49118E-03	6.99420E-03	5.19734E-03	3.16621E-03	1.30418E-03	6.63382E-04
2.0E+19	9.59182E-03	9.39626E-03	9.08142E-03	8.49104E-03	6.99407E-03	5.19722E-03	3.16611E-03	1.30410E-03	6.63331E-04
5.0E+19	9.59157E-03	9.39601E-03	9.08117E-03	8.49080E-03	6.99384E-03	5.19702E-03	3.16593E-03	1.30397E-03	6.63247E-04
1.0E+20	9.59127E-03	9.39571E-03	9.08087E-03	8.49051E-03	6.99357E-03	5.19641E-03	3.16573E-03	1.30384E-03	6.63163E-04
2.0E+20	9.59080E-03	9.39522E-03	9.08039E-03	8.49005E-03	6.99315E-03	5.19641E-03	3.16544E-03	1.30366E-03	6.63053E-04
5.0E+20	9.58980E-03	9.39426E-03	9.07945E-03	8.48915E-03	6.99236E-03	5.19577E-03	3.16500E-03	1.30348E-03	6.62982E-04
1.0E+21	9.58793E-03	9.39241E-03	9.07763E-03	8.48740E-03	6.99081E-03	5.19447E-03	3.16405E-03	1.30279E-03	6.62727E-04
2.0E+21	9.58448E-03	9.38901E-03	9.07430E-03	8.48421E-03	6.98799E-03	5.19214E-03	3.16241E-03	1.30223E-03	6.62374E-04
5.0E+21	9.57461E-03	9.37927E-03	9.06478E-03	8.47510E-03	6.97998E-03	5.18561E-03	3.15788E-03	1.30223E-03	6.62374E-04
1.0E+22	9.56847E-03	9.36335E-03	9.04921E-03	8.46020E-03	6.96689E-03	5.17494E-03	3.15051E-03	1.29710E-03	6.60209E-04
2.0E+22	9.52750E-03	9.33282E-03	9.01937E-03	8.43168E-03	6.94189E-03	5.15466E-03	3.13662E-03	1.29129E-03	6.57873E-04
5.0E+22	9.44251E-03	9.24900E-03	8.93748E-03	8.35348E-03	6.87359E-03	5.09956E-03	3.10993E-03	1.27624E-03	6.52088E-04
1.0E+23	9.32171E-03	9.12551E-03	8.82126E-03	8.24270E-03	6.77734E-03	5.02258E-03	3.04812E-03	1.25639E-03	6.4724E-04
2.0E+23	9.13986E-03	9.95083E-03	8.64678E-03	8.07693E-03	6.63473E-03	4.91022E-03	2.97595E-03	1.23084E-03	6.36150E-04
5.0E+23	8.85060E-03	8.66073E-03	8.37083E-03	7.65152E-03	6.41556E-03	4.74424E-03	2.87670E-03	1.20232E-03	6.25553E-04
1.0E+24	8.67521E-03	8.45436E-03	8.12649E-03	7.68191E-03	6.20374E-03	4.65444E-03	2.82956E-03	1.19333E-03	6.27124E-04
2.0E+24	8.57203E-03	8.35424E-03	8.10827E-03	7.47274E-03	6.21975E-03	4.60753E-03	2.80818E-03	1.19096E-03	6.26930E-04
5.0E+24	8.51528E-03	8.38972E-03	8.05530E-03	7.44331E-03	6.18260E-03	4.56363E-03	2.79826E-03	1.19023E-03	6.26979E-04
1.0E+25	8.50751E-03	8.37332E-03	8.04850E-03	7.43180E-03	6.17782E-03	4.56058E-03	2.79702E-03	1.19015E-03	6.26978E-04
2.0E+25	8.50765E-03	8.37315E-03	8.04825E-03	7.43175E-03	6.17765E-03	4.56047E-03	2.79697E-03	1.19015E-03	6.26978E-04

O3 COLUMN DENSITY

Table 13a. Total Photodissociation Rate Coefficients for the Process  $O_3 + h\nu \rightarrow O(^1D) + O_2(^1\Delta g)$  for Wavelengths Below 510 nm (Contd)

O3 COLUMN DENSITY									
5.0E+18	1.0E+19	2.0E+19	5.0E+19	1.0E+20	2.0E+20	5.0E+20	1.0E+21		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.31466E-07	1.71194E-09	4.71332E-14	9.84126E-28	1.55808E-50		
1.09487E-04	3.98002E-05	9.65152E-06	3.						

O2 COLUMN DENSITY

Table B7. Total Photodissociation Rate Coefficients for the Process  $O_3 + h\nu \rightarrow O + O_2$  for Wavelengths From 310 to 730 nm

1.0E+14	4.17996E-04
2.0E+14	4.17995E-04
5.0E+14	4.17994E-04
1.0E+15	4.17992E-04
2.0E+15	4.17989E-04
5.0E+15	4.17978E-04
1.0E+16	4.17960E-04
2.0E+16	4.17924E-04
5.0E+16	4.17816E-04
1.0E+17	4.17636E-04
2.0E+17	4.17276E-04
5.0E+17	4.16205E-04
1.0E+18	4.14441E-04
2.0E+18	4.10992E-04
5.0E+18	4.01237E-04
1.0E+19	3.86702E-04
2.0E+19	3.62634E-04
5.0E+19	3.13047E-04
1.0E+20	2.60086E-04
2.0E+20	1.90049E-04
5.0E+20	8.70967E-05
1.0E+21	3.45505E-05

O3 COLUMN DENSITY



Table B6. Total Photodissociation Rate Coefficients for the Process  $\text{H}_2\text{O} + h\nu \rightarrow \text{OH} + \text{H}$  for Wavelengths From 121.9 to 186.4 nm

O3 COLUMN DENSITY

	1.0E+11	2.0E+11	5.0E+11	1.0E+12	2.0E+12	5.0E+12	1.0E+13	2.0E+13	5.0E+13	1.0E+14
1.0E+13	7.38657E-06	7.38656E-06	7.38653E-06	7.38647E-06	7.38637E-06	7.38606E-06	7.38554E-06	7.38451E-06	7.38141E-06	7.37625E-06
2.0E+13	7.38653E-06	7.38652E-06	7.38649E-06	7.38643E-06	7.38633E-06	7.38603E-06	7.38550E-06	7.38447E-06	7.38137E-06	7.37621E-06
5.0E+13	7.38640E-06	7.38639E-06	7.38636E-06	7.38631E-06	7.38621E-06	7.38590E-06	7.38538E-06	7.38435E-06	7.38125E-06	7.37609E-06
1.0E+14	7.38620E-06	7.38619E-06	7.38616E-06	7.38611E-06	7.38600E-06	7.38569E-06	7.38518E-06	7.38414E-06	7.38104E-06	7.37598E-06
2.0E+14	7.38579E-06	7.38578E-06	7.38575E-06	7.38570E-06	7.38560E-06	7.38529E-06	7.38477E-06	7.38374E-06	7.38064E-06	7.37547E-06
5.0E+14	7.38457E-06	7.38456E-06	7.38453E-06	7.38448E-06	7.38437E-06	7.38405E-06	7.38353E-06	7.38251E-06	7.37941E-06	7.37425E-06
1.0E+15	7.38254E-06	7.38253E-06	7.38250E-06	7.38245E-06	7.38234E-06	7.38203E-06	7.38152E-06	7.38048E-06	7.37738E-06	7.37222E-06
2.0E+15	7.37849E-06	7.37848E-06	7.37845E-06	7.37840E-06	7.37829E-06	7.37798E-06	7.37747E-06	7.37643E-06	7.37333E-06	7.36817E-06
5.0E+15	7.36647E-06	7.36646E-06	7.36643E-06	7.36638E-06	7.36627E-06	7.36596E-06	7.36545E-06	7.36441E-06	7.36132E-06	7.35616E-06
1.0E+16	7.34685E-06	7.34684E-06	7.34680E-06	7.34675E-06	7.34665E-06	7.34634E-06	7.34583E-06	7.34479E-06	7.34169E-06	7.33654E-06
2.0E+16	7.30904E-06	7.30903E-06	7.30900E-06	7.30895E-06	7.30885E-06	7.30854E-06	7.30802E-06	7.30699E-06	7.30390E-06	7.29875E-06
5.0E+16	7.20579E-06	7.20577E-06	7.20574E-06	7.20569E-06	7.20559E-06	7.20528E-06	7.20477E-06	7.20374E-06	7.20065E-06	7.19552E-06
1.0E+17	7.06019E-06	7.06018E-06	7.06015E-06	7.06010E-06	7.06000E-06	7.05969E-06	7.05918E-06	7.05815E-06	7.05508E-06	7.04996E-06
2.0E+17	6.82192E-06	6.82191E-06	6.82188E-06	6.82183E-06	6.82172E-06	6.82142E-06	6.82091E-06	6.81989E-06	6.81683E-06	6.81174E-06
5.0E+17	6.35730E-06	6.35729E-06	6.35726E-06	6.35721E-06	6.35711E-06	6.35681E-06	6.35631E-06	6.35530E-06	6.35227E-06	6.34723E-06
1.0E+18	5.89929E-06	5.89928E-06	5.89925E-06	5.89920E-06	5.89910E-06	5.89880E-06	5.89830E-06	5.89730E-06	5.89431E-06	5.88934E-06
2.0E+18	5.40915E-06	5.40914E-06	5.40912E-06	5.40907E-06	5.40897E-06	5.40867E-06	5.40819E-06	5.40721E-06	5.40427E-06	5.39939E-06
5.0E+18	4.82323E-06	4.82322E-06	4.82319E-06	4.82314E-06	4.82305E-06	4.82277E-06	4.82230E-06	4.82136E-06	4.81854E-06	4.81395E-06
1.0E+19	4.41601E-06	4.41600E-06	4.41598E-06	4.41593E-06	4.41584E-06	4.41558E-06	4.41513E-06	4.41424E-06	4.41158E-06	4.40715E-06
2.0E+19	3.91448E-06	3.91447E-06	3.91445E-06	3.91441E-06	3.91433E-06	3.91409E-06	3.91369E-06	3.91289E-06	3.91048E-06	3.90648E-06
5.0E+19	2.88069E-06	2.88069E-06	2.88067E-06	2.88064E-06	2.88058E-06	2.88040E-06	2.88011E-06	2.87951E-06	2.87773E-06	2.87477E-06
1.0E+20	1.78257E-06	1.78256E-06	1.78255E-06	1.78254E-06	1.78250E-06	1.78239E-06	1.78221E-06	1.78185E-06	1.78077E-06	1.77897E-06
2.0E+20	7.20230E-07	7.20228E-07	7.20224E-07	7.20218E-07	7.20204E-07	7.20165E-07	7.20098E-07	7.19965E-07	7.19566E-07	7.18902E-07
5.0E+20	1.80122E-07	1.80122E-07	1.80122E-07	1.80121E-07	1.80121E-07	1.80118E-07	1.80114E-07	1.80107E-07	1.80084E-07	1.80045E-07
1.0E+21	6.60228E-08	6.60228E-08	6.60227E-08	6.60227E-08	6.60227E-08	6.60225E-08	6.60223E-08	6.60217E-08	6.60201E-08	6.60174E-08
2.0E+21	2.82041E-08	2.82041E-08	2.82040E-08	2.82040E-08	2.82040E-08	2.82040E-08	2.82039E-08	2.82036E-08	2.82030E-08	2.82020E-08
5.0E+21	1.06830E-08	1.06830E-08	1.06830E-08	1.06830E-08	1.06830E-08	1.06830E-08	1.06830E-08	1.06829E-08	1.06827E-08	1.06823E-08
1.0E+22	2.28878E-09	2.28878E-09	2.28878E-09	2.28878E-09	2.28878E-09	2.28877E-09	2.28877E-09	2.28877E-09	2.28870E-09	2.28862E-09
2.0E+22	6.07985E-10	6.07985E-10	6.07985E-10	6.07985E-10	6.07984E-10	6.07983E-10	6.07981E-10	6.07976E-10	6.07963E-10	6.07940E-10
5.0E+22	3.05080E-10	3.05080E-10	3.05080E-10	3.05080E-10	3.05080E-10	3.05079E-10	3.05078E-10	3.05076E-10	3.05068E-10	3.05056E-10
1.0E+23	2.82473E-10	2.82473E-10	2.82473E-10	2.82473E-10	2.82472E-10	2.82472E-10	2.82471E-10	2.82468E-10	2.82462E-10	2.82450E-10

O2 COLUMN DENSITY

Table B3. Total Photodissociation Rate Coefficients for the Process  $\text{H}_2\text{O} + h\nu \rightarrow \text{OH} + \text{H}$  for Wavelengths From 121.9 to 186.4 nm (Contd)

		O3 COLUMN DENSITY									
		2.0E+14	5.0E+14	1.0E+15	2.0E+15	5.0E+15	1.0E+16	2.0E+16	5.0E+16	1.0E+17	2.0E+17
1.0E+13	7.36594E-06	7.33516E-06	7.28433E-06	7.18434E-06	6.89750E-06	6.46021E-06	5.71905E-06	4.26319E-06	3.18727E-06	2.55012E-06	
2.0E+13	7.36590E-06	7.33512E-06	7.28430E-06	7.18430E-06	6.89746E-06	6.46017E-06	5.71901E-06	4.26316E-06	3.18724E-06	2.55009E-06	
5.0E+13	7.36578E-06	7.33500E-06	7.28416E-06	7.18418E-06	6.89734E-06	6.46005E-06	5.71899E-06	4.26305E-06	3.18714E-06	2.55001E-06	
1.0E+14	7.36555E-06	7.33480E-06	7.28396E-06	7.18398E-06	6.89714E-06	6.45985E-06	5.71871E-06	4.26287E-06	3.18698E-06	2.54987E-06	
2.0E+14	7.36517E-06	7.33439E-06	7.28355E-06	7.18357E-06	6.89673E-06	6.45946E-06	5.71832E-06	4.26251E-06	3.18665E-06	2.54960E-06	
5.0E+14	7.36335E-06	7.33317E-06	7.28233E-06	7.18236E-06	6.89553E-06	6.45827E-06	5.71716E-06	4.26143E-06	3.18568E-06	2.54878E-06	
1.0E+15	7.36142E-06	7.33114E-06	7.28031E-06	7.18034E-06	6.89353E-06	6.45629E-06	5.71524E-06	4.25964E-06	3.18407E-06	2.54741E-06	
2.0E+15	7.35787E-06	7.32710E-06	7.27627E-06	7.17631E-06	6.88953E-06	6.45235E-06	5.71140E-06	4.25607E-06	3.18084E-06	2.54468E-06	
5.0E+15	7.34586E-06	7.31510E-06	7.26429E-06	7.16436E-06	6.87768E-06	6.44066E-06	5.70001E-06	4.24547E-06	3.17126E-06	2.53656E-06	
1.0E+16	7.32624E-06	7.29550E-06	7.2472E-06	7.14484E-06	6.85833E-06	6.42157E-06	5.68141E-06	4.22813E-06	3.15557E-06	2.52325E-06	
2.0E+16	7.28846E-06	7.25775E-06	7.20703E-06	7.10725E-06	6.82104E-06	6.38477E-06	5.64554E-06	4.19465E-06	3.12523E-06	2.49740E-06	
5.0E+16	7.18526E-06	7.15463E-06	7.10403E-06	7.00454E-06	6.71913E-06	6.28416E-06	5.54735E-06	4.10273E-06	3.04146E-06	2.42547E-06	
1.0E+17	7.03974E-06	7.00922E-06	6.95880E-06	6.85967E-06	6.57532E-06	6.14205E-06	5.40844E-06	3.97202E-06	2.92136E-06	2.32094E-06	
2.0E+17	6.80157E-06	6.77121E-06	6.72107E-06	6.62247E-06	6.33970E-06	5.90896E-06	5.18004E-06	3.75553E-06	2.72019E-06	2.14258E-06	
5.0E+17	6.33717E-06	6.30713E-06	6.25752E-06	6.15996E-06	5.88026E-06	5.45437E-06	4.73437E-06	3.33178E-06	2.32344E-06	1.78536E-06	
1.0E+18	5.87940E-06	5.84973E-06	5.80072E-06	5.70437E-06	5.42817E-06	5.0780E-06	4.29774E-06	2.91851E-06	1.93689E-06	1.43551E-06	
2.0E+18	5.38963E-06	5.36050E-06	5.31239E-06	5.21782E-06	4.94876E-06	4.53438E-06	3.83845E-06	2.49069E-06	1.54144E-06	1.07926E-06	
5.0E+18	4.80449E-06	4.77654E-06	4.73038E-06	4.63963E-06	4.37960E-06	3.98419E-06	3.31750E-06	2.03036E-06	1.13268E-06	7.19502E-07	
1.0E+19	4.39830E-06	4.37187E-06	4.32822E-06	4.24242E-06	3.99658E-06	3.62282E-06	2.99288E-06	1.77826E-06	9.35994E-07	5.59245E-07	
2.0E+19	3.89849E-06	3.87464E-06	3.83524E-06	3.75781E-06	3.53555E-06	3.19868E-06	2.63035E-06	1.53522E-06	7.77633E-07	4.40097E-07	
5.0E+19	2.86886E-06	2.85119E-06	2.82202E-06	2.76469E-06	2.60042E-06	2.35070E-06	1.92999E-06	1.11935E-06	5.59076E-07	3.10607E-07	
1.0E+20	1.77538E-06	1.76466E-06	1.74698E-06	1.71216E-06	1.61244E-06	1.46086E-06	1.20539E-06	7.12988E-07	3.71940E-07	2.18914E-07	
2.0E+20	7.17577E-07	7.13618E-07	7.07081E-07	6.94231E-07	6.57405E-07	6.01359E-07	5.06945E-07	3.24393E-07	1.96655E-07	1.36061E-07	
5.0E+20	1.79968E-07	1.79739E-07	1.79353E-07	1.78610E-07	1.76451E-07	1.73122E-07	1.67344E-07	1.55077E-07	1.43577E-07	1.30845E-07	
1.0E+21	6.60121E-08	6.59962E-08	6.59695E-08	6.59165E-08	6.57585E-08	6.54974E-08	6.49837E-08	6.34979E-08	6.11503E-08	5.67694E-08	
2.0E+21	2.82000E-08	2.81938E-08	2.81938E-08	2.81632E-08	2.81021E-08	2.80034E-08	2.77982E-08	2.72005E-08	2.62327E-08	2.43995E-08	
5.0E+21	1.06815E-08	1.06793E-08	1.06755E-08	1.06679E-08	1.06452E-08	1.06075E-08	1.05325E-08	1.03107E-08	9.95128E-09	9.26975E-09	
1.0E+22	2.28846E-09	2.28797E-09	2.28717E-09	2.28555E-09	2.28071E-09	2.27267E-09	2.25667E-09	2.20936E-09	2.13270E-09	1.98730E-09	
2.0E+22	6.07896E-10	6.07761E-10	6.07537E-10	6.07089E-10	6.05748E-10	6.03520E-10	5.99088E-10	5.85988E-10	5.64791E-10	5.24684E-10	
5.0E+22	3.05032E-10	3.04960E-10	3.04840E-10	3.04599E-10	3.03880E-10	3.02684E-10	3.00306E-10	2.81943E-10	2.60565E-10		
1.0E+23	2.82429E-10	2.82363E-10	2.82248E-10	2.82023E-10	2.81349E-10	2.80229E-10	2.78003E-10	2.71431E-10	2.60821E-10	2.40830E-10	

O2 COLUMN DENSITY

Table B3. Total Photodissociation Rate Coefficients for the Process  $\text{H}_2\text{O} + h\nu \rightarrow \text{OH} + \text{H}$  for Wavelengths From 121.9 to 186.4 nm (Contd)

		O3 COLUMN DENSITY									
		5.0E+17	1.0E+18	2.0E+18	5.0E+18	1.0E+19	2.0E+19	5.0E+19	1.0E+20	2.0E+20	5.0E+20
1.0E+13	1.92246E-06	1.25722E-06	5.46968E-07	4.69360E-08	8.30989E-10	3.13497E-13	1.24003E-22	4.70744E-37	1.40762E-65	4.19584E-151	
2.0E+13	1.92245E-06	1.25721E-06	5.46964E-07	4.69357E-08	8.30985E-10	3.13496E-13	1.24003E-22	4.70744E-37	1.40762E-65	4.19584E-151	
5.0E+13	1.92239E-06	1.25717E-06	5.46952E-07	4.69349E-08	8.30972E-10	3.13493E-13	1.24003E-22	4.70744E-37	1.40762E-65	4.19584E-151	
1.0E+14	1.92230E-06	1.25712E-06	5.46947E-07	4.69334E-08	8.30952E-10	3.13488E-13	1.24003E-22	4.70744E-37	1.40762E-65	4.19584E-151	
2.0E+14	1.92211E-06	1.25701E-06	5.46890E-07	4.69305E-08	8.30911E-10	3.13478E-13	1.24001E-22	4.70744E-37	1.40762E-65	4.19584E-151	
5.0E+14	1.92156E-06	1.25669E-06	5.46767E-07	4.69219E-08	8.30788E-10	3.13449E-13	1.24001E-22	4.70744E-37	1.40762E-65	4.19584E-151	
1.0E+15	1.92053E-06	1.25615E-06	5.46561E-07	4.69075E-08	8.30584E-10	3.13400E-13	1.24000E-22	4.70744E-37	1.40762E-65	4.19584E-151	
2.0E+15	1.91878E-06	1.25507E-06	5.46151E-07	4.68787E-08	8.30176E-10	3.13303E-13	1.23998E-22	4.70743E-37	1.40762E-65	4.19584E-151	
5.0E+15	1.91328E-06	1.25186E-06	5.45326E-07	4.67920E-08	8.28955E-10	3.13012E-13	1.23992E-22	4.70743E-37	1.40762E-65	4.19584E-151	
1.0E+16	1.90422E-06	1.24657E-06	5.44901E-07	4.66504E-08	8.26930E-10	3.12529E-13	1.23983E-22	4.70743E-37	1.40762E-65	4.19584E-151	
2.0E+16	1.88754E-06	1.23619E-06	5.38514E-07	4.63691E-08	8.22923E-10	3.11572E-13	1.23965E-22	4.70743E-37	1.40762E-65	4.19584E-151	
5.0E+16	1.83632E-06	1.20658E-06	5.27438E-07	4.55517E-08	8.11219E-10	3.08767E-13	1.23910E-22	4.70743E-37	1.40762E-65	4.19584E-151	
1.0E+17	1.63141E-06	1.08022E-06	4.76607E-07	4.42723E-08	7.92723E-10	3.04302E-13	1.23823E-22	4.70743E-37	1.40632E-65	4.19197E-151	
5.0E+17	1.36039E-06	9.06076E-07	4.03288E-07	3.59825E-08	6.65582E-10	2.70930E-13	1.22406E-22	4.68932E-37	1.40246E-65	4.18046E-151	
1.0E+18	1.09022E-06	7.28659E-07	3.26428E-07	2.95381E-08	5.63528E-10	2.42722E-13	1.20955E-22	4.66731E-37	1.39616E-65	4.16168E-151	
2.0E+18	8.14274E-07	5.46233E-07	2.46519E-07	2.28901E-08	4.52332E-10	2.10869E-13	1.18777E-22	4.62521E-37	1.38401E-65	4.12548E-151	
5.0E+18	5.36387E-07	3.62213E-07	1.65588E-07	1.59748E-08	3.55915E-10	1.75261E-13	1.14401E-22	4.51179E-37	1.35090E-65	4.02684E-151	
1.0E+19	4.10798E-07	2.78686E-07	1.28502E-07	1.27069E-08	2.77544E-10	1.54356E-13	1.09395E-22	4.35489E-37	1.30460E-65	3.88884E-151	
2.0E+19	3.22841E-07	2.19694E-07	1.01880E-07	1.02443E-08	2.29857E-10	1.34277E-13	1.02431E-22	4.11734E-37	1.23403E-65	3.67851E-151	
5.0E+19	2.27430E-07	1.55232E-07	7.24053E-08	7.41035E-09	1.71387E-10	1.06409E-13	8.99826E-23	3.67342E-37	1.10184E-65	3.28448E-151	
1.0E+20	1.62437E-07	1.11127E-07	5.20745E-08	5.40725E-09	1.28313E-10	8.40530E-14	7.80227E-23	3.23362E-37	9.70704E-66	2.89361E-151	
2.0E+20	1.04150E-07	7.14751E-08	3.37009E-08	3.56743E-09	8.75905E-11	6.15006E-14	6.38836E-23	2.69464E-37	8.09655E-66	2.41356E-151	
5.0E+20	1.04151E-07	7.14751E-08	3.37009E-08	3.56743E-09	8.75905E-11	6.15006E-14	6.38836E-23	2.69464E-37	8.09655E-66	2.41356E-151	
1.0E+21	4.54621E-08	3.14083E-08	1.50104E-08	1.65583E-09	4.35838E-11	3.47797E-14	4.29870E-23	1.85582E-37	5.58139E-66	1.66381E-151	
2.0E+21	1.96353E-08	1.36752E-08	6.64109E-09	7.67802E-10	2.7352E-11	1.94766E-14	2.73702E-23	1.19715E-37	3.60025E-66	1.07323E-151	
5.0E+21	7.49321E-09	5.25744E-09	2.59052E-09	3.12148E-10	9.39104E-12	9.21005E-15	1.42319E-23	6.27559E-38	1.88588E-66	5.62169E-152	
1.0E+22	1.60809E-09	1.13033E-09	5.59159E-10	6.83291E-11	2.11332E-12	2.19137E-15	3.69045E-24	1.65256E-38	4.96672E-67	1.48054E-152	
2.0E+22	4.20746E-10	2.91428E-10	1.40184E-10	1.59283E-11	4.52356E-13	4.37401E-16	7.55264E-25	3.48454E-39	1.05148E-67	3.13457E-153	
5.0E+22	2.05689E-10	1.38726E-10	6.31726E-11	6.02498E-12	1.25114E-13	6.79248E-17	6.95153E-26	3.27616E-40	9.97526E-69	2.97413E-154	
1.0E+23	1.89593E-10	1.27265E-10	5.73956E-11	5.26449E-12	9.92411E-14	3.69711E-17	3.79418E-27	1.41534E-42	2.33328E-71	6.90008E-157	

O2 COLUMN DENSITY

Table B. Total Photodissociation Rate Coefficients for the Process  $\text{H}_2\text{O}_2 + h\nu \rightarrow \text{OH} + \text{OH}$  for Wavelengths From 188.2 to 303 nm

	O3 COLUMN DENSITY									
	1.0E+12	2.0E+12	5.0E+12	1.0E+13	2.0E+13	5.0E+13	1.0E+14	2.0E+14	5.0E+14	1.0E+15
1.0E+17	1.59387E-04	1.59386E-04	1.59384E-04	1.59380E-04	1.59373E-04	1.59351E-04	1.59314E-04	1.59241E-04	1.59021E-04	1.58655E-04
2.0E+17	1.59386E-04	1.59386E-04	1.59384E-04	1.59380E-04	1.59373E-04	1.59350E-04	1.59314E-04	1.59240E-04	1.59020E-04	1.58655E-04
5.0E+17	1.59386E-04	1.59385E-04	1.59383E-04	1.59379E-04	1.59372E-04	1.59350E-04	1.59313E-04	1.59240E-04	1.59020E-04	1.58654E-04
1.0E+18	1.59385E-04	1.59384E-04	1.59382E-04	1.59378E-04	1.59371E-04	1.59349E-04	1.59312E-04	1.59239E-04	1.59019E-04	1.58653E-04
2.0E+18	1.59382E-04	1.59382E-04	1.59380E-04	1.59376E-04	1.59368E-04	1.59346E-04	1.59310E-04	1.59236E-04	1.59016E-04	1.58651E-04
5.0E+18	1.59376E-04	1.59375E-04	1.59373E-04	1.59369E-04	1.59362E-04	1.59340E-04	1.59303E-04	1.59230E-04	1.59010E-04	1.58644E-04
1.0E+19	1.59366E-04	1.59365E-04	1.59363E-04	1.59359E-04	1.59352E-04	1.59330E-04	1.59293E-04	1.59219E-04	1.59000E-04	1.58634E-04
2.0E+19	1.59347E-04	1.59346E-04	1.59344E-04	1.59340E-04	1.59333E-04	1.59311E-04	1.59274E-04	1.59200E-04	1.58981E-04	1.58615E-04
5.0E+19	1.59296E-04	1.59295E-04	1.59295E-04	1.59291E-04	1.59284E-04	1.59262E-04	1.59225E-04	1.59151E-04	1.58932E-04	1.58566E-04
1.0E+20	1.59230E-04	1.59229E-04	1.59227E-04	1.59223E-04	1.59216E-04	1.59194E-04	1.59157E-04	1.59084E-04	1.58864E-04	1.58498E-04
2.0E+20	1.59117E-04	1.59116E-04	1.59114E-04	1.59110E-04	1.59103E-04	1.59081E-04	1.59044E-04	1.58971E-04	1.58751E-04	1.58385E-04
5.0E+20	1.59015E-04	1.59014E-04	1.59012E-04	1.59008E-04	1.59001E-04	1.58979E-04	1.58942E-04	1.58869E-04	1.58649E-04	1.58284E-04
1.0E+21	1.58681E-04	1.58680E-04	1.58678E-04	1.58674E-04	1.58667E-04	1.58645E-04	1.58608E-04	1.58535E-04	1.58315E-04	1.57951E-04
2.0E+21	1.58161E-04	1.58160E-04	1.58158E-04	1.58154E-04	1.58147E-04	1.58125E-04	1.58088E-04	1.58015E-04	1.57796E-04	1.57431E-04
5.0E+21	1.56917E-04	1.56916E-04	1.56914E-04	1.56911E-04	1.56903E-04	1.56881E-04	1.56845E-04	1.56772E-04	1.56553E-04	1.56190E-04
1.0E+22	1.54846E-04	1.54845E-04	1.54843E-04	1.54839E-04	1.54832E-04	1.54810E-04	1.54774E-04	1.54701E-04	1.54484E-04	1.54127E-04
2.0E+22	1.51283E-04	1.51282E-04	1.51280E-04	1.51277E-04	1.51269E-04	1.51248E-04	1.51212E-04	1.51140E-04	1.50925E-04	1.50567E-04
5.0E+22	1.42514E-04	1.42513E-04	1.42511E-04	1.42508E-04	1.42501E-04	1.42480E-04	1.42445E-04	1.42375E-04	1.42166E-04	1.41818E-04
1.0E+23	1.30898E-04	1.30897E-04	1.30895E-04	1.30891E-04	1.30885E-04	1.30865E-04	1.30831E-04	1.30764E-04	1.30563E-04	1.30223E-04
2.0E+23	1.16527E-04	1.16527E-04	1.16525E-04	1.16522E-04	1.16515E-04	1.16498E-04	1.16465E-04	1.16402E-04	1.16213E-04	1.15899E-04
5.0E+23	1.00617E-04	1.00616E-04	1.00614E-04	1.00612E-04	1.00606E-04	1.00589E-04	1.00560E-04	1.00503E-04	1.00332E-04	1.00048E-04
1.0E+24	9.47553E-05	9.47547E-05	9.47531E-05	9.47504E-05	9.47450E-05	9.47288E-05	9.47019E-05	9.46480E-05	9.44867E-05	9.42188E-05
2.0E+24	9.25133E-05	9.25132E-05	9.25117E-05	9.25091E-05	9.25038E-05	9.24882E-05	9.24621E-05	9.24099E-05	9.23537E-05	9.19942E-05
5.0E+24	9.15194E-05	9.15188E-05	9.15173E-05	9.15147E-05	9.15096E-05	9.14942E-05	9.14685E-05	9.14172E-05	9.13636E-05	9.10085E-05
1.0E+25	9.13956E-05	9.13951E-05	9.13936E-05	9.13910E-05	9.13859E-05	9.13705E-05	9.13449E-05	9.12937E-05	9.11405E-05	9.08859E-05
2.0E+25	9.13912E-05	9.13907E-05	9.13892E-05	9.13866E-05	9.13815E-05	9.13661E-05	9.13405E-05	9.12894E-05	9.11361E-05	9.08815E-05
5.0E+25	9.13912E-05	9.13907E-05	9.13892E-05	9.13866E-05	9.13815E-05	9.13661E-05	9.13405E-05	9.12894E-05	9.11361E-05	9.08815E-05

O3 COLUMN DENSITY

Table B. Total Photodissociation Rate Coefficients for the Process  $\text{H}_2\text{O}_2 + h\nu \rightarrow \text{OH} + \text{OH}$  for Wavelengths From 188.2 to 303 nm (Contd)

	O3 COLUMN DENSITY									
	2.0E+15	5.0E+15	1.0E+16	2.0E+16	5.0E+16	1.0E+17	2.0E+17	5.0E+17	1.0E+18	2.0E+18
1.0E+17	1.57929E-04	1.55782E-04	1.52310E-04	1.45746E-04	1.28723E-04	1.07248E-04	8.02864E-05	4.71942E-05	2.81931E-05	1.39291E-05
2.0E+17	1.57928E-04	1.55781E-04	1.52310E-04	1.45746E-04	1.28723E-04	1.07248E-04	8.02862E-05	4.71940E-05	2.81930E-05	1.39290E-05
5.0E+17	1.57928E-04	1.55781E-04	1.52310E-04	1.45746E-04	1.28722E-04	1.07247E-04	8.02856E-05	4.71935E-05	2.81926E-05	1.39288E-05
1.0E+18	1.57927E-04	1.55779E-04	1.52308E-04	1.45744E-04	1.28721E-04	1.07246E-04	8.02846E-05	4.71927E-05	2.81919E-05	1.39284E-05
2.0E+18	1.57924E-04	1.55777E-04	1.52306E-04	1.45742E-04	1.28719E-04	1.07244E-04	8.02827E-05	4.71911E-05	2.81907E-05	1.39277E-05
5.0E+18	1.57918E-04	1.55771E-04	1.52299E-04	1.45736E-04	1.28713E-04	1.07238E-04	8.02770E-05	4.71853E-05	2.81871E-05	1.39255E-05
1.0E+19	1.57908E-04	1.55761E-04	1.52289E-04	1.45726E-04	1.28703E-04	1.07228E-04	8.02681E-05	4.71789E-05	2.81814E-05	1.39221E-05
2.0E+19	1.57831E-04	1.55742E-04	1.52270E-04	1.45707E-04	1.28685E-04	1.07211E-04	8.02516E-05	4.71651E-05	2.81709E-05	1.39158E-05
5.0E+19	1.57740E-04	1.55693E-04	1.52222E-04	1.45659E-04	1.28638E-04	1.07166E-04	8.02095E-05	4.71302E-05	2.81433E-05	1.38998E-05
1.0E+20	1.57772E-04	1.55625E-04	1.52154E-04	1.45592E-04	1.28573E-04	1.07103E-04	8.01518E-05	4.70826E-05	2.81082E-05	1.38779E-05
2.0E+20	1.57559E-04	1.55513E-04	1.52043E-04	1.45482E-04	1.28465E-04	1.07001E-04	8.00571E-05	4.70053E-05	2.80498E-05	1.38426E-05
5.0E+20	1.57558E-04	1.55412E-04	1.51943E-04	1.45384E-04	1.28374E-04	1.06918E-04	7.99879E-05	4.69599E-05	2.80235E-05	1.38297E-05
1.0E+21	1.57225E-04	1.55081E-04	1.51614E-04	1.45059E-04	1.28061E-04	1.06623E-04	7.97232E-05	4.67539E-05	2.78732E-05	1.37421E-05
2.0E+21	1.56706E-04	1.54565E-04	1.51102E-04	1.44555E-04	1.27560E-04	1.06175E-04	7.93277E-05	4.64582E-05	2.76662E-05	1.36243E-05
5.0E+21	1.55467E-04	1.53333E-04	1.49882E-04	1.43358E-04	1.26445E-04	1.05132E-04	7.84280E-05	4.58194E-05	2.72420E-05	1.33956E-05
1.0E+22	1.53404E-04	1.51281E-04	1.47849E-04	1.41362E-04	1.24553E-04	1.03389E-04	7.69211E-05	4.47408E-05	2.65175E-05	1.29974E-05
2.0E+22	1.49856E-04	1.47755E-04	1.44359E-04	1.37942E-04	1.21327E-04	1.00443E-04	7.44119E-05	4.30054E-05	2.53946E-05	1.24042E-05
5.0E+22	1.41127E-04	1.39085E-04	1.35785E-04	1.29557E-04	1.13463E-04	9.33263E-05	6.84478E-05	3.90351E-05	2.29249E-05	1.11594E-05
1.0E+23	1.29566E-04	1.27606E-04	1.24442E-04	1.18474E-04	1.03104E-04	8.39956E-05	6.05861E-05	3.39183E-05	1.97384E-05	9.52302E-06
2.0E+23	1.15273E-04	1.12435E-04	1.10466E-04	1.04876E-04	9.05393E-05	7.28821E-05	5.17291E-05	2.83863E-05	1.64855E-05	7.93577E-06
5.0E+23	9.94636E-05	9.73186E-05	9.51356E-05	9.00952E-05	7.72450E-05	6.16097E-05	4.32964E-05	2.39161E-05	1.41448E-05	6.88049E-06
1.0E+24	9.36864E-05	9.21162E-05	8.95869E-05	8.48393E-05	7.27602E-05	5.81211E-05	4.10755E-05	2.30816E-05	1.37856E-05	6.71577E-06
2.0E+24	9.14786E-05	8.91582E-05	8.75092E-05	8.29128E-05	7.12219E-05	5.70570E-05	4.05524E-05	2.29988E-05	1.37732E-05	6.71252E-06
5.0E+24	9.05015E-05	8.91064E-05	8.65982E-05	8.20783E-05	7.05801E-05	5.66424E-05	4.03767E-05	2.29854E-05	1.37729E-05	6.71251E-06
1.0E+25	9.03800E-05	8.81881E-05	8.64851E-05	8.19749E-05	7.05012E-05	5.65921E-05	4.03582E-05	2.29841E-05	1.37729E-05	6.71251E-06
2.0E+25	9.03757E-05	8.81839E-05	8.64811E-05	8.19713E-05	7.04984E-05	5.65903E-05	4.03575E-05	2.28840E-05	1.37729E-05	6.71251E-06
5.0E+25	9.03757E-05	8.81839E-05	8.64811E-05	8.19713E-05	7.04984E-05	5.65903E-05	4.03575E-05	2.28840E-05	1.37729E-05	6.71251E-06

Table IV. Total Photoassociation Rate Coefficients for the Process  $\text{H}_2\text{O}_2 + h\nu \rightarrow \text{OH} + \text{OH}$  for Wave-  
lengths From 133.2 to 305 nm (Contd)

		O3 COLUMN DENSITY							
		5.0E+18	1.0E+19	2.0E+19	5.0E+19	1.0E+20	2.0E+20	5.0E+20	1.0E+21
1.0E+17	3.06840E-06	3.96455E-07	1.00025E-08	3.00632E-13	1.72372E-20	9.76796E-35	2.44366E-77	3.00780-148	
2.0E+17	3.06839E-06	3.98494E-07	1.00025E-08	3.00632E-13	1.72372E-20	9.76795E-35	2.44365E-77	3.00780-148	
5.0E+17	3.06834E-06	3.98489E-07	1.00024E-08	3.00630E-13	1.72371E-20	9.76750E-35	2.44364E-77	3.00779-148	
1.0E+18	3.06825E-06	3.98480E-07	1.00023E-08	3.00628E-13	1.72369E-20	9.76782E-35	2.44362E-77	3.00776-148	
2.0E+18	3.05808E-06	3.98454E-07	1.00021E-08	3.00523E-13	1.72368E-20	9.76765E-35	2.44358E-77	3.00771-148	
5.0E+18	3.08758E-06	3.98416E-07	1.00014E-08	3.00507E-13	1.72357E-20	9.76717E-35	2.44347E-77	3.00757-148	
1.0E+19	3.06679E-06	3.98339E-07	1.00003E-08	3.00582E-13	1.72341E-20	9.76635E-35	2.44327E-77	3.00733-148	
2.0E+19	3.06532E-06	3.98192E-07	9.99808E-09	3.00531E-13	1.72311E-20	9.76473E-35	2.44288E-77	3.00684-148	
5.0E+19	3.06150E-06	3.97797E-07	9.99183E-09	3.00381E-13	1.72219E-20	9.75986E-35	2.44171E-77	3.00540-148	
1.0E+20	3.05619E-06	3.97223E-07	9.98207E-09	3.00134E-13	1.72067E-20	9.75178E-35	2.43976E-77	3.00299-148	
2.0E+20	3.04744E-06	3.96238E-07	9.96411E-09	2.99551E-13	1.71767E-20	9.73577E-35	2.43589E-77	2.99822-148	
5.0E+20	3.02346E-06	3.93483E-07	9.91092E-09	2.99599E-13	1.71756E-20	9.73571E-35	2.43589E-77	2.99822-148	
1.0E+21	2.99480E-06	3.90040E-07	9.83867E-09	2.95988E-13	1.69486E-20	9.61232E-35	2.40587E-77	2.96130-148	
2.0E+21	2.94191E-06	3.83712E-07	9.70263E-09	2.91766E-13	1.66824E-20	9.46598E-35	2.37008E-77	2.91741-148	
5.0E+21	2.84524E-06	3.71293E-07	9.40340E-09	2.81018E-13	1.59618E-20	9.05682E-35	2.26929E-77	2.79392-148	
1.0E+22	2.70660E-06	3.53507E-07	8.96473E-09	2.64835E-13	1.48690E-20	8.43140E-35	2.11448E-77	2.60398-148	
2.0E+22	2.43341E-06	3.19813E-07	8.15846E-09	2.35940E-13	1.29412E-20	7.32892E-35	1.84046E-77	2.25631-148	
5.0E+22	2.04965E-06	2.67769E-07	6.73786E-09	1.76935E-13	8.76265E-21	4.87091E-35	1.22464E-77	1.50709-148	
1.0E+23	1.69456E-06	2.20257E-07	5.43161E-09	1.21507E-13	4.78734E-21	2.51090E-35	6.30669E-78	7.73536-149	
2.0E+23	1.46600E-06	1.88854E-07	4.52037E-09	8.03634E-14	1.75909E-21	6.90188E-36	1.71700E-78	2.08641-149	
5.0E+23	1.42056E-06	1.80846E-07	4.24356E-09	6.60542E-14	6.63379E-22	2.12690E-37	3.75249E-80	4.40693-151	
1.0E+24	1.41973E-06	1.80846E-07	4.23803E-09	6.57690E-14	6.40503E-22	7.27530E-38	3.02906E-81	3.46487-152	
2.0E+24	1.41973E-06	1.80846E-07	4.23803E-09	6.57690E-14	6.40503E-22	7.27530E-38	3.02906E-81	3.46487-152	
5.0E+24	1.41973E-06	1.80846E-07	4.23803E-09	6.57690E-14	6.40503E-22	7.27530E-38	3.02906E-81	3.46487-152	
1.0E+25	1.41973E-06	1.80846E-07	4.23803E-09	6.57690E-14	6.40503E-22	7.27530E-38	3.02906E-81	3.46487-152	
2.0E+25	1.41973E-06	1.80846E-07	4.23803E-09	6.57690E-14	6.40503E-22	7.27530E-38	3.02906E-81	3.46487-152	
5.0E+25	1.41973E-06	1.80846E-07	4.23803E-09	6.57690E-14	6.40503E-22	7.27530E-38	3.02906E-81	3.46487-152	

O2 COLUMN DENSITY

AD-A157 122

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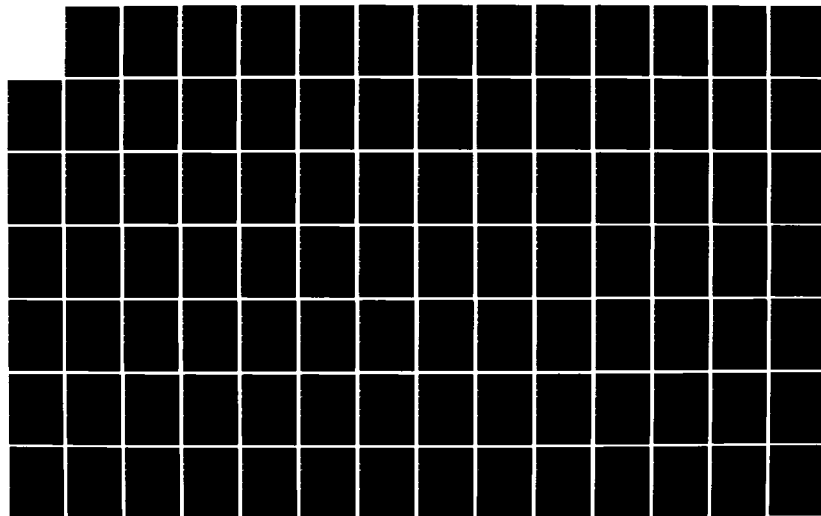
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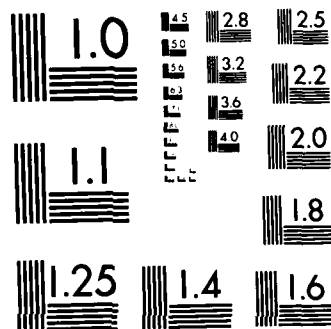
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Table B10. Total Photodissociation Rate Coefficients for the Process  $\text{NO}_2 + h\nu \rightarrow \text{NO} + \text{O}(^1\text{D})$  for Wavelengths From 190 to 420 nm

		O3 COLUMN DENSITY									
		1.0E+14	2.0E+14	5.0E+14	1.0E+15	2.0E+15	5.0E+15	1.0E+16	2.0E+16	5.0E+16	1.0E+17
1.0E+19	1.51038E-02	1.51038E-02	1.51036E-02	1.51033E-02	1.51027E-02	1.51008E-02	1.51008E-02	1.50978E-02	1.50920E-02	1.50759E-02	1.50530E-02
2.0E+19	1.51038E-02	1.51038E-02	1.51036E-02	1.51033E-02	1.51026E-02	1.51026E-02	1.51008E-02	1.50978E-02	1.50920E-02	1.50759E-02	1.50530E-02
5.0E+19	1.51038E-02	1.51037E-02	1.51035E-02	1.51032E-02	1.51026E-02	1.51026E-02	1.51008E-02	1.50978E-02	1.50920E-02	1.50759E-02	1.50530E-02
1.0E+20	1.51037E-02	1.51037E-02	1.51035E-02	1.51032E-02	1.51026E-02	1.51026E-02	1.51007E-02	1.50977E-02	1.50919E-02	1.50759E-02	1.50529E-02
2.0E+20	1.51037E-02	1.51036E-02	1.51034E-02	1.51031E-02	1.51025E-02	1.51025E-02	1.51007E-02	1.50977E-02	1.50918E-02	1.50758E-02	1.50529E-02
5.0E+20	1.51035E-02	1.51035E-02	1.51033E-02	1.51030E-02	1.51024E-02	1.51024E-02	1.51005E-02	1.50975E-02	1.50917E-02	1.50757E-02	1.50528E-02
1.0E+21	1.51033E-02	1.51032E-02	1.51030E-02	1.51027E-02	1.51021E-02	1.51003E-02	1.51003E-02	1.50973E-02	1.50914E-02	1.50754E-02	1.50525E-02
2.0E+21	1.51028E-02	1.51027E-02	1.51025E-02	1.51022E-02	1.51016E-02	1.50998E-02	1.50998E-02	1.50968E-02	1.50910E-02	1.50750E-02	1.50521E-02
5.0E+21	1.51014E-02	1.51013E-02	1.51011E-02	1.51008E-02	1.51002E-02	1.50984E-02	1.50984E-02	1.50954E-02	1.50897E-02	1.50737E-02	1.50510E-02
1.0E+22	1.50991E-02	1.50991E-02	1.50989E-02	1.50986E-02	1.50980E-02	1.50962E-02	1.50962E-02	1.50932E-02	1.50875E-02	1.50717E-02	1.50491E-02
2.0E+22	1.50951E-02	1.50950E-02	1.50948E-02	1.50945E-02	1.50939E-02	1.50922E-02	1.50922E-02	1.50892E-02	1.50836E-02	1.50680E-02	1.50457E-02
5.0E+22	1.50847E-02	1.50847E-02	1.50845E-02	1.50842E-02	1.50836E-02	1.50819E-02	1.50819E-02	1.50791E-02	1.50737E-02	1.50587E-02	1.50373E-02
1.0E+23	1.50712E-02	1.50711E-02	1.50709E-02	1.50707E-02	1.50701E-02	1.50685E-02	1.50685E-02	1.50658E-02	1.50607E-02	1.50465E-02	1.50263E-02
2.0E+23	1.50543E-02	1.50543E-02	1.50541E-02	1.50538E-02	1.50533E-02	1.50519E-02	1.50519E-02	1.50494E-02	1.50447E-02	1.50316E-02	1.50131E-02
5.0E+23	1.50364E-02	1.50364E-02	1.50362E-02	1.50360E-02	1.50356E-02	1.50342E-02	1.50342E-02	1.50321E-02	1.50279E-02	1.50164E-02	1.49999E-02
1.0E+24	1.50309E-02	1.50309E-02	1.50308E-02	1.50306E-02	1.50301E-02	1.50289E-02	1.50289E-02	1.50268E-02	1.50229E-02	1.50120E-02	1.49964E-02
2.0E+24	1.50294E-02	1.50294E-02	1.50293E-02	1.50291E-02	1.50287E-02	1.50275E-02	1.50275E-02	1.50255E-02	1.50216E-02	1.50110E-02	1.49956E-02
5.0E+24	1.50289E-02	1.50289E-02	1.50288E-02	1.50286E-02	1.50282E-02	1.50270E-02	1.50270E-02	1.50250E-02	1.50212E-02	1.50106E-02	1.49954E-02
1.0E+25	1.50289E-02	1.50288E-02	1.50287E-02	1.50285E-02	1.50281E-02	1.50269E-02	1.50269E-02	1.50250E-02	1.50211E-02	1.50106E-02	1.49954E-02

O2 COLUMN DENSITY

Table B10. Total Photodissociation Rate Coefficients for the Process  
 $\text{NO}_2 + h\nu \rightarrow \text{NO} + \text{O}({}^1\text{D})$  for Wavelengths From 190 to 420 nm (Contd)

03 COLUMN DENSITY				
	2.0E+17	5.0E+17	1.0E+18	5.0E+18
1.0E+19	1.50170E-02	1.49479E-02	1.48792E-02	1.47941E-02
2.0E+19	1.50170E-02	1.49479E-02	1.48791E-02	1.47941E-02
5.0E+19	1.50170E-02	1.49479E-02	1.48791E-02	1.47941E-02
1.0E+20	1.50170E-02	1.49479E-02	1.48791E-02	1.47940E-02
2.0E+20	1.50169E-02	1.49478E-02	1.48791E-02	1.47940E-02
5.0E+20	1.50168E-02	1.49478E-02	1.48790E-02	1.47940E-02
1.0E+21	1.50166E-02	1.49476E-02	1.48789E-02	1.47940E-02
2.0E+21	1.50162E-02	1.49473E-02	1.48788E-02	1.47939E-02
5.0E+21	1.50153E-02	1.49467E-02	1.48784E-02	1.47937E-02
1.0E+22	1.50137E-02	1.49456E-02	1.48777E-02	1.47933E-02
2.0E+22	1.50108E-02	1.49437E-02	1.48765E-02	1.47928E-02
5.0E+22	1.50038E-02	1.49391E-02	1.48738E-02	1.47915E-02
1.0E+23	1.49847E-02	1.49333E-02	1.48704E-02	1.47899E-02
2.0E+23	1.49840E-02	1.49268E-02	1.48668E-02	1.47883E-02
5.0E+23	1.49739E-02	1.49214E-02	1.48641E-02	1.47872E-02
1.0E+24	1.49711E-02	1.49204E-02	1.48637E-02	1.47870E-02
2.0E+24	1.49710E-02	1.49204E-02	1.48637E-02	1.47870E-02
5.0E+24	1.49710E-02	1.49204E-02	1.48637E-02	1.47870E-02
1.0E+25	1.49710E-02	1.49204E-02	1.48637E-02	1.47870E-02

02 COLUMN DENSITY

Table B11. Total Photodissociation Rate Coefficients  
for the Process  $\text{NO}_3 + h\nu \rightarrow \text{NO} + \text{O}_2$  for Wavelengths  
From 450 to 680 nm

1.0E+14	7.04137E-02
2.0E+14	7.04137E-02
5.0E+14	7.04136E-02
1.0E+15	7.04135E-02
2.0E+15	7.04133E-02
5.0E+15	7.04126E-02
1.0E+16	7.04115E-02
2.0E+16	7.04093E-02
5.0E+16	7.04027E-02
1.0E+17	7.03918E-02
2.0E+17	7.03699E-02
5.0E+17	7.03042E-02
1.0E+18	7.01948E-02
2.0E+18	6.99767E-02
5.0E+18	6.93271E-02
1.0E+19	6.82601E-02
2.0E+19	6.61829E-02
5.0E+19	6.03813E-02
1.0E+20	5.19884E-02
2.0E+20	3.90163E-02
5.0E+20	1.81717E-02
1.0E+21	6.74160E-03

03 COLUMN DENSITY

Table B12. Total Photodissociation Rate Coefficients for the Process  $N_2O + h\nu \rightarrow N_2 + O(^1D)$  for Wavelengths From 190 to 315 nm

O3 COLUMN DENSITY

	1.0E+11	2.0E+11	5.0E+11	1.0E+12	2.0E+12	5.0E+12	1.0E+13	2.0E+13	5.0E+13	1.0E+14
1.0E+17	7.76688E-07	7.76688E-07	7.76687E-07	7.76687E-07	7.76687E-07	7.76685E-07	7.76683E-07	7.76678E-07	7.76665E-07	7.76642E-07
2.0E+17	7.76675E-07	7.76675E-07	7.76675E-07	7.76674E-07	7.76674E-07	7.76673E-07	7.76670E-07	7.76668E-07	7.76652E-07	7.76629E-07
5.0E+17	7.76637E-07	7.76637E-07	7.76636E-07	7.76636E-07	7.76636E-07	7.76634E-07	7.76632E-07	7.76628E-07	7.76614E-07	7.76591E-07
1.0E+18	7.76573E-07	7.76573E-07	7.76573E-07	7.76573E-07	7.76572E-07	7.76571E-07	7.76569E-07	7.76564E-07	7.76550E-07	7.76527E-07
2.0E+18	7.76447E-07	7.76447E-07	7.76446E-07	7.76446E-07	7.76446E-07	7.76444E-07	7.76442E-07	7.76438E-07	7.76424E-07	7.76401E-07
5.0E+18	7.76072E-07	7.76072E-07	7.76071E-07	7.76071E-07	7.76071E-07	7.76069E-07	7.76067E-07	7.76062E-07	7.76049E-07	7.76026E-07
1.0E+19	7.75460E-07	7.75460E-07	7.75460E-07	7.75460E-07	7.75459E-07	7.75458E-07	7.75456E-07	7.75451E-07	7.75437E-07	7.75414E-07
2.0E+19	7.74287E-07	7.74287E-07	7.74287E-07	7.74287E-07	7.74286E-07	7.74285E-07	7.74282E-07	7.74278E-07	7.74264E-07	7.74241E-07
5.0E+19	7.71086E-07	7.71086E-07	7.71086E-07	7.71085E-07	7.71085E-07	7.71084E-07	7.71081E-07	7.71077E-07	7.71063E-07	7.71040E-07
1.0E+20	7.66513E-07	7.66513E-07	7.66512E-07	7.66512E-07	7.66512E-07	7.66510E-07	7.66508E-07	7.66504E-07	7.66490E-07	7.66467E-07
2.0E+20	7.59021E-07	7.59021E-07	7.59021E-07	7.59021E-07	7.59020E-07	7.59019E-07	7.59017E-07	7.59012E-07	7.58999E-07	7.58976E-07
5.0E+20	7.58248E-07	7.58248E-07	7.58248E-07	7.58248E-07	7.58247E-07	7.58246E-07	7.58244E-07	7.58239E-07	7.58226E-07	7.58203E-07
1.0E+21	7.41207E-07	7.41207E-07	7.41207E-07	7.41207E-07	7.41206E-07	7.41205E-07	7.41203E-07	7.41198E-07	7.41185E-07	7.41163E-07
2.0E+21	7.20595E-07	7.20595E-07	7.20595E-07	7.20594E-07	7.20594E-07	7.20593E-07	7.20590E-07	7.20586E-07	7.20573E-07	7.20551E-07
5.0E+21	6.88458E-07	6.88458E-07	6.88458E-07	6.88458E-07	6.88457E-07	6.88456E-07	6.88454E-07	6.88450E-07	6.88437E-07	6.88416E-07
1.0E+22	6.30746E-07	6.30746E-07	6.30746E-07	6.30746E-07	6.30746E-07	6.30744E-07	6.30742E-07	6.30739E-07	6.30727E-07	6.30707E-07
2.0E+22	5.60380E-07	5.60380E-07	5.60380E-07	5.60380E-07	5.60380E-07	5.60379E-07	5.60377E-07	5.60375E-07	5.60363E-07	5.60345E-07
5.0E+22	4.41787E-07	4.41787E-07	4.41787E-07	4.41787E-07	4.41787E-07	4.41786E-07	4.41784E-07	4.41781E-07	4.41773E-07	4.41758E-07
1.0E+23	2.74667E-07	2.74667E-07	2.74667E-07	2.74667E-07	2.74667E-07	2.74666E-07	2.74665E-07	2.74663E-07	2.74657E-07	2.74646E-07
2.0E+23	1.31564E-07	1.31564E-07	1.31564E-07	1.31564E-07	1.31564E-07	1.31563E-07	1.31563E-07	1.31561E-07	1.31557E-07	1.31551E-07
5.0E+23	3.86021E-08	3.86021E-08	3.86021E-08	3.86020E-08	3.86020E-08	3.86018E-08	3.86014E-08	3.86009E-08	3.85988E-08	3.85955E-08
1.0E+24	1.89016E-08	1.89016E-08	1.89016E-08	1.89015E-08	1.89015E-08	1.89013E-08	1.89011E-08	1.89006E-08	1.88990E-08	1.88965E-08
2.0E+24	1.82305E-08	1.82305E-08	1.82305E-08	1.82305E-08	1.82305E-08	1.82303E-08	1.82301E-08	1.82296E-08	1.82281E-08	1.82257E-08
5.0E+24	1.81457E-08	1.81457E-08	1.81457E-08	1.81456E-08	1.81456E-08	1.81455E-08	1.81452E-08	1.81447E-08	1.81433E-08	1.81409E-08
1.0E+25	1.81365E-08	1.81365E-08	1.81365E-08	1.81364E-08	1.81364E-08	1.81362E-08	1.81360E-08	1.81355E-08	1.81341E-08	1.81317E-08
2.0E+25	1.81362E-08	1.81361E-08	1.81361E-08	1.81361E-08	1.81361E-08	1.81359E-08	1.81357E-08	1.81352E-08	1.81338E-08	1.81314E-08

O2 COLUMN DENSITY

Table B12. Total Photodissociation Rate Coefficients for the Process  $N_2O + h\nu \rightarrow N_2 + O(^1D)$  for Wavelengths From 190 to 315 nm (Contd)

		O3 COLUMN DENSITY									
		2.0E+14	5.0E+14	1.0E+15	2.0E+15	5.0E+15	1.0E+16	2.0E+16	5.0E+16	1.0E+17	2.0E+17
1.0E+17	7.76596E-07	7.76458E-07	7.76229E-07	7.75772E-07	7.74405E-07	7.72142E-07	7.67675E-07	7.54704E-07	7.34323E-07	6.97141E-07	
2.0E+17	7.76583E-07	7.76446E-07	7.76217E-07	7.75759E-07	7.74392E-07	7.72129E-07	7.67662E-07	7.54692E-07	7.34311E-07	6.97129E-07	
5.0E+17	7.76545E-07	7.76407E-07	7.76178E-07	7.75721E-07	7.74354E-07	7.72091E-07	7.67624E-07	7.54654E-07	7.34274E-07	6.97094E-07	
1.0E+18	7.76481E-07	7.76344E-07	7.76115E-07	7.75658E-07	7.74291E-07	7.72028E-07	7.67561E-07	7.54592E-07	7.34214E-07	6.97036E-07	
2.0E+18	7.76355E-07	7.76218E-07	7.75989E-07	7.75531E-07	7.74164E-07	7.71902E-07	7.67436E-07	7.54469E-07	7.34093E-07	6.96921E-07	
5.0E+18	7.75980E-07	7.75843E-07	7.75614E-07	7.75157E-07	7.73790E-07	7.71529E-07	7.67064E-07	7.54102E-07	7.33735E-07	6.96579E-07	
1.0E+19	7.75369E-07	7.75231E-07	7.75003E-07	7.74546E-07	7.73180E-07	7.70920E-07	7.66459E-07	7.53505E-07	7.33151E-07	6.96021E-07	
2.0E+19	7.74196E-07	7.74058E-07	7.73830E-07	7.73374E-07	7.72010E-07	7.69752E-07	7.65296E-07	7.52358E-07	7.32030E-07	6.94950E-07	
5.0E+19	7.70995E-07	7.70858E-07	7.70630E-07	7.70175E-07	7.68816E-07	7.66566E-07	7.62124E-07	7.49229E-07	7.28972E-07	6.92028E-07	
1.0E+20	7.66422E-07	7.66286E-07	7.66059E-07	7.65606E-07	7.64253E-07	7.62013E-07	7.57592E-07	7.44758E-07	7.24601E-07	6.87850E-07	
2.0E+20	7.58931E-07	7.58796E-07	7.58571E-07	7.58121E-07	7.56778E-07	7.54555E-07	7.50168E-07	7.37433E-07	7.17439E-07	6.81002E-07	
5.0E+20	7.58158E-07	7.58023E-07	7.57799E-07	7.57350E-07	7.56008E-07	7.53788E-07	7.49405E-07	7.36686E-07	7.16715E-07	6.80321E-07	
1.0E+21	7.41119E-07	7.40986E-07	7.40765E-07	7.40324E-07	7.39005E-07	7.36824E-07	7.32518E-07	7.20026E-07	7.00426E-07	6.64748E-07	
2.0E+21	7.20508E-07	7.20378E-07	7.20162E-07	7.19731E-07	7.18400E-07	7.16303E-07	7.12093E-07	6.99879E-07	6.80733E-07	6.45925E-07	
5.0E+21	6.88375E-07	6.88249E-07	6.88041E-07	6.87625E-07	6.86381E-07	6.84233E-07	6.80263E-07	6.68501E-07	6.50088E-07	6.16682E-07	
1.0E+22	6.30668E-07	6.30551E-07	6.30356E-07	6.29967E-07	6.28803E-07	6.26879E-07	6.23086E-07	6.12112E-07	5.94981E-07	5.64024E-07	
2.0E+22	5.60309E-07	5.60202E-07	5.60024E-07	5.59669E-07	5.58608E-07	5.56855E-07	5.53400E-07	5.43429E-07	5.27919E-07	5.00042E-07	
5.0E+22	4.41729E-07	4.41641E-07	4.41494E-07	4.41202E-07	4.40339E-07	4.38888E-07	4.36054E-07	4.27910E-07	4.15340E-07	3.92990E-07	
1.0E+23	2.74625E-07	2.74563E-07	2.74459E-07	2.74251E-07	2.73632E-07	2.72611E-07	2.70613E-07	2.64931E-07	2.56323E-07	2.41429E-07	
2.0E+23	1.31538E-07	1.31500E-07	1.31436E-07	1.31308E-07	1.30929E-07	1.30307E-07	1.29099E-07	1.25731E-07	1.20814E-07	1.12767E-07	
5.0E+23	3.85889E-08	3.85692E-08	3.85364E-08	3.84712E-08	3.82778E-08	3.79634E-08	3.73623E-08	3.57555E-08	3.35931E-08	3.05016E-08	
1.0E+24	1.88914E-08	1.88762E-08	1.88508E-08	1.88004E-08	1.86514E-08	1.84099E-08	1.79518E-08	1.67513E-08	1.52016E-08	1.31551E-08	
2.0E+24	1.82208E-08	1.82063E-08	1.81822E-08	1.81341E-08	1.79921E-08	1.77620E-08	1.73255E-08	1.61820E-08	1.47065E-08	1.27561E-08	
5.0E+24	1.81361E-08	1.81218E-08	1.80980E-08	1.80507E-08	1.79198E-08	1.76841E-08	1.72539E-08	1.61266E-08	1.46702E-08	1.27403E-08	
1.0E+25	1.81269E-08	1.81127E-08	1.80889E-08	1.80417E-08	1.79020E-08	1.76756E-08	1.72462E-08	1.61207E-08	1.46684E-08	1.27388E-08	
2.0E+25	1.81266E-08	1.81123E-08	1.80886E-08	1.80413E-08	1.79017E-08	1.76753E-08	1.72459E-08	1.61205E-08	1.46663E-08	1.27387E-08	

Table B12. Total Photodissociation Rate Coefficients for the Process  $N_2O + h\nu \rightarrow N_2 + O(^1D)$  for Wavelengths From 190 to 315 nm (Contd)

O3 COLUMN DENSITY							
	5.0E+17	1.0E+18	2.0E+18	5.0E+18	1.0E+19	2.0E+19	5.0E+19
1.0E+17	6.03763E-07	4.83551E-07	3.18465E-07	9.86375E-08	1.63090E-08	1.07089E-09	8.59453E-11
2.0E+17	6.03753E-07	4.83543E-07	3.18460E-07	9.86362E-08	1.63089E-08	1.07089E-09	8.59453E-11
5.0E+17	6.03723E-07	4.83519E-07	3.18444E-07	9.86322E-08	1.63084E-08	1.07088E-09	8.59453E-11
1.0E+18	6.03672E-07	4.83479E-07	3.18419E-07	9.86255E-08	1.63077E-08	1.07087E-09	8.59453E-11
2.0E+18	6.03572E-07	4.83399E-07	3.18368E-07	9.86123E-08	1.63062E-08	1.07085E-09	8.59453E-11
5.0E+18	6.03273E-07	4.83161E-07	3.18217E-07	9.85730E-08	1.63018E-08	1.07078E-09	8.59453E-11
1.0E+19	6.02787E-07	4.82774E-07	3.17971E-07	9.85087E-08	1.62946E-08	1.07066E-09	8.59453E-11
2.0E+19	6.01853E-07	4.82030E-07	3.17497E-07	9.83847E-08	1.62806E-08	1.07044E-09	8.59453E-11
5.0E+19	5.99303E-07	4.79995E-07	3.16199E-07	9.80421E-08	1.62413E-08	1.06979E-09	8.59453E-11
1.0E+20	5.95653E-07	4.77078E-07	3.14330E-07	9.75427E-08	1.61828E-08	1.06877E-09	8.59453E-11
2.0E+20	5.89662E-07	4.72279E-07	3.11242E-07	9.67042E-08	1.60817E-08	1.06692E-09	8.59452E-11
5.0E+20	5.89032E-07	4.71844E-07	3.10977E-07	9.66372E-08	1.60738E-08	1.06678E-09	8.59452E-11
1.0E+21	5.75467E-07	4.60915E-07	3.03913E-07	9.46837E-08	1.58296E-08	1.06198E-09	8.59451E-11
2.0E+21	5.59003E-07	4.47700E-07	2.95339E-07	9.22722E-08	1.55172E-08	1.05539E-09	8.59449E-11
5.0E+21	5.33511E-07	4.27298E-07	2.82119E-07	8.85198E-08	1.50175E-08	1.04420E-09	8.59446E-11
1.0E+22	4.87436E-07	3.90206E-07	2.57815E-07	8.13909E-08	1.40144E-08	1.01943E-09	8.59437E-11
2.0E+22	4.31625E-07	3.45375E-07	2.28419E-07	7.26317E-08	1.27358E-08	9.85761E-10	8.59425E-11
5.0E+22	3.38947E-07	2.71525E-07	1.80395E-07	5.63839E-08	1.06352E-08	9.29097E-10	8.59403E-11
1.0E+23	2.06846E-07	1.65135E-07	1.09845E-07	3.63482E-08	7.14610E-09	8.25112E-10	8.59359E-11
2.0E+23	9.55816E-08	7.61533E-08	5.11481E-08	1.79497E-08	4.17913E-09	7.33719E-10	8.59318E-11
5.0E+23	2.52507E-08	2.03050E-08	1.43418E-08	6.21662E-09	2.22475E-09	6.70637E-10	8.59289E-11
1.0E+24	1.02400E-08	8.04676E-09	5.85509E-09	3.22418E-09	1.67355E-09	6.50942E-10	8.59279E-11
2.0E+24	9.95878E-09	7.83253E-09	5.70855E-09	3.17142E-09	1.66353E-09	6.50572E-10	8.59278E-11
5.0E+24	9.95734E-09	7.83247E-09	5.70855E-09	3.17142E-09	1.66353E-09	6.50572E-10	8.59278E-11
1.0E+25	9.95724E-09	7.83247E-09	5.70855E-09	3.17142E-09	1.66353E-09	6.50572E-10	8.59278E-11
2.0E+25	9.95723E-09	7.83247E-09	5.70855E-09	3.17142E-09	1.66353E-09	6.50572E-10	8.59278E-11

O2 COLUMN DENSITY

Table B13. Total Photodissociation Rate Coefficients for the Process  $N_2O_5 + h\nu \rightarrow NO_2 + NO_2 + O$  for Wavelengths From 210 to 380 nm

	O3 COLUMN DENSITY									
	1.0E+11	2.0E+11	5.0E+11	1.0E+12	2.0E+12	5.0E+12	1.0E+13	2.0E+13	5.0E+13	1.0E+14
1.0E+17	6.92337E-04	6.92337E-04	6.92336E-04	6.92334E-04	6.92331E-04	6.92323E-04	6.92309E-04	6.92281E-04	6.92198E-04	6.92059E-04
2.0E+17	6.92337E-04	6.92336E-04	6.92335E-04	6.92334E-04	6.92331E-04	6.92323E-04	6.92309E-04	6.92281E-04	6.92198E-04	6.92058E-04
5.0E+17	6.92336E-04	6.92336E-04	6.92335E-04	6.92333E-04	6.92331E-04	6.92322E-04	6.92308E-04	6.92280E-04	6.92197E-04	6.92058E-04
1.0E+18	6.92335E-04	6.92334E-04	6.92334E-04	6.92332E-04	6.92329E-04	6.92321E-04	6.92307E-04	6.92279E-04	6.92196E-04	6.92056E-04
2.0E+18	6.92332E-04	6.92332E-04	6.92331E-04	6.92330E-04	6.92327E-04	6.92319E-04	6.92305E-04	6.92277E-04	6.92193E-04	6.92054E-04
5.0E+18	6.92326E-04	6.92325E-04	6.92324E-04	6.92323E-04	6.92320E-04	6.92312E-04	6.92298E-04	6.92270E-04	6.92187E-04	6.92047E-04
1.0E+19	6.92314E-04	6.92314E-04	6.92313E-04	6.92312E-04	6.92309E-04	6.92300E-04	6.92287E-04	6.92259E-04	6.92175E-04	6.92036E-04
2.0E+19	6.92291E-04	6.92291E-04	6.92290E-04	6.92289E-04	6.92286E-04	6.92278E-04	6.92264E-04	6.92236E-04	6.92152E-04	6.92013E-04
5.0E+19	6.92223E-04	6.92222E-04	6.92222E-04	6.92220E-04	6.92217E-04	6.92209E-04	6.92195E-04	6.92167E-04	6.92084E-04	6.91944E-04
1.0E+20	6.92108E-04	6.92108E-04	6.92107E-04	6.92106E-04	6.92103E-04	6.92095E-04	6.92081E-04	6.92053E-04	6.91969E-04	6.91830E-04
2.0E+20	6.91880E-04	6.91880E-04	6.91879E-04	6.91877E-04	6.91875E-04	6.91866E-04	6.91852E-04	6.91824E-04	6.91741E-04	6.91603E-04
5.0E+20	6.91195E-04	6.91195E-04	6.91194E-04	6.91193E-04	6.91190E-04	6.91182E-04	6.91168E-04	6.91140E-04	6.91057E-04	6.90917E-04
1.0E+21	6.90058E-04	6.90057E-04	6.90057E-04	6.90055E-04	6.90052E-04	6.90044E-04	6.90030E-04	6.90002E-04	6.89919E-04	6.89780E-04
2.0E+21	6.87794E-04	6.87793E-04	6.87793E-04	6.87791E-04	6.87788E-04	6.87780E-04	6.87766E-04	6.87738E-04	6.87655E-04	6.87516E-04
5.0E+21	6.81093E-04	6.81093E-04	6.81092E-04	6.81090E-04	6.81088E-04	6.81079E-04	6.81066E-04	6.81038E-04	6.80955E-04	6.80817E-04
1.0E+22	6.70223E-04	6.70222E-04	6.70222E-04	6.70220E-04	6.70217E-04	6.70209E-04	6.70195E-04	6.70168E-04	6.70086E-04	6.69949E-04
2.0E+22	6.49550E-04	6.49550E-04	6.49549E-04	6.49548E-04	6.49545E-04	6.49537E-04	6.49524E-04	6.49497E-04	6.49416E-04	6.49281E-04
5.0E+22	5.95214E-04	5.95214E-04	5.95213E-04	5.95212E-04	5.95210E-04	5.95202E-04	5.95189E-04	5.95163E-04	5.95086E-04	5.94957E-04
1.0E+23	5.25402E-04	5.25402E-04	5.25401E-04	5.25400E-04	5.25398E-04	5.25390E-04	5.25378E-04	5.25354E-04	5.25281E-04	5.25160E-04
2.0E+23	4.37587E-04	4.37587E-04	4.37586E-04	4.37585E-04	4.37583E-04	4.37576E-04	4.37565E-04	4.37543E-04	4.37477E-04	4.37367E-04
5.0E+23	3.45059E-04	3.45059E-04	3.45059E-04	3.45058E-04	3.45056E-04	3.45050E-04	3.45041E-04	3.45022E-04	3.44965E-04	3.44870E-04
1.0E+24	3.16513E-04	3.16513E-04	3.16512E-04	3.16511E-04	3.16509E-04	3.16504E-04	3.16495E-04	3.16478E-04	3.16425E-04	3.16338E-04
2.0E+24	3.06849E-04	3.06849E-04	3.06848E-04	3.06847E-04	3.06846E-04	3.06840E-04	3.06832E-04	3.06815E-04	3.06765E-04	3.06681E-04
5.0E+24	3.02786E-04	3.02785E-04	3.02785E-04	3.02784E-04	3.02783E-04	3.02778E-04	3.02769E-04	3.02753E-04	3.02704E-04	3.02622E-04
1.0E+25	3.02285E-04	3.02285E-04	3.02284E-04	3.02283E-04	3.02283E-04	3.02277E-04	3.02269E-04	3.02252E-04	3.02203E-04	3.02121E-04
2.0E+25	3.02267E-04	3.02267E-04	3.02267E-04	3.02266E-04	3.02264E-04	3.02259E-04	3.02251E-04	3.02235E-04	3.02185E-04	3.02104E-04

O3 COLUMN DENSITY

Table B13. Total Photodissociation Rate Coefficients for the Process  $N_2C_5 + h\nu \rightarrow NO_2 + NO_2 + O$  for Wavelengths From 210 to 380 nm (Contd)

O3 COLUMN DENSITY										
	2.0E+14	5.0E+14	1.0E+15	2.0E+15	5.0E+15	1.0E+16	2.0E+16	5.0E+16	1.0E+17	2.0E+17
1.0E+17	6.91780E-04	6.90946E-04	6.89561E-04	6.86805E-04	6.78656E-04	7.72142E-07	7.67675E-07	7.54704E-07	7.34323E-07	6.97141E-07
2.0E+17	6.91780E-04	6.90946E-04	6.89561E-04	6.86805E-04	6.78656E-04	7.72129E-07	7.67662E-07	7.54692E-07	7.34311E-07	6.97129E-07
5.0E+17	6.91779E-04	6.90946E-04	6.89560E-04	6.86804E-04	6.78655E-04	7.72091E-07	7.67624E-07	7.54654E-07	7.34274E-07	6.97094E-07
1.0E+18	6.91778E-04	6.90944E-04	6.89559E-04	6.86803E-04	6.78654E-04	7.72028E-07	7.67561E-07	7.54592E-07	7.34214E-07	6.97036E-07
2.0E+18	6.91776E-04	6.90942E-04	6.89557E-04	6.86801E-04	6.78652E-04	7.71902E-07	7.67436E-07	7.54469E-07	7.34093E-07	6.96921E-07
5.0E+18	6.91769E-04	6.90935E-04	6.89550E-04	6.86794E-04	6.78645E-04	7.71529E-07	7.67064E-07	7.54102E-07	7.33735E-07	6.96579E-07
1.0E+19	6.91759E-04	6.90924E-04	6.89538E-04	6.86782E-04	6.78634E-04	7.70920E-07	7.66459E-07	7.53505E-07	7.33151E-07	6.96021E-07
2.0E+19	6.91735E-04	6.90901E-04	6.89516E-04	6.86760E-04	6.78611E-04	7.69752E-07	7.65296E-07	7.52358E-07	7.32030E-07	6.94950E-07
5.0E+19	6.91668E-04	6.90833E-04	6.89447E-04	6.86591E-04	6.78543E-04	7.66566E-07	7.62124E-07	7.49229E-07	7.28972E-07	6.92028E-07
1.0E+20	6.91552E-04	6.90718E-04	6.89333E-04	6.86577E-04	6.78430E-04	7.62013E-07	7.57592E-07	7.44758E-07	7.24601E-07	6.87850E-07
2.0E+20	6.91324E-04	6.90490E-04	6.89105E-04	6.86350E-04	6.78204E-04	7.54555E-07	7.50168E-07	7.37433E-07	7.17439E-07	6.81002E-07
5.0E+20	6.90639E-04	6.89806E-04	6.88422E-04	6.85668E-04	6.77526E-04	7.53788E-07	7.49405E-07	7.36866E-07	7.16715E-07	6.80321E-07
1.0E+21	6.89502E-04	6.88670E-04	6.87286E-04	6.84535E-04	6.76400E-04	7.53682E-07	7.49405E-07	7.36866E-07	7.16715E-07	6.80321E-07
2.0E+21	6.87239E-04	6.86408E-04	6.85027E-04	6.82280E-04	6.74158E-04	7.16305E-07	7.12093E-07	6.99879E-07	6.80733E-07	6.45925E-07
5.0E+21	6.80541E-04	6.79714E-04	6.78340E-04	6.75607E-04	6.67525E-04	6.84323E-07	6.80263E-07	6.68501E-07	6.50088E-07	6.16682E-07
1.0E+22	6.69675E-04	6.68855E-04	6.67492E-04	6.64781E-04	6.56765E-04	6.26879E-07	6.23086E-07	6.12112E-07	5.94981E-07	5.64024E-07
2.0E+22	6.49011E-04	6.48204E-04	6.46862E-04	6.44194E-04	6.36305E-04	5.56855E-07	5.53400E-07	5.43429E-07	5.27919E-07	5.00042E-07
5.0E+22	5.94699E-04	5.93926E-04	5.92642E-04	5.90089E-04	5.82543E-04	4.38888E-07	4.35400E-07	4.27910E-07	4.15340E-07	3.92590E-07
1.0E+23	5.24918E-04	5.24193E-04	5.23987E-04	5.20591E-04	5.13514E-04	2.72611E-07	2.70613E-07	2.64931E-07	2.56323E-07	2.41429E-07
2.0E+23	4.37147E-04	4.36488E-04	4.35394E-04	4.33218E-04	4.26798E-04	1.30307E-07	1.29099E-07	1.25731E-07	1.20814E-07	1.12767E-07
5.0E+23	3.44680E-04	3.44112E-04	3.43169E-04	3.41296E-04	3.35771E-04	3.79634E-08	3.73623E-08	3.57555E-08	3.35931E-08	3.05016E-08
1.0E+24	3.16163E-04	3.15639E-04	3.14769E-04	3.13042E-04	3.07949E-04	1.84099E-08	1.79518E-08	1.67513E-08	1.52016E-08	1.31551E-08
2.0E+24	3.06513E-04	3.06011E-04	3.05177E-04	3.03521E-04	2.98638E-04	1.77620E-08	1.73255E-08	1.61820E-08	1.47065E-08	1.27561E-08
5.0E+24	3.02457E-04	3.01966E-04	3.01150E-04	2.99528E-04	2.94749E-04	1.76841E-08	1.72539E-08	1.61266E-08	1.46703E-08	1.27403E-08
1.0E+25	3.01958E-04	3.01467E-04	3.00653E-04	2.99036E-04	2.94271E-04	1.76756E-08	1.72462E-08	1.61207E-08	1.46664E-08	1.27388E-08
2.0E+25	3.01940E-04	3.01450E-04	3.00636E-04	2.99019E-04	2.94254E-04	1.76753E-08	1.72459E-08	1.61205E-08	1.46663E-08	1.27387E-08

O2 COLUMN DENSITY



Table B13. Total Photodissociation Rate Coefficients for the Process  
 $\text{N}_2\text{O}_5 + h\nu \rightarrow \text{NO}_2 + \text{NO}_2 + \text{O}$  for Wavelengths From 210 to 380 nm (Contd)

		O3 COLUMN DENSITY				
		5.0E+17	1.0E+18	2.0E+18	5.0E+18	1.0E+19
1.0E+17	6.03763E-07	4.83551E-07	3.18465E-07	9.86375E-08	1.63090E-08	
2.0E+17	6.03753E-07	4.83543E-07	3.18460E-07	9.86362E-08	1.63089E-08	
5.0E+17	6.03723E-07	4.83519E-07	3.18444E-07	9.86322E-08	1.63084E-08	
1.0E+18	6.03672E-07	4.83479E-07	3.18419E-07	9.86255E-08	1.63077E-08	
2.0E+18	6.03572E-07	4.83399E-07	3.18368E-07	9.86123E-08	1.63062E-08	
5.0E+18	6.03273E-07	4.83161E-07	3.18217E-07	9.85730E-08	1.63018E-08	
1.0E+19	6.02787E-07	4.82774E-07	3.17971E-07	9.85087E-08	1.62946E-08	
2.0E+19	6.01853E-07	4.82030E-07	3.17497E-07	9.83847E-08	1.62806E-08	
5.0E+19	5.99303E-07	4.79995E-07	3.16199E-07	9.80421E-08	1.62413E-08	
1.0E+20	5.96653E-07	4.77078E-07	3.14330E-07	9.75427E-08	1.61828E-08	
2.0E+20	5.89662E-07	4.72279E-07	3.11242E-07	9.67042E-08	1.60817E-08	
5.0E+20	5.89092E-07	4.71844E-07	3.10977E-07	9.66372E-08	1.60738E-08	
1.0E+21	5.75467E-07	4.60915E-07	3.03913E-07	9.46837E-08	1.58296E-08	
2.0E+21	5.59003E-07	4.47700E-07	2.95339E-07	9.22722E-08	1.55172E-08	
5.0E+21	5.33511E-07	4.27298E-07	2.82119E-07	8.85198E-08	1.50175E-08	
1.0E+22	4.87436E-07	3.90206E-07	2.57815E-07	8.13909E-08	1.40144E-08	
2.0E+22	4.31625E-07	3.45375E-07	2.28419E-07	7.26317E-08	1.27358E-08	
5.0E+22	3.38947E-07	2.71525E-07	1.80395E-07	5.83839E-08	1.06352E-08	
1.0E+23	2.06846E-07	1.65135E-07	1.09845E-07	3.63482E-08	7.14610E-09	
2.0E+23	9.55816E-08	7.61533E-08	5.11481E-08	1.79497E-08	4.17913E-09	
5.0E+23	2.52507E-08	2.03050E-08	1.43418E-08	6.21662E-09	2.22475E-09	
1.0E+24	1.02400E-08	8.04676E-09	5.85509E-09	3.22418E-09	1.67355E-09	
2.0E+24	9.95878E-09	7.83253E-09	5.70855E-09	3.17142E-09	1.66353E-09	
5.0E+24	9.95734E-09	7.83247E-09	5.70855E-09	3.17142E-09	1.66353E-09	
1.0E+25	9.95724E-09	7.83247E-09	5.70855E-09	3.17142E-09	1.66353E-09	
2.0E+25	9.95723E-09	7.83247E-09	5.70855E-09	3.17142E-09	1.66353E-09	

O2 COLUMN DENSITY

Table B14. Total Photodissociation Rate Coefficients for the Process  $\text{HNO}_2 + h\nu \rightarrow \text{OH} + \text{NO}$  for Wavelengths From 300 to 390 nm

1.0E+14	5.84756E-04
2.0E+14	5.84755E-04
5.0E+14	5.84754E-04
1.0E+15	5.84753E-04
2.0E+15	5.84749E-04
5.0E+15	5.84739E-04
1.0E+16	5.84722E-04
2.0E+16	5.84688E-04
5.0E+16	5.84585E-04
1.0E+17	5.84416E-04
2.0E+17	5.84083E-04
5.0E+17	5.83115E-04
1.0E+18	5.81605E-04
2.0E+18	5.78914E-04
5.0E+18	5.72656E-04
1.0E+19	5.65442E-04
2.0E+19	5.55729E-04
5.0E+19	5.37947E-04
1.0E+20	5.20145E-04
2.0E+20	4.99103E-04
5.0E+20	4.68331E-04
1.0E+21	4.43897E-04

O3 COLUMN DENSITY

Table B15. Total Photodissociation Rate Coefficients for the Process  $\text{HNO}_3 + h\nu \rightarrow \text{OH} + \text{NO}_2$  for Wavelengths From 192 to 325 nm

	O3 COLUMN DENSITY									
	1.0E+12	2.0E+12	5.0E+12	1.0E+13	2.0E+13	5.0E+13	1.0E+14	2.0E+14	5.0E+14	1.0E+15
1.0E+17	1.16539E-04	1.16539E-04	1.16539E-04	1.16537E-04	1.16535E-04	1.16528E-04	1.16516E-04	1.16493E-04	1.16424E-04	1.16309E-04
2.0E+17	1.16539E-04	1.16539E-04	1.16538E-04	1.16537E-04	1.16535E-04	1.16528E-04	1.16516E-04	1.16493E-04	1.16424E-04	1.16308E-04
5.0E+17	1.16539E-04	1.16539E-04	1.16538E-04	1.16537E-04	1.16534E-04	1.16528E-04	1.16516E-04	1.16493E-04	1.16423E-04	1.16308E-04
1.0E+18	1.16538E-04	1.16538E-04	1.16537E-04	1.16536E-04	1.16534E-04	1.16527E-04	1.16515E-04	1.16492E-04	1.16423E-04	1.16307E-04
2.0E+18	1.16537E-04	1.16537E-04	1.16536E-04	1.16535E-04	1.16532E-04	1.16525E-04	1.16514E-04	1.16491E-04	1.16421E-04	1.16306E-04
5.0E+18	1.16532E-04	1.16532E-04	1.16532E-04	1.16530E-04	1.16528E-04	1.16521E-04	1.16510E-04	1.16486E-04	1.16417E-04	1.16302E-04
1.0E+19	1.16525E-04	1.16525E-04	1.16524E-04	1.16523E-04	1.16521E-04	1.16514E-04	1.16502E-04	1.16479E-04	1.16410E-04	1.16295E-04
2.0E+19	1.16511E-04	1.16511E-04	1.16510E-04	1.16509E-04	1.16507E-04	1.16500E-04	1.16488E-04	1.16465E-04	1.16396E-04	1.16280E-04
5.0E+19	1.16469E-04	1.16469E-04	1.16468E-04	1.16467E-04	1.16465E-04	1.16458E-04	1.16446E-04	1.16423E-04	1.16354E-04	1.16238E-04
1.0E+20	1.16400E-04	1.16400E-04	1.16399E-04	1.16398E-04	1.16396E-04	1.16389E-04	1.16377E-04	1.16354E-04	1.16285E-04	1.16169E-04
2.0E+20	1.16265E-04	1.16265E-04	1.16264E-04	1.16263E-04	1.16261E-04	1.16254E-04	1.16242E-04	1.16219E-04	1.16150E-04	1.16035E-04
5.0E+20	1.16127E-04	1.16127E-04	1.16126E-04	1.16125E-04	1.16122E-04	1.16116E-04	1.16104E-04	1.16081E-04	1.16012E-04	1.15896E-04
1.0E+21	1.15652E-04	1.15652E-04	1.15652E-04	1.15650E-04	1.15648E-04	1.15641E-04	1.15630E-04	1.15606E-04	1.15537E-04	1.15422E-04
2.0E+21	1.14835E-04	1.14835E-04	1.14834E-04	1.14833E-04	1.14831E-04	1.14824E-04	1.14812E-04	1.14789E-04	1.14720E-04	1.14605E-04
5.0E+21	1.12858E-04	1.12857E-04	1.12857E-04	1.12856E-04	1.12853E-04	1.12846E-04	1.12835E-04	1.12812E-04	1.12743E-04	1.12629E-04
1.0E+22	1.09086E-04	1.09085E-04	1.09085E-04	1.09084E-04	1.09081E-04	1.09075E-04	1.09063E-04	1.09041E-04	1.08973E-04	1.08860E-04

O2 COLUMN DENSITY

Table B15. Total Photodissociation Rate Coefficients for the Process  $\text{HNO}_3 + h\nu \rightarrow \text{OH} + \text{NO}_2$  for Wavelengths From 192 to 325 nm (Contd)

		O3 COLUMN DENSITY									
		2.0E+15	5.0E+15	1.0E+16	2.0E+16	5.0E+16	1.0E+17	2.0E+17	5.0E+17	1.0E+18	2.0E+18
1.0E+17	1.16079E-04	1.15398E-04	1.14292E-04	1.12176E-04	1.06523E-04	9.89202E-05	8.80795E-05	8.80795E-05	6.98619E-05	5.31722E-05	3.41525E-05
2.0E+17	1.16079E-04	1.15398E-04	1.14292E-04	1.12176E-04	1.06523E-04	9.89201E-05	8.80794E-05	8.80794E-05	6.98618E-05	5.31721E-05	3.41525E-05
5.0E+17	1.16078E-04	1.15398E-04	1.14291E-04	1.12176E-04	1.06522E-04	9.89197E-05	8.80790E-05	8.80790E-05	6.98614E-05	5.31718E-05	3.41523E-05
1.0E+18	1.16078E-04	1.15397E-04	1.14290E-04	1.12175E-04	1.06522E-04	9.89190E-05	8.80784E-05	8.80784E-05	6.98609E-05	5.31713E-05	3.41520E-05
2.0E+18	1.16076E-04	1.15396E-04	1.14289E-04	1.12174E-04	1.06520E-04	9.89177E-05	8.80771E-05	8.80771E-05	6.98597E-05	5.31704E-05	3.41514E-05
5.0E+18	1.16072E-04	1.15391E-04	1.14285E-04	1.12169E-04	1.06516E-04	9.89136E-05	8.80733E-05	8.80733E-05	6.98564E-05	5.31677E-05	3.41495E-05
1.0E+19	1.16065E-04	1.15384E-04	1.14278E-04	1.12162E-04	1.06509E-04	9.89069E-05	8.80669E-05	8.80669E-05	6.98508E-05	5.31631E-05	3.41464E-05
2.0E+19	1.16051E-04	1.15370E-04	1.14264E-04	1.12148E-04	1.06495E-04	9.88935E-05	8.80541E-05	8.80541E-05	6.98396E-05	5.31540E-05	3.41402E-05
5.0E+19	1.16009E-04	1.15328E-04	1.14222E-04	1.12107E-04	1.06454E-04	9.88536E-05	8.80161E-05	8.80161E-05	6.98064E-05	5.31269E-05	3.41217E-05
1.0E+20	1.15940E-04	1.15260E-04	1.14133E-04	1.12038E-04	1.06387E-04	9.87880E-05	8.79536E-05	8.79536E-05	6.97518E-05	5.30825E-05	3.40914E-05
2.0E+20	1.15805E-04	1.15125E-04	1.14019E-04	1.11905E-04	1.06256E-04	9.86602E-05	8.78319E-05	8.78319E-05	6.96455E-05	5.29960E-05	3.40325E-05
5.0E+20	1.15667E-04	1.14987E-04	1.13802E-04	1.11769E-04	1.06124E-04	9.85336E-05	8.77152E-05	8.77152E-05	6.95513E-05	5.29266E-05	3.39918E-05
1.0E+21	1.15193E-04	1.14514E-04	1.13411E-04	1.11301E-04	1.05664E-04	9.80871E-05	8.72930E-05	8.72930E-05	6.91883E-05	5.26366E-05	3.37992E-05
2.0E+21	1.14377E-04	1.13700E-04	1.12599E-04	1.10494E-04	1.04873E-04	9.73209E-05	8.65711E-05	8.65711E-05	6.85728E-05	5.21498E-05	3.34803E-05
5.0E+21	1.12402E-04	1.11730E-04	1.10636E-04	1.08546E-04	1.02968E-04	9.54811E-05	8.48483E-05	8.48483E-05	6.71253E-05	5.10251E-05	3.27621E-05
1.0E+22	1.08636E-04	1.07971E-04	1.06890E-04	1.04826E-04	9.93215E-05	9.19509E-05	8.15257E-05	8.15257E-05	6.42989E-05	4.87946E-05	3.13045E-05

Table B20. Total Photodissociation Rate Coefficients for the Process  $\text{HO}_2 + h\nu \rightarrow \text{O}_2 + \text{H}$  for Wavelengths From 180 to 274 nm

	O3 COLUMN DENSITY									
	2.0E+15	5.0E+15	1.0E+16	2.0E+16	5.0E+16	1.0E+17	2.0E+17	5.0E+17	1.0E+18	2.0E+18
1.0E+17	1.12763E-03	1.11447E-03	1.09309E-03	1.05241E-03	9.45069E-04	8.04875E-04	6.17887E-04	3.63050E-04	2.08833E-04	9.88600E-05
2.0E+17	1.12763E-03	1.11445E-03	1.09307E-03	1.05239E-03	9.45050E-04	8.04857E-04	6.17870E-04	3.63037E-04	2.08824E-04	9.88554E-05
5.0E+17	1.12757E-03	1.11439E-03	1.09302E-03	1.05234E-03	9.44997E-04	8.04805E-04	6.17823E-04	3.62998E-04	2.08797E-04	9.88421E-05
1.0E+18	1.12748E-03	1.11431E-03	1.09293E-03	1.05226E-03	9.44916E-04	8.04728E-04	6.17751E-04	3.62940E-04	2.08757E-04	9.88220E-05
2.0E+18	1.12734E-03	1.11417E-03	1.09279E-03	1.05212E-03	9.44773E-04	8.04595E-04	6.17628E-04	3.62841E-04	2.08687E-04	9.87871E-05
5.0E+18	1.12731E-03	1.11384E-03	1.09247E-03	1.05179E-03	9.44463E-04	8.04292E-04	6.17346E-04	3.62614E-04	2.08526E-04	9.87059E-05
1.0E+19	1.12663E-03	1.11344E-03	1.09207E-03	1.05140E-03	9.44081E-04	8.03924E-04	6.17003E-04	3.62337E-04	2.08330E-04	9.86049E-05
2.0E+19	1.12603E-03	1.11287E-03	1.09150E-03	1.05083E-03	9.43523E-04	8.03387E-04	6.16506E-04	3.61934E-04	2.08042E-04	9.84546E-05
5.0E+19	1.12467E-03	1.11170E-03	1.09034E-03	1.04968E-03	9.42404E-04	8.02312E-04	6.15510E-04	3.61130E-04	2.07465E-04	9.81468E-05
1.0E+20	1.12355E-03	1.11039E-03	1.08903E-03	1.04836E-03	9.41138E-04	8.01099E-04	6.14391E-04	3.60232E-04	2.05818E-04	9.77951E-05
2.0E+20	1.12163E-03	1.10843E-03	1.08714E-03	1.04652E-03	9.39327E-04	7.99371E-04	6.12808E-04	3.58970E-04	2.05910E-04	9.77939E-05
5.0E+20	1.12007E-03	1.10692E-03	1.08559E-03	1.04500E-03	9.37898E-04	7.98076E-04	6.11722E-04	3.58261E-04	2.05491E-04	9.71014E-05
1.0E+21	1.11508E-03	1.10193E-03	1.08066E-03	1.04013E-03	9.33225E-04	7.93687E-04	6.07804E-04	3.55288E-04	2.03424E-04	9.59730E-05
2.0E+21	1.10763E-03	1.09454E-03	1.07330E-03	1.03290E-03	9.3328E-04	7.87288E-04	6.02206E-04	3.51219E-04	2.00694E-04	9.45129E-05
5.0E+21	1.08948E-03	1.07650E-03	1.05544E-03	1.01537E-03	9.09742E-04	7.72075E-04	5.89175E-04	3.42196E-04	1.94936E-04	9.15811E-05
1.0E+22	1.05983E-03	1.04702E-03	1.02624E-03	9.86722E-04	8.82631E-04	7.47200E-04	5.67849E-04	3.27368E-04	1.85390E-04	8.66197E-05
2.0E+22	1.00734E-03	9.94850E-04	9.74605E-04	9.36127E-04	8.34937E-04	7.03715E-04	5.30908E-04	3.02450E-04	1.69846E-04	7.88314E-05
5.0E+22	8.75133E-04	8.63526E-04	8.44722E-04	8.09046E-04	7.15656E-04	5.95698E-04	4.40585E-04	2.43079E-04	1.34025E-04	6.16213E-05
1.0E+23	7.01310E-04	6.90918E-04	6.74107E-04	6.42298E-04	5.59643E-04	4.55085E-04	3.23772E-04	1.67262E-04	8.83747E-05	3.93658E-05
2.0E+23	4.85107E-04	4.76452E-04	4.62485E-04	4.36185E-04	3.68712E-04	2.85655E-04	1.86793E-04	8.33320E-05	4.04439E-05	1.71553E-05
5.0E+23	2.50555E-04	2.44369E-04	2.34434E-04	2.15892E-04	1.69502E-04	1.15414E-04	5.79847E-05	1.45263E-05	5.33679E-06	2.20992E-06
1.0E+24	1.70615E-04	1.65677E-04	1.57771E-04	1.43098E-04	1.06935E-04	6.61750E-05	2.59885E-05	2.17455E-06	2.00761E-07	4.55079E-08
2.0E+24	1.42977E-04	1.38649E-04	1.31728E-04	1.18914E-04	8.75310E-05	5.26373E-05	1.92008E-05	1.01890E-06	1.52165E-08	2.52692E-09
5.0E+24	1.31568E-04	1.27536E-04	1.21090E-04	1.09166E-04	6.90283E-05	4.77828E-05	1.71599E-05	5.59583E-07	1.19301E-08	2.49510E-09
1.0E+25	1.30174E-04	1.26179E-04	1.19793E-04	1.07980E-04	7.91231E-05	4.72054E-05	1.69250E-05	8.43752E-07	1.17530E-08	2.49508E-09
2.0E+25	1.30125E-04	1.26131E-04	1.19747E-04	1.07939E-04	7.90911E-05	4.71850E-05	1.69167E-05	8.43194E-07	1.17468E-08	2.49508E-09

O3 COLUMN DENSITY

Table B20. Total Photodissociation Rate Coefficients for the Process  $\text{HO}_2 + h\nu \rightarrow \text{O}_2 + \text{H}$  for Wavelengths From 180 to 274 nm

	O3 COLUMN DENSITY									
	1.0E+12	2.0E+12	5.0E+12	1.0E+13	2.0E+13	5.0E+13	1.0E+14	2.0E+14	5.0E+14	1.0E+15
1.0E+17	1.13657E-03	1.13656E-03	1.13655E-03	1.13653E-03	1.13648E-03	1.13635E-03	1.13612E-03	1.13567E-03	1.13433E-03	1.13209E-03
2.0E+17	1.13655E-03	1.13654E-03	1.13653E-03	1.13651E-03	1.13646E-03	1.13633E-03	1.13610E-03	1.13565E-03	1.13431E-03	1.13207E-03
5.0E+17	1.13649E-03	1.13648E-03	1.13647E-03	1.13645E-03	1.13641E-03	1.13627E-03	1.13605E-03	1.13560E-03	1.13425E-03	1.13202E-03
1.0E+18	1.13641E-03	1.13640E-03	1.13639E-03	1.13637E-03	1.13632E-03	1.13619E-03	1.13596E-03	1.13551E-03	1.13417E-03	1.13193E-03
2.0E+18	1.13627E-03	1.13626E-03	1.13625E-03	1.13623E-03	1.13618E-03	1.13605E-03	1.13582E-03	1.13537E-03	1.13403E-03	1.13179E-03
5.0E+18	1.13594E-03	1.13593E-03	1.13592E-03	1.13590E-03	1.13585E-03	1.13572E-03	1.13549E-03	1.13504E-03	1.13370E-03	1.13146E-03
1.0E+19	1.13554E-03	1.13554E-03	1.13552E-03	1.13550E-03	1.13546E-03	1.13532E-03	1.13510E-03	1.13465E-03	1.13330E-03	1.13107E-03
2.0E+19	1.13496E-03	1.13496E-03	1.13494E-03	1.13492E-03	1.13488E-03	1.13474E-03	1.13452E-03	1.13407E-03	1.13272E-03	1.13049E-03
5.0E+19	1.13379E-03	1.13379E-03	1.13378E-03	1.13375E-03	1.13371E-03	1.13357E-03	1.13335E-03	1.13290E-03	1.13156E-03	1.12932E-03
1.0E+20	1.13247E-03	1.13246E-03	1.13245E-03	1.13243E-03	1.13238E-03	1.13225E-03	1.13202E-03	1.13158E-03	1.13023E-03	1.12800E-03
2.0E+20	1.13056E-03	1.13056E-03	1.13055E-03	1.13052E-03	1.13048E-03	1.13034E-03	1.13012E-03	1.12967E-03	1.12833E-03	1.12609E-03
5.0E+20	1.12838E-03	1.12897E-03	1.12896E-03	1.12894E-03	1.12889E-03	1.12876E-03	1.12853E-03	1.12808E-03	1.12674E-03	1.12451E-03
1.0E+21	1.12397E-03	1.12397E-03	1.12396E-03	1.12393E-03	1.12389E-03	1.12376E-03	1.12353E-03	1.12308E-03	1.12174E-03	1.11951E-03
2.0E+21	1.11649E-03	1.11649E-03	1.11648E-03	1.11645E-03	1.11641E-03	1.11628E-03	1.11605E-03	1.11561E-03	1.11427E-03	1.11205E-03
5.0E+21	1.09827E-03	1.09827E-03	1.09826E-03	1.09824E-03	1.09819E-03	1.09806E-03	1.09784E-03	1.09740E-03	1.09607E-03	1.09387E-03
1.0E+22	1.06851E-03	1.06851E-03	1.06850E-03	1.06847E-03	1.06843E-03	1.06830E-03	1.06808E-03	1.06764E-03	1.06633E-03	1.06416E-03
2.0E+22	1.01580E-03	1.01580E-03	1.01578E-03	1.01576E-03	1.01572E-03	1.01559E-03	1.01538E-03	1.01495E-03	1.01368E-03	1.01156E-03
5.0E+22	8.83007E-04	8.83003E-04	8.82991E-04	8.82971E-04	8.82932E-04	8.82613E-04	8.82614E-04	8.82218E-04	8.81031E-04	8.79058E-04
1.0E+23	7.08363E-04	7.08363E-04	7.08352E-04	7.08334E-04	7.08299E-04	7.08192E-04	7.08014E-04	7.07659E-04	7.06595E-04	7.04827E-04
2.0E+23	4.90993E-04	4.90990E-04	4.90981E-04	4.90967E-04	4.90937E-04	4.90848E-04	4.90699E-04	4.90403E-04	4.89515E-04	4.88040E-04
5.0E+23	2.54772E-04	2.54772E-04	2.54766E-04	2.54755E-04	2.54734E-04	2.54670E-04	2.54564E-04	2.54351E-04	2.53714E-04	2.52656E-04
1.0E+24	1.73989E-04	1.73987E-04	1.73982E-04	1.73974E-04	1.73957E-04	1.73905E-04	1.73820E-04	1.73650E-04	1.73140E-04	1.72294E-04
2.0E+24	1.45936E-04	1.45934E-04	1.45930E-04	1.45922E-04	1.45907E-04	1.45862E-04	1.45788E-04	1.45638E-04	1.45191E-04	1.44449E-04
5.0E+24	1.34326E-04	1.34325E-04	1.34321E-04	1.34314E-04	1.34300E-04	1.34258E-04	1.34188E-04	1.34049E-04	1.33632E-04	1.32941E-04
1.0E+25	1.32907E-04	1.32906E-04	1.32901E-04	1.32894E-04	1.32881E-04	1.32839E-04	1.32770E-04	1.32632E-04	1.32219E-04	1.31534E-04
2.0E+25	1.32857E-04	1.32855E-04	1.32851E-04	1.32844E-04	1.32830E-04	1.32789E-04	1.32720E-04	1.32582E-04	1.32169E-04	1.31484E-04

O2 COLUMN DENSITY

Table B19. Total Photodissociation Rate Coefficients for the Process  $\text{CH}_2\text{O} + h\nu \rightarrow \text{CHO} + \text{H}$  and  $\text{CH}_2\text{O} + h\nu \rightarrow \text{CO} + \text{H}_2$  for Wavelengths From 240 to 360 nm (Contd)

		O3 COLUMN DENSITY											
		5.0E+15	1.0E+16	2.0E+16	5.0E+16	1.0E+17	2.0E+17	5.0E+17	1.0E+18	2.0E+18	5.0E+18		
1.0E+13	2.58223E-04	2.57561E-04	2.56282E-04	2.52774E-04	2.47810E-04	2.40115E-04	2.25324E-04	2.10458E-04	1.92675E-04	1.66137E-04			
2.0E+13	2.58223E-04	2.57561E-04	2.56282E-04	2.52774E-04	2.47810E-04	2.40115E-04	2.25324E-04	2.10458E-04	1.92675E-04	1.66137E-04			
5.0E+13	2.58223E-04	2.57561E-04	2.56282E-04	2.52774E-04	2.47810E-04	2.40115E-04	2.25324E-04	2.10458E-04	1.92675E-04	1.66137E-04			
1.0E+14	2.58222E-04	2.57560E-04	2.56281E-04	2.52773E-04	2.47809E-04	2.40114E-04	2.25324E-04	2.10458E-04	1.92675E-04	1.66137E-04			
2.0E+14	2.58221E-04	2.57559E-04	2.56280E-04	2.52772E-04	2.47809E-04	2.40114E-04	2.25324E-04	2.10458E-04	1.92675E-04	1.66137E-04			
5.0E+14	2.58219E-04	2.57556E-04	2.56278E-04	2.52770E-04	2.47806E-04	2.40112E-04	2.25323E-04	2.10457E-04	1.92675E-04	1.66137E-04			
1.0E+15	2.58214E-04	2.57552E-04	2.56273E-04	2.52768E-04	2.47796E-04	2.40109E-04	2.25321E-04	2.10457E-04	1.92675E-04	1.66137E-04			
2.0E+15	2.58205E-04	2.57543E-04	2.56265E-04	2.52758E-04	2.47796E-04	2.40109E-04	2.25319E-04	2.10456E-04	1.92675E-04	1.66137E-04			
5.0E+15	2.58178E-04	2.57517E-04	2.56239E-04	2.52735E-04	2.47776E-04	2.40089E-04	2.25311E-04	2.10453E-04	1.92675E-04	1.66137E-04			
1.0E+16	2.58135E-04	2.57474E-04	2.56198E-04	2.52697E-04	2.47743E-04	2.40064E-04	2.25299E-04	2.10447E-04	1.92672E-04	1.66137E-04			
2.0E+16	2.58054E-04	2.57395E-04	2.56121E-04	2.52626E-04	2.47682E-04	2.40017E-04	2.25275E-04	2.10437E-04	1.92669E-04	1.66137E-04			
5.0E+16	2.57950E-04	2.57193E-04	2.55925E-04	2.52446E-04	2.47525E-04	2.39895E-04	2.25211E-04	2.10408E-04	1.92659E-04	1.66136E-04			
1.0E+17	2.57602E-04	2.56943E-04	2.55687E-04	2.52225E-04	2.47329E-04	2.39739E-04	2.25124E-04	2.10366E-04	1.92644E-04	1.66135E-04			
5.0E+17	2.57396E-04	2.56645E-04	2.55390E-04	2.51946E-04	2.47076E-04	2.39529E-04	2.24991E-04	2.10293E-04	1.92615E-04	1.66132E-04			
1.0E+18	2.56836E-04	2.56189E-04	2.54939E-04	2.51511E-04	2.46666E-04	2.39163E-04	2.24723E-04	2.10124E-04	1.92544E-04	1.66128E-04			
2.0E+18	2.56368E-04	2.55722E-04	2.54476E-04	2.51060E-04	2.46234E-04	2.38765E-04	2.24414E-04	2.09920E-04	1.92454E-04	1.66119E-04			
5.0E+18	2.55808E-04	2.55164E-04	2.53923E-04	2.50520E-04	2.45716E-04	2.38288E-04	2.24041E-04	2.09673E-04	1.92346E-04	1.66110E-04			
1.0E+19	2.55395E-04	2.54644E-04	2.53407E-04	2.50017E-04	2.45333E-04	2.37844E-04	2.23695E-04	2.09444E-04	1.92246E-04	1.66100E-04			
2.0E+19	2.55120E-04	2.54540E-04	2.53303E-04	2.49916E-04	2.45136E-04	2.37755E-04	2.23626E-04	2.09399E-04	1.92224E-04	1.66099E-04			
5.0E+19	2.55168E-04	2.54528E-04	2.53291E-04	2.49904E-04	2.45125E-04	2.37745E-04	2.23617E-04	2.09393E-04	1.92224E-04	1.66099E-04			
1.0E+20	2.55163E-04	2.54527E-04	2.53291E-04	2.49904E-04	2.45125E-04	2.37745E-04	2.23617E-04	2.09393E-04	1.92224E-04	1.66099E-04			
2.0E+20	2.55163E-04	2.54527E-04	2.53291E-04	2.49904E-04	2.45125E-04	2.37745E-04	2.23617E-04	2.09393E-04	1.92224E-04	1.66099E-04			
5.0E+20	2.55163E-04	2.54527E-04	2.53291E-04	2.49904E-04	2.45125E-04	2.37745E-04	2.23617E-04	2.09393E-04	1.92224E-04	1.66099E-04			
1.0E+21	2.55163E-04	2.54527E-04	2.53291E-04	2.49904E-04	2.45125E-04	2.37745E-04	2.23617E-04	2.09393E-04	1.92224E-04	1.66099E-04			
2.0E+21	2.55163E-04	2.54527E-04	2.53291E-04	2.49904E-04	2.45125E-04	2.37745E-04	2.23617E-04	2.09393E-04	1.92224E-04	1.66099E-04			
5.0E+21	2.55163E-04	2.54527E-04	2.53291E-04	2.49904E-04	2.45125E-04	2.37745E-04	2.23617E-04	2.09393E-04	1.92224E-04	1.66099E-04			
1.0E+22	2.55167E-04	2.54527E-04	2.53290E-04	2.49903E-04	2.45124E-04	2.37744E-04	2.23617E-04	2.09393E-04	1.92224E-04	1.66099E-04			
2.0E+22	2.55167E-04	2.54527E-04	2.53290E-04	2.49903E-04	2.45124E-04	2.37744E-04	2.23617E-04	2.09393E-04	1.92224E-04	1.66099E-04			
5.0E+22	2.55165E-04	2.54525E-04	2.53288E-04	2.49902E-04	2.45123E-04	2.37743E-04	2.23617E-04	2.09393E-04	1.92224E-04	1.66099E-04			
1.0E+23	2.55163E-04	2.54522E-04	2.53286E-04	2.49900E-04	2.45122E-04	2.37743E-04	2.23617E-04	2.09393E-04	1.92224E-04	1.66099E-04			
2.0E+23	2.55157E-04	2.54517E-04	2.53282E-04	2.49897E-04	2.45120E-04	2.37742E-04	2.23617E-04	2.09393E-04	1.92224E-04	1.66099E-04			
5.0E+23	2.55149E-04	2.54504E-04	2.53270E-04	2.49888E-04	2.45114E-04	2.37740E-04	2.23617E-04	2.09393E-04	1.92224E-04	1.66099E-04			
1.0E+24	2.55127E-04	2.54488E-04	2.53255E-04	2.49877E-04	2.45107E-04	2.37737E-04	2.23617E-04	2.09393E-04	1.92224E-04	1.66099E-04			
2.0E+24	2.55106E-04	2.54468E-04	2.53237E-04	2.49863E-04	2.45098E-04	2.37733E-04	2.23617E-04	2.09393E-04	1.92224E-04	1.66099E-04			
5.0E+24	2.55087E-04	2.54450E-04	2.53220E-04	2.49850E-04	2.45090E-04	2.37730E-04	2.23616E-04	2.09393E-04	1.92224E-04	1.66099E-04			
1.0E+25	2.55084E-04	2.54447E-04	2.53218E-04	2.49848E-04	2.45089E-04	2.37730E-04	2.23616E-04	2.09393E-04	1.92224E-04	1.66099E-04			

O2 COLUMN DENSITY

Table B19. Total Photodissociation Rate Coefficients for the Process  $\text{CH}_2\text{O} + h\nu \rightarrow \text{CHO} + \text{H}$  and  $\text{CH}_2\text{O} + h\nu \rightarrow \text{CO} + \text{H}_2$  for Wavelengths From 240 to 360 nm

		O3 COLUMN DENSITY											
		2.0E+12	5.0E+12	1.0E+13	2.0E+13	5.0E+13	1.0E+14	2.0E+14	5.0E+14	1.0E+15	2.0E+15		
1.0E+13	2.58901E-04	2.58901E-04	2.58901E-04	2.58900E-04	2.58899E-04	2.58895E-04	2.58888E-04	2.58874E-04	2.58833E-04	2.58764E-04	2.58628E-04	2.58901E-04	2.58901E-04
2.0E+13	2.58901E-04	2.58901E-04	2.58901E-04	2.58900E-04	2.58899E-04	2.58895E-04	2.58888E-04	2.58874E-04	2.58833E-04	2.58764E-04	2.58628E-04	2.58901E-04	2.58901E-04
5.0E+13	2.58901E-04	2.58900E-04	2.58900E-04	2.58900E-04	2.58898E-04	2.58894E-04	2.58887E-04	2.58874E-04	2.58833E-04	2.58764E-04	2.58628E-04	2.58901E-04	2.58901E-04
1.0E+14	2.58900E-04	2.58900E-04	2.58900E-04	2.58899E-04	2.58898E-04	2.58894E-04	2.58887E-04	2.58874E-04	2.58833E-04	2.58764E-04	2.58628E-04	2.58901E-04	2.58901E-04
2.0E+14	2.58899E-04	2.58899E-04	2.58898E-04	2.58897E-04	2.58896E-04	2.58893E-04	2.58886E-04	2.58872E-04	2.58831E-04	2.58763E-04	2.58627E-04	2.58899E-04	2.58899E-04
5.0E+14	2.58897E-04	2.58896E-04	2.58896E-04	2.58894E-04	2.58890E-04	2.58883E-04	2.58875E-04	2.58869E-04	2.58828E-04	2.58760E-04	2.58624E-04	2.58897E-04	2.58897E-04
1.0E+15	2.58892E-04	2.58892E-04	2.58891E-04	2.58890E-04	2.58889E-04	2.58885E-04	2.58878E-04	2.58865E-04	2.58824E-04	2.58755E-04	2.58619E-04	2.58892E-04	2.58892E-04
2.0E+15	2.58883E-04	2.58882E-04	2.58882E-04	2.58880E-04	2.58876E-04	2.58869E-04	2.58862E-04	2.58848E-04	2.58807E-04	2.58738E-04	2.58602E-04	2.58883E-04	2.58883E-04
5.0E+15	2.58856E-04	2.58855E-04	2.58854E-04	2.58853E-04	2.58849E-04	2.58842E-04	2.58835E-04	2.58822E-04	2.58781E-04	2.58712E-04	2.58576E-04	2.58856E-04	2.58856E-04
1.0E+16	2.58812E-04	2.58811E-04	2.58811E-04	2.58809E-04	2.58807E-04	2.58803E-04	2.58796E-04	2.58783E-04	2.58742E-04	2.58673E-04	2.58537E-04	2.58812E-04	2.58812E-04
2.0E+16	2.58730E-04	2.58729E-04	2.58729E-04	2.58727E-04	2.58725E-04	2.58721E-04	2.58714E-04	2.58701E-04	2.58660E-04	2.58591E-04	2.58455E-04	2.58730E-04	2.58730E-04
5.0E+16	2.58523E-04	2.58522E-04	2.58522E-04	2.58520E-04	2.58516E-04	2.58509E-04	2.58502E-04	2.58489E-04	2.58448E-04	2.58379E-04	2.58243E-04	2.58523E-04	2.58523E-04
1.0E+17	2.58271E-04	2.58271E-04	2.58271E-04	2.58269E-04	2.58265E-04	2.58258E-04	2.58251E-04	2.58238E-04	2.58197E-04	2.58128E-04	2.57992E-04	2.58271E-04	2.58271E-04
2.0E+17	2.57962E-04	2.57961E-04	2.57961E-04	2.57959E-04	2.57955E-04	2.57948E-04	2.57941E-04	2.57928E-04	2.57887E-04	2.57818E-04	2.57682E-04	2.57962E-04	2.57962E-04
5.0E+17	2.57499E-04	2.57499E-04	2.57498E-04	2.57497E-04	2.57493E-04	2.57486E-04	2.57479E-04	2.57466E-04	2.57425E-04	2.57356E-04	2.57220E-04	2.57499E-04	2.57499E-04
1.0E+18	2.57029E-04	2.57028E-04	2.57028E-04	2.57026E-04	2.57022E-04	2.57015E-04	2.57008E-04	2.56995E-04	2.56954E-04	2.56885E-04	2.56749E-04	2.57029E-04	2.57029E-04
2.0E+18	2.56466E-04	2.56465E-04	2.56465E-04	2.56463E-04	2.56459E-04	2.56452E-04	2.56445E-04	2.56432E-04	2.56391E-04	2.56322E-04	2.56186E-04	2.56466E-04	2.56466E-04
5.0E+18	2.55942E-04	2.55941E-04	2.55941E-04	2.55939E-04	2.55935E-04	2.55928E-04	2.55921E-04	2.55908E-04	2.55867E-04	2.55798E-04	2.55662E-04	2.55942E-04	2.55942E-04
1.0E+19	2.55837E-04	2.55836E-04	2.55836E-04	2.55834E-04	2.55830E-04	2.55823E-04	2.55816E-04	2.55803E-04	2.55762E-04	2.55693E-04	2.55557E-04	2.55837E-04	2.55837E-04
2.0E+19	2.55824E-04	2.55824E-04	2.55824E-04	2.55822E-04	2.55818E-04	2.55811E-04	2.55804E-04	2.55791E-04	2.55750E-04	2.55681E-04	2.55545E-04	2.55824E-04	2.55824E-04
5.0E+19	2.55824E-04	2.55824E-04	2.55824E-04	2.55822E-04	2.55818E-04	2.55811E-04	2.55804E-04	2.55791E-04	2.55750E-04	2.55681E-04	2.55545E-04	2.55824E-04	2.55824E-04
1.0E+20	2.55824E-04	2.55824E-04	2.55824E-04	2.55822E-04	2.55818E-04	2.55811E-04	2.55804E-04	2.55791E-04	2.55750E-04	2.55681E-04	2.55545E-04	2.55824E-04	2.55824E-04
2.0E+20	2.55824E-04	2.55824E-04	2.55824E-04	2.55822E-04	2.55818E-04	2.55811E-04	2.55804E-04	2.55791E-04	2.55750E-04	2.55681E-04	2.55545E-04	2.55824E-04	2.55824E-04
5.0E+20	2.55824E-04	2.55824E-04	2.55824E-04	2.55822E-04	2.55818E-04	2.55811E-04	2.55804E-04	2.55791E-04	2.55750E-04	2.55681E-04	2.55545E-04	2.55824E-04	2.55824E-04
1.0E+21	2.55824E-04	2.55824E-04	2.55824E-04	2.55822E-04	2.55818E-04	2.55811E-04	2.55804E-04	2.55791E-04	2.55750E-04	2.55681E-04	2.55545E-04	2.55824E-04	2.55824E-04
2.0E+21	2.55824E-04	2.55824E-04	2.55824E-04	2.55822E-04	2.55818E-04	2.55811E-04	2.55804E-04	2.55791E-04	2.55750E-04	2.55681E-04	2.55545E-04	2.55824E-04	2.55824E-04
5.0E+21	2.55824E-04	2.55824E-04	2.55824E-04	2.55822E-04	2.55818E-04	2.55811E-04	2.55804E-04	2.55791E-04	2.55750E-04	2.55681E-04	2.55545E-04	2.55824E-04	2.55824E-04
1.0E+22	2.55824E-04	2.55824E-04	2.55824E-04	2.55822E-04	2.55818E-04	2.55811E-04	2.55804E-04	2.55791E-04	2.55750E-04	2.55681E-04	2.55545E-04	2.55824E-04	2.55824E-04
2.0E+22	2.55824E-04	2.55824E-04	2.55824E-04	2.55822E-04	2.55818E-04	2.55811E-04	2.55804E-04	2.55791E-04	2.55750E-04	2.55681E-04	2.55545E-04	2.55824E-04	2.55824E-04
5.0E+22	2.55824E-04	2.55824E-04	2.55824E-04	2.55822E-04	2.55818E-04	2.55811E-04	2.55804E-04	2.55791E-04	2.55750E-04	2.55681E-04	2.55545E-04	2.55824E-04	2.55824E-04
1.0E+23	2.55818E-04	2.55818E-04	2.55818E-04	2.55816E-04	2.55812E-04	2.55805E-04	2.55798E-04	2.55785E-04	2.55744E-04	2.55675E-04	2.55539E-04	2.55818E-04	2.55818E-04
2.0E+23	2.55813E-04	2.55813E-04	2.55813E-04	2.55811E-04	2.55807E-04	2.55800E-04	2.55793E-04	2.55786E-04	2.55745E-04	2.55676E-04	2.55540E-04	2.55813E-04	2.55813E-04
5.0E+23	2.55799E-04	2.55799E-04	2.55798E-04	2.55797E-04	2.55793E-04	2.55786E-04	2.55779E-04	2.55766E-04	2.55725E-04	2.55656E-04	2.55520E-04	2.55799E-04	2.55799E-04
1.0E+24	2.55781E-04	2.55781E-04	2.55780E-04	2.55779E-04	2.55775E-04	2.55768E-04	2.55761E-04	2.55748E-04	2.55707E-04	2.55638E-04	2.55502E-04	2.55781E-04	2.55781E-04
2.0E+24	2.55759E-04	2.55759E-04	2.55758E-04	2.55757E-04	2.55753E-04	2.55746E-04	2.55739E-04	2.55726E-04	2.55685E-04	2.55616E-04	2.55480E-04	2.55759E-04	2.55759E-04
5.0E+24	2.55739E-04	2.55739E-04	2.55738E-04	2.55737E-04	2.55733E-04	2.55726E-04	2.55719E-04	2.55706E-04	2.55665E-04	2.55596E-04	2.55460E-04	2.55739E-04	2.55739E-04
1.0E+25	2.55737E-04	2.55736E-04	2.55736E-04	2.55734E-04	2.55730E-04	2.55723E-04	2.55716E-04	2.55703E-04	2.55662E-04	2.55593E-04	2.55457E-04	2.55737E-04	2.55737E-04

O2 COLUMN DENSITY



Table B18. Total Photodissociation Rate Coefficients for the Process  $\text{CO}_2 + h\nu \rightarrow \text{CO} + \text{O}$  for Wavelengths From 166 to 215 nm (Contd)

		O3 COLUMN DENSITY							
		5.0E+18	1.0E+19	2.0E+19	5.0E+19	1.0E+20	2.0E+20	5.0E+20	1.0E+21
1.0E+13	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
2.0E+13	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
5.0E+13	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
1.0E+14	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
2.0E+14	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
5.0E+14	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
1.0E+15	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
2.0E+15	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
5.0E+15	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
1.0E+16	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
2.0E+16	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
5.0E+16	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
1.0E+17	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
2.0E+17	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
5.0E+17	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
1.0E+18	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
2.0E+18	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
5.0E+18	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
1.0E+19	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
2.0E+19	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
5.0E+19	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
1.0E+20	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
2.0E+20	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
5.0E+20	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
1.0E+21	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
2.0E+21	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
5.0E+21	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
1.0E+22	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
2.0E+22	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
5.0E+22	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
1.0E+23	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
2.0E+23	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
5.0E+23	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
1.0E+24	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	
2.0E+24	1.11969E-11	1.51540E-12	4.02055E-14	1.62200E-18	1.13333E-25	6.57859E-40	1.63313E-82	2.00839-153	

O2 COLUMN DENSITY

Table B18. Total Photodissociation Rate Coefficients for the Process  $\text{CO}_2 + h\nu \rightarrow \text{CO} + \text{O}$  for Wavelengths From 166 to 215 nm (Contd)

		O3 COLUMN DENSITY									
		2.0E+15	5.0E+15	1.0E+16	2.0E+16	5.0E+16	1.0E+17	2.0E+17	5.0E+17	1.0E+18	2.0E+18
1.0E+13	8.23559E-09	8.21569E-09	8.18264E-09	8.11694E-09	7.92300E-09	7.61006E-09	7.02095E-09	5.51462E-09	3.69031E-09	1.65855E-09	
2.0E+13	8.23553E-09	8.21563E-09	8.18258E-09	8.11688E-09	7.92294E-09	7.61000E-09	7.02090E-09	5.51458E-09	3.69028E-09	1.65854E-09	
5.0E+13	8.23535E-09	8.21546E-09	8.18241E-09	8.11671E-09	7.92277E-09	7.60984E-09	7.02075E-09	5.51446E-09	3.69021E-09	1.65850E-09	
1.0E+14	8.23506E-09	8.21516E-09	8.18211E-09	8.11642E-09	7.92249E-09	7.60955E-09	7.02050E-09	5.51427E-09	3.69008E-09	1.65845E-09	
2.0E+14	8.23447E-09	8.21457E-09	8.18153E-09	8.11584E-09	7.92192E-09	7.60903E-09	7.02000E-09	5.51388E-09	3.68982E-09	1.65833E-09	
5.0E+14	8.23270E-09	8.21281E-09	8.17977E-09	8.11409E-09	7.92022E-09	7.60739E-09	7.01849E-09	5.51270E-09	3.68903E-09	1.65799E-09	
1.0E+15	8.22975E-09	8.20987E-09	8.1784E-09	8.11119E-09	7.91739E-09	7.60467E-09	7.01599E-09	5.51074E-09	3.68773E-09	1.65741E-09	
2.0E+15	8.22386E-09	8.20400E-09	8.17099E-09	8.10538E-09	7.91172E-09	7.59923E-09	7.01098E-09	5.50682E-09	3.68513E-09	1.65626E-09	
5.0E+15	8.20623E-09	8.18641E-09	8.15347E-09	8.08801E-09	7.89477E-09	7.58296E-09	6.99598E-09	5.49508E-09	3.67733E-09	1.65282E-09	
2.0E+16	8.11889E-09	8.09928E-09	8.06670E-09	8.00194E-09	7.81079E-09	7.50233E-09	6.92170E-09	5.43696E-09	3.63871E-09	1.63577E-09	
5.0E+16	7.94821E-09	7.92902E-09	7.89714E-09	7.83376E-09	7.64688E-09	7.3481E-09	6.77654E-09	5.32339E-09	3.56326E-09	1.60246E-09	
1.0E+17	7.67522E-09	7.65670E-09	7.62593E-09	7.56476E-09	7.38421E-09	7.09286E-09	6.54437E-09	5.14173E-09	3.4258E-09	1.54920E-09	
2.0E+17	7.15081E-09	7.13357E-09	7.10493E-09	7.04801E-09	6.8997E-09	6.60881E-09	6.09833E-09	4.79270E-09	3.21064E-09	1.44677E-09	
5.0E+17	5.85974E-09	5.84567E-09	5.82229E-09	5.77581E-09	5.63861E-09	5.41720E-09	5.00030E-09	3.93360E-09	2.63989E-09	1.19483E-09	
1.0E+18	4.38135E-09	4.37090E-09	4.35355E-09	4.31905E-09	4.21719E-09	4.05279E-09	3.74314E-09	2.95019E-09	1.98678E-09	9.06714E-10	
2.0E+18	2.83407E-09	2.82743E-09	2.81639E-09	2.79445E-09	2.72966E-09	2.62504E-09	2.42783E-09	1.92180E-09	1.30434E-09	6.06123E-10	
5.0E+18	1.55073E-09	1.54725E-09	1.54147E-09	1.52998E-09	1.49604E-09	1.44116E-09	1.33751E-09	1.07004E-09	7.39870E-10	3.58122E-10	
1.0E+19	1.14257E-09	1.14010E-09	1.13598E-09	1.12780E-09	1.10361E-09	1.06448E-09	9.90439E-10	7.98532E-10	5.59504E-10	2.78444E-10	
2.0E+19	9.20991E-10	9.19045E-10	9.15810E-10	9.09377E-10	8.90355E-10	8.59560E-10	8.01226E-10	6.49564E-10	4.59465E-10	2.33258E-10	
5.0E+19	7.11624E-10	7.10164E-10	7.07738E-10	7.02911E-10	6.88636E-10	6.65510E-10	6.21645E-10	5.07214E-10	3.62768E-10	1.88543E-10	
1.0E+20	5.73567E-10	5.72422E-10	5.70518E-10	5.66731E-10	5.5534E-10	5.37359E-10	5.02866E-10	4.12617E-10	2.97993E-10	1.58086E-10	
2.0E+20	4.4748E-10	4.46286E-10	4.44854E-10	4.42003E-10	4.33565E-10	4.19669E-10	3.93849E-10	3.25484E-10	2.37963E-10	1.29490E-10	
5.0E+20	4.46927E-10	4.46066E-10	4.44634E-10	4.41784E-10	4.33350E-10	4.19669E-10	3.93652E-10	3.25319E-10	2.37839E-10	1.29419E-10	
1.0E+21	3.08433E-10	3.07875E-10	3.06947E-10	3.05101E-10	2.99633E-10	2.90751E-10	2.73817E-10	2.29036E-10	1.70898E-10	9.68980E-11	
2.0E+21	2.34369E-10	2.33967E-10	2.33299E-10	2.31968E-10	2.28025E-10	2.21612E-10	2.09361E-10	1.76783E-10	1.34005E-10	7.83751E-11	
5.0E+21	1.84499E-10	1.84196E-10	1.83691E-10	1.82687E-10	1.79710E-10	1.74864E-10	1.65593E-10	1.40837E-10	1.08055E-10	6.47285E-11	
1.0E+22	1.41710E-10	1.41484E-10	1.41109E-10	1.40362E-10	1.38148E-10	1.34542E-10	1.27637E-10	1.09152E-10	8.45402E-11	5.16358E-11	
2.0E+22	1.15859E-10	1.15677E-10	1.15373E-10	1.14768E-10	1.12973E-10	1.10051E-10	1.04455E-10	8.94741E-11	6.95121E-11	4.27606E-11	
5.0E+22	8.48856E-11	8.47527E-11	8.45316E-11	8.40914E-11	8.27862E-11	8.06608E-11	7.65907E-11	6.56940E-11	5.11706E-11	3.16775E-11	
1.0E+23	4.98125E-11	4.97335E-11	4.96020E-11	4.93402E-11	4.85642E-11	4.73012E-11	4.48846E-11	3.84294E-11	2.98519E-11	1.84374E-11	
2.0E+23	2.07956E-11	2.07625E-11	2.07075E-11	2.05980E-11	2.02734E-11	1.97452E-11	1.87351E-11	1.60400E-11	1.24702E-11	7.72202E-12	
5.0E+23	3.00891E-12	3.00448E-12	2.99711E-12	2.98900E-12	2.93890E-12	2.86802E-12	2.73219E-12	2.36794E-12	1.88005E-12	1.21561E-12	
1.0E+24	4.35417E-13	4.34426E-13	4.32780E-13	4.29508E-13	4.19844E-13	4.04232E-13	3.74777E-13	2.99008E-13	2.06060E-13	9.97381E-14	
2.0E+24	3.94567E-13	3.93629E-13	3.92071E-13	3.88973E-13	3.79825E-13	3.65056E-13	3.37227E-13	2.65877E-13	1.79013E-13	8.13910E-14	

O2 COLUMN DENSITY

Table B18. Total Photodissociation Rate Coefficients for the Process  $\text{CO}_2 + h\nu \rightarrow \text{CO} + \text{O}$  for Wavelengths From 166 to 215 nm

	O3 COLUMN DENSITY									
	1.0E+12	2.0E+12	5.0E+12	1.0E+13	2.0E+13	5.0E+13	1.0E+14	2.0E+14	5.0E+14	1.0E+15
1.0E+13	8.24887E-09	8.24886E-09	8.24884E-09	8.24881E-09	8.24875E-09	8.24855E-09	8.24821E-09	8.24755E-09	8.24555E-09	8.24223E-09
2.0E+13	8.24881E-09	8.24881E-09	8.24879E-09	8.24875E-09	8.24869E-09	8.24849E-09	8.24815E-09	8.24749E-09	8.24549E-09	8.24217E-09
5.0E+13	8.24864E-09	8.24863E-09	8.24861E-09	8.24858E-09	8.24851E-09	8.24831E-09	8.24798E-09	8.24731E-09	8.24532E-09	8.24199E-09
1.0E+14	8.24834E-09	8.24833E-09	8.24831E-09	8.24828E-09	8.24821E-09	8.24801E-09	8.24768E-09	8.24702E-09	8.24502E-09	8.24170E-09
2.0E+14	8.24775E-09	8.24774E-09	8.24772E-09	8.24769E-09	8.24762E-09	8.24742E-09	8.24709E-09	8.24643E-09	8.24443E-09	8.24111E-09
5.0E+14	8.24598E-09	8.24597E-09	8.24595E-09	8.24592E-09	8.24585E-09	8.24565E-09	8.24532E-09	8.24465E-09	8.24266E-09	8.23934E-09
1.0E+15	8.24303E-09	8.24302E-09	8.24300E-09	8.24297E-09	8.24290E-09	8.24270E-09	8.24237E-09	8.24170E-09	8.23971E-09	8.23639E-09
2.0E+15	8.23713E-09	8.23712E-09	8.23710E-09	8.23707E-09	8.23700E-09	8.23680E-09	8.23647E-09	8.23580E-09	8.23381E-09	8.23049E-09
5.0E+15	8.21947E-09	8.21946E-09	8.21944E-09	8.21941E-09	8.21934E-09	8.21914E-09	8.21881E-09	8.21815E-09	8.21616E-09	8.21285E-09
1.0E+16	8.19015E-09	8.19015E-09	8.19013E-09	8.19009E-09	8.19003E-09	8.18983E-09	8.18950E-09	8.18884E-09	8.18686E-09	8.18356E-09
2.0E+16	8.17198E-09	8.17197E-09	8.17195E-09	8.17192E-09	8.17185E-09	8.17166E-09	8.17133E-09	8.17067E-09	8.16871E-09	8.16543E-09
5.0E+16	7.96102E-09	7.96102E-09	7.96100E-09	7.96097E-09	7.96090E-09	7.96071E-09	7.96039E-09	7.95973E-09	7.95782E-09	7.95462E-09
1.0E+17	7.68759E-09	7.68758E-09	7.68756E-09	7.68753E-09	7.68747E-09	7.68729E-09	7.68698E-09	7.68636E-09	7.68450E-09	7.68141E-09
2.0E+17	7.16231E-09	7.16231E-09	7.16229E-09	7.16226E-09	7.16220E-09	7.16203E-09	7.16174E-09	7.16117E-09	7.15944E-09	7.15656E-09
5.0E+17	5.86913E-09	5.86913E-09	5.86912E-09	5.86909E-09	5.86905E-09	5.86890E-09	5.86867E-09	5.86820E-09	5.86679E-09	5.86444E-09
1.0E+18	4.38832E-09	4.38832E-09	4.38831E-09	4.38829E-09	4.38826E-09	4.38815E-09	4.38798E-09	4.38763E-09	4.38658E-09	4.38484E-09
2.0E+18	2.83851E-09	2.83850E-09	2.83849E-09	2.83847E-09	2.83840E-09	2.83829E-09	2.83807E-09	2.83740E-09	2.83629E-09	2.83462E-09
5.0E+18	1.55305E-09	1.55305E-09	1.55304E-09	1.55304E-09	1.55303E-09	1.55299E-09	1.55293E-09	1.55282E-09	1.55247E-09	1.55189E-09
1.0E+19	1.14423E-09	1.14423E-09	1.14422E-09	1.14422E-09	1.14421E-09	1.14419E-09	1.14415E-09	1.14406E-09	1.14381E-09	1.14340E-09
2.0E+19	9.22290E-10	9.22289E-10	9.22287E-10	9.22284E-10	9.22278E-10	9.22258E-10	9.22235E-10	9.22160E-10	9.21965E-10	9.21640E-10
5.0E+19	7.12598E-10	7.12597E-10	7.12596E-10	7.12594E-10	7.12589E-10	7.12574E-10	7.12550E-10	7.12501E-10	7.12355E-10	7.12111E-10
1.0E+20	5.74332E-10	5.74331E-10	5.74330E-10	5.74328E-10	5.74325E-10	5.74313E-10	5.74294E-10	5.74256E-10	5.74141E-10	5.73950E-10
2.0E+20	4.47723E-10	4.47723E-10	4.47722E-10	4.47721E-10	4.47718E-10	4.47709E-10	4.47695E-10	4.47666E-10	4.47580E-10	4.47436E-10
5.0E+20	4.47502E-10	4.47502E-10	4.47501E-10	4.47500E-10	4.47497E-10	4.47488E-10	4.47474E-10	4.47445E-10	4.47359E-10	4.47215E-10
1.0E+21	3.08805E-10	3.08805E-10	3.08804E-10	3.08803E-10	3.08802E-10	3.08796E-10	3.08787E-10	3.08768E-10	3.08712E-10	3.08619E-10
2.0E+21	2.34638E-10	2.34637E-10	2.34636E-10	2.34635E-10	2.34633E-10	2.34631E-10	2.34624E-10	2.34611E-10	2.34540E-10	2.34504E-10
5.0E+21	1.84702E-10	1.84702E-10	1.84701E-10	1.84701E-10	1.84700E-10	1.84697E-10	1.84692E-10	1.84681E-10	1.84651E-10	1.84600E-10
1.0E+22	1.41860E-10	1.41860E-10	1.41860E-10	1.41860E-10	1.41859E-10	1.41857E-10	1.41853E-10	1.41845E-10	1.41823E-10	1.41785E-10
2.0E+22	1.15981E-10	1.15981E-10	1.15981E-10	1.15981E-10	1.15980E-10	1.15978E-10	1.15975E-10	1.15969E-10	1.15951E-10	1.15920E-10
5.0E+22	8.49743E-11	8.49743E-11	8.49741E-11	8.49739E-11	8.49735E-11	8.49721E-11	8.49699E-11	8.49655E-11	8.49522E-11	8.49300E-11
1.0E+23	4.98653E-11	4.98653E-11	4.98652E-11	4.98651E-11	4.98648E-11	4.98640E-11	4.98627E-11	4.98601E-11	4.98521E-11	4.98389E-11
2.0E+23	2.08177E-11	2.08176E-11	2.08176E-11	2.08175E-11	2.08174E-11	2.08171E-11	2.08166E-11	2.08155E-11	2.08121E-11	2.08066E-11
5.0E+23	3.01187E-12	3.01186E-12	3.01186E-12	3.01185E-12	3.01184E-12	3.01179E-12	3.01172E-12	3.01157E-12	3.01113E-12	3.01039E-12
1.0E+24	4.36078E-13	4.36078E-13	4.36077E-13	4.36075E-13	4.36072E-13	4.36062E-13	4.36045E-13	4.36012E-13	4.35913E-13	4.35747E-13
2.0E+24	3.95193E-13	3.95193E-13	3.95192E-13	3.95190E-13	3.95187E-13	3.95178E-13	3.95162E-13	3.95131E-13	3.95037E-13	3.94880E-13

O2 COLUMN DENSITY

Table B17. Total Photodissociation Rate Coefficients for the Process  $\text{CO}_2 + h\nu \rightarrow \text{CO} + \text{O}(^1\text{D})$  for Wavelengths From 116.2 to 166 nm (Contd)

O3 COLUMN DENSITY									
	5.0E+17	1.0E+18	2.0E+18	5.0E+18	1.0E+19	2.0E+19	5.0E+19	1.0E+20	2.0E+20
1.0E+13	1.44282E-08	6.24892E-09	1.78563E-09	8.73281E-11	8.97046E-13	1.29487E-16	6.18488E-28	9.65893E-47	2.37149E-84
2.0E+13	1.44273E-08	6.24861E-09	1.78556E-09	8.73257E-11	8.97025E-13	1.29484E-16	6.18475E-28	9.65873E-47	2.37144E-84
5.0E+13	1.44245E-08	6.24766E-09	1.78536E-09	8.73182E-11	8.96959E-13	1.29476E-16	6.18436E-28	9.65812E-47	2.37129E-84
1.0E+14	1.44198E-08	6.24608E-09	1.78502E-09	8.73058E-11	8.96849E-13	1.29461E-16	6.18371E-28	9.65712E-47	2.37104E-84
2.0E+14	1.44104E-08	6.24293E-09	1.78433E-09	8.72810E-11	8.96630E-13	1.29433E-16	6.18243E-28	9.65511E-47	2.37055E-84
5.0E+14	1.43823E-08	6.23348E-09	1.78228E-09	8.72066E-11	8.95973E-13	1.29348E-16	6.17856E-28	9.64909E-47	2.36907E-84
1.0E+15	1.43355E-08	6.21777E-09	1.77887E-09	8.70829E-11	8.94879E-13	1.29205E-16	6.17212E-28	9.63906E-47	2.36661E-84
2.0E+15	1.42429E-08	6.18650E-09	1.77208E-09	8.68360E-11	8.92695E-13	1.28921E-16	6.15927E-28	9.61903E-47	2.36169E-84
5.0E+15	1.39692E-08	6.09393E-09	1.75189E-09	8.60999E-11	8.86177E-13	1.28073E-16	6.12087E-28	9.55919E-47	2.34700E-84
1.0E+16	1.35281E-08	5.94358E-09	1.71889E-09	8.48891E-11	8.75429E-13	1.26673E-16	6.05741E-28	9.48029E-47	2.32272E-84
2.0E+16	1.26987E-08	5.65705E-09	1.65517E-09	8.25252E-11	8.54351E-13	1.23919E-16	5.93245E-28	9.26555E-47	2.27491E-84
5.0E+16	1.05782E-08	4.89851E-09	1.48097E-09	7.58722E-11	7.94332E-13	1.16022E-16	5.57285E-28	8.70504E-47	2.13729E-84
1.0E+17	7.97646E-09	3.90476E-09	1.23854E-09	6.60946E-11	7.04143E-13	1.03993E-16	5.02135E-28	7.84520E-47	1.92618E-84
2.0E+17	4.87398E-09	2.58936E-09	8.85155E-10	5.05224E-11	5.55023E-13	8.36308E-17	4.07685E-28	6.37192E-47	1.56446E-84
5.0E+17	1.62428E-09	9.52031E-10	3.65897E-10	2.36286E-11	2.77408E-13	4.37894E-17	2.18249E-28	3.41404E-47	8.38231E-85
1.0E+18	4.54105E-10	2.58205E-10	1.04641E-10	7.34631E-12	9.15228E-14	1.51281E-17	7.70764E-29	1.20671E-47	2.96277E-85
2.0E+18	8.08768E-11	2.89490E-11	1.13689E-11	8.34787E-13	1.09426E-14	1.85701E-18	9.62304E-30	1.50754E-48	3.70139E-86
5.0E+18	1.89959E-11	1.01080E-12	2.41356E-14	1.57727E-15	2.07641E-17	3.59944E-21	1.87595E-32	2.93947E-51	7.21718E-89
1.0E+19	8.09561E-12	4.35638E-13	1.41722E-15	4.80283E-20	6.31712E-22	1.09529E-25	5.70897E-37	8.94555E-56	2.19637E-93
2.0E+19	2.38741E-12	1.22251E-13	4.06649E-16	1.63975E-23	5.85059E-31	1.01439E-34	5.28729E-46	8.28480E-65	2.03413-102
5.0E+19	2.84047E-13	5.74015E-15	1.43921E-17	5.76535E-25	2.94718E-37	1.57837E-61	4.20008E-73	6.58122E-92	1.61586-129
1.0E+20	1.07654E-13	6.66417E-16	3.14633E-19	2.36667E-27	1.20319E-39	3.15692E-64	2.86175E-118	4.48415-137	1.10098-174
2.0E+20	3.14917E-14	8.63465E-17	3.49187E-20	2.43571E-30	2.01228E-44	5.27258E-69	5.9402-143	2.08175-227	5.11123-265
5.0E+20	1.36298E-15	2.23290E-19	8.63655E-23	5.94019E-33	6.85986E-50	3.37128E-83	4.43713-157	5.51778-280	0.
1.0E+21	9.11393E-18	9.31033E-23	3.92055E-27	2.69684E-37	3.11437E-54	4.15337E-88	5.76641-181	0.	0.
2.0E+21	4.13750E-22	3.79249E-27	8.39948E-36	5.5861E-46	6.41920E-63	8.56074E-97	2.03050-198	0.	0.
5.0E+21	3.87172E-35	3.54885E-40	2.98165E-50	4.86740E-72	5.62098E-89	7.49622-123	1.77801-224	0.	0.
1.0E+22	7.46758E-57	6.84485E-62	5.75085E-72	3.41064-102	2.09105-132	2.78865-166	6.61433-268	0.	0.
2.0E+22	2.77800-100	2.54634-105	2.13936-115	1.26878-145	5.31163-186	3.85921-253	0.	0.	0.
5.0E+22	1.43017-230	1.31090-235	1.10139-245	6.53195-276	0.	0.	0.	0.	0.

O3 COLUMN DENSITY

Table B17. Total Photodissociation Rate Coefficients for the Process  $\text{CO}_2 + h\nu \rightarrow \text{CO} + \text{O}(^1\text{D})$  for Wavelengths From 116.2 to 166 nm (Contd)

		O3 COLUMN DENSITY									
		2.0E+14	5.0E+14	1.0E+15	2.0E+15	5.0E+15	1.0E+16	2.0E+16	5.0E+16	1.0E+17	2.0E+17
1.0E+13	8.82221E-08	8.79581E-08	8.75211E-08	8.66585E-08	8.41591E-08	8.02701E-08	7.34105E-08	5.83252E-08	4.37704E-08	2.98301E-08	
2.0E+13	8.82167E-08	8.79527E-08	8.75157E-08	8.66532E-08	8.41539E-08	8.02650E-08	7.34055E-08	5.83210E-08	4.37669E-08	2.98278E-08	
5.0E+13	8.82006E-08	8.79366E-08	8.74937E-08	8.66372E-08	8.41381E-08	8.02496E-08	7.33910E-08	5.83082E-08	4.37567E-08	2.98208E-08	
1.0E+14	8.81738E-08	8.79098E-08	8.74730E-08	8.66107E-08	8.41119E-08	8.02240E-08	7.33666E-08	5.82870E-08	4.37395E-08	2.98091E-08	
2.0E+14	8.81202E-08	8.78563E-08	8.74196E-08	8.65575E-08	8.40596E-08	8.01729E-08	7.33179E-08	5.82446E-08	4.37053E-08	2.97857E-08	
5.0E+14	8.79597E-08	8.76960E-08	8.72597E-08	8.63984E-08	8.39028E-08	8.00200E-08	7.31721E-08	5.81176E-08	4.35028E-08	2.97157E-08	
1.0E+15	8.76933E-08	8.74301E-08	8.69944E-08	8.61344E-08	8.36427E-08	7.97651E-08	7.29302E-08	5.79069E-08	4.34327E-08	2.95996E-08	
2.0E+15	8.71649E-08	8.69024E-08	8.64681E-08	8.56107E-08	8.31267E-08	7.92625E-08	7.24502E-08	5.74889E-08	4.30952E-08	2.93691E-08	
5.0E+15	8.56136E-08	8.53534E-08	8.49229E-08	8.40732E-08	8.16116E-08	7.77840E-08	7.10409E-08	5.62614E-08	4.21037E-08	2.86911E-08	
1.0E+16	8.31372E-08	8.28807E-08	8.24563E-08	8.16187E-08	7.91930E-08	7.54235E-08	6.87908E-08	5.43007E-08	4.05187E-08	2.76052E-08	
2.0E+16	7.85653E-08	7.83156E-08	7.79024E-08	7.70871E-08	7.47276E-08	7.10652E-08	6.46355E-08	5.06776E-08	3.75855E-08	2.55877E-08	
5.0E+16	6.74127E-08	6.71794E-08	6.67935E-08	6.60325E-08	6.38334E-08	6.04304E-08	5.44922E-08	4.18188E-08	3.03855E-08	2.05860E-08	
1.0E+17	5.49301E-08	5.47151E-08	5.43595E-08	5.36587E-08	5.16375E-08	4.85219E-08	4.31265E-08	3.18623E-08	2.22316E-08	1.48077E-08	
2.0E+17	4.21191E-08	4.19228E-08	4.15984E-08	4.09596E-08	3.91210E-08	3.62994E-08	3.14552E-08	2.15994E-08	1.37268E-08	8.57459E-09	
5.0E+17	3.12219E-08	3.10436E-08	3.07491E-08	3.01694E-08	2.85041E-08	2.59585E-08	2.16222E-08	1.30026E-08	6.54646E-09	3.04871E-09	
1.0E+18	2.69793E-08	2.68113E-08	2.65338E-08	2.59879E-08	2.44211E-08	2.20304E-08	1.79729E-08	9.99335E-09	4.18178E-09	1.27610E-09	
2.0E+18	2.42727E-08	2.41140E-08	2.38519E-08	2.33655E-08	2.18582E-08	1.96063E-08	1.57966E-08	8.37242E-09	3.09299E-09	6.20073E-10	
5.0E+18	2.16428E-08	2.14958E-08	2.12531E-08	2.07760E-08	1.94088E-08	1.73297E-08	1.38239E-08	7.05849E-09	2.37318E-09	3.42583E-10	
1.0E+19	1.99580E-08	1.98205E-08	1.95934E-08	1.91471E-08	1.78686E-08	1.59254E-08	1.26528E-08	6.36014E-09	2.04692E-09	2.40989E-10	
2.0E+19	1.78972E-08	1.77733E-08	1.75687E-08	1.71668E-08	1.60146E-08	1.42642E-08	1.13171E-08	5.65592E-09	1.78723E-09	1.86582E-10	
5.0E+19	1.32281E-08	1.31364E-08	1.29850E-08	1.26873E-08	1.18346E-08	1.05388E-08	8.35753E-09	4.16853E-09	1.30843E-09	1.29718E-10	
1.0E+20	8.02109E-09	7.95546E-09	7.87361E-09	7.69307E-09	7.17592E-09	6.39010E-09	5.06723E-09	2.52684E-09	7.92565E-10	7.81748E-11	
2.0E+20	2.95034E-09	2.92988E-09	2.89609E-09	2.82968E-09	2.63944E-09	2.35037E-09	1.86375E-09	9.29273E-10	2.91368E-10	2.86597E-11	
5.0E+20	1.46878E-09	1.45860E-09	1.44178E-09	1.40871E-09	1.31400E-09	1.17008E-09	9.27814E-10	4.62587E-10	1.42521E-10	1.42521E-12	
1.0E+21	9.89656E-10	9.82792E-10	9.71457E-10	9.49179E-10	8.85336E-10	7.88393E-10	6.25154E-10	3.11686E-10	9.77094E-11	9.60225E-15	
2.0E+21	4.49303E-10	4.46187E-10	4.41041E-10	4.30927E-10	4.01954E-10	3.57930E-10	2.83819E-10	1.41505E-10	4.43600E-11	4.35941E-19	
5.0E+21	4.20441E-10	4.17525E-10	4.12709E-10	4.03245E-10	3.76133E-10	3.34917E-10	2.65587E-10	1.32415E-10	4.15104E-11	4.07937E-32	
1.0E+22	8.10925E-11	8.05301E-11	7.96013E-11	7.77758E-11	7.25467E-11	6.46011E-11	5.12252E-11	2.55396E-11	8.00632E-12	7.86809E-54	
2.0E+22	3.01670E-11	2.99578E-11	2.96123E-11	2.89333E-11	2.75467E-11	2.40321E-11	1.90561E-11	9.50093E-12	2.97841E-12	2.92699E-97	
5.0E+22	1.55306E-11	1.54229E-11	1.52450E-11	1.48954E-11	1.38939E-11	1.23722E-11	9.81049E-12	4.89127E-12	1.53335E-12	1.50887E-227	

Table B17. Total Photodissociation Rate Coefficients for the Process  $\text{CO}_2 + h\nu \rightarrow \text{CO} + \text{O}(^1\text{D})$  for Wavelengths From 116.2 to 166 nm

		O3 COLUMN DENSITY									
		1.0E+11	2.0E+11	5.0E+11	1.0E+12	2.0E+12	5.0E+12	1.0E+13	2.0E+13	5.0E+13	1.0E+14
1.0E+13	8.83988E-08	8.83987E-08	8.83984E-08	8.83984E-08	8.83980E-08	8.83971E-08	8.83945E-08	8.83900E-08	8.83812E-08	8.83546E-08	8.83104E-08
2.0E+13	8.83934E-08	8.83933E-08	8.83931E-08	8.83931E-08	8.83926E-08	8.83917E-08	8.83891E-08	8.83847E-08	8.83758E-08	8.83493E-08	8.83050E-08
5.0E+13	8.83773E-08	8.83772E-08	8.83769E-08	8.83765E-08	8.83756E-08	8.83730E-08	8.83685E-08	8.83597E-08	8.83331E-08	8.82889E-08	8.82261E-08
1.0E+14	8.83504E-08	8.83504E-08	8.83501E-08	8.83496E-08	8.83488E-08	8.83461E-08	8.83417E-08	8.83328E-08	8.83063E-08	8.82621E-08	8.82084E-08
2.0E+14	8.82968E-08	8.82967E-08	8.82964E-08	8.82950E-08	8.82930E-08	8.82915E-08	8.82890E-08	8.82792E-08	8.82526E-08	8.82084E-08	8.80478E-08
5.0E+14	8.81361E-08	8.81360E-08	8.81357E-08	8.81353E-08	8.81344E-08	8.81318E-08	8.81273E-08	8.81185E-08	8.80920E-08	8.80478E-08	8.77814E-08
1.0E+15	8.78695E-08	8.78694E-08	8.78691E-08	8.78687E-08	8.78687E-08	8.78678E-08	8.78651E-08	8.78607E-08	8.78254E-08	8.77814E-08	8.72527E-08
2.0E+15	8.73405E-08	8.73405E-08	8.73402E-08	8.73398E-08	8.73389E-08	8.73362E-08	8.73318E-08	8.73230E-08	8.72966E-08	8.72527E-08	8.67490E-08
5.0E+15	8.57877E-08	8.57876E-08	8.57874E-08	8.57869E-08	8.57861E-08	8.57834E-08	8.57791E-08	8.57703E-08	8.57442E-08	8.57006E-08	8.52230E-08
1.0E+16	8.33088E-08	8.33087E-08	8.33085E-08	8.33081E-08	8.33072E-08	8.33046E-08	8.33003E-08	8.32917E-08	8.32659E-08	8.32230E-08	8.28488E-08
2.0E+16	7.87324E-08	7.87323E-08	7.87321E-08	7.87317E-08	7.87308E-08	7.87283E-08	7.87241E-08	7.87157E-08	7.86906E-08	7.86488E-08	7.82908E-08
5.0E+16	6.75689E-08	6.75688E-08	6.75686E-08	6.75682E-08	6.75674E-08	6.75651E-08	6.75611E-08	6.75533E-08	6.75298E-08	6.74908E-08	6.71848E-08
1.0E+17	5.50741E-08	5.50741E-08	5.50739E-08	5.50735E-08	5.50728E-08	5.50706E-08	5.50670E-08	5.50598E-08	5.50381E-08	5.50021E-08	5.46848E-08
2.0E+17	4.22505E-08	4.22505E-08	4.22503E-08	4.22499E-08	4.22493E-08	4.22473E-08	4.22440E-08	4.22374E-08	4.22177E-08	4.21848E-08	4.18616E-08
5.0E+17	3.13414E-08	3.13413E-08	3.13412E-08	3.13409E-08	3.13403E-08	3.13385E-08	3.13355E-08	3.13295E-08	3.13115E-08	3.12816E-08	3.12556E-08
1.0E+18	2.70919E-08	2.70919E-08	2.70917E-08	2.70914E-08	2.70908E-08	2.70891E-08	2.70863E-08	2.70807E-08	2.70638E-08	2.70356E-08	2.69999E-08
2.0E+18	2.43791E-08	2.43790E-08	2.43789E-08	2.43786E-08	2.43781E-08	2.43755E-08	2.43738E-08	2.43685E-08	2.43525E-08	2.43259E-08	2.42900E-08
5.0E+18	2.17413E-08	2.17412E-08	2.17411E-08	2.17408E-08	2.17403E-08	2.17388E-08	2.17364E-08	2.17314E-08	2.17166E-08	2.16920E-08	2.16573E-08
1.0E+19	2.00502E-08	2.00501E-08	2.00500E-08	2.00497E-08	2.00493E-08	2.00479E-08	2.00456E-08	2.00410E-08	2.00271E-08	2.00041E-08	1.99737E-08
2.0E+19	1.79802E-08	1.79802E-08	1.79801E-08	1.79798E-08	1.79794E-08	1.79782E-08	1.79761E-08	1.79719E-08	1.79595E-08	1.79387E-08	1.79187E-08
5.0E+19	1.32896E-08	1.32896E-08	1.32895E-08	1.32893E-08	1.32890E-08	1.32881E-08	1.32865E-08	1.32835E-08	1.32742E-08	1.32588E-08	1.32357E-08
1.0E+20	8.05837E-09	8.05835E-09	8.05829E-09	8.05820E-09	8.05801E-09	8.05745E-09	8.05652E-09	8.05465E-09	8.04905E-09	8.03972E-09	8.02700E-09
2.0E+20	2.96406E-09	2.96405E-09	2.96403E-09	2.96400E-09	2.96393E-09	2.96372E-09	2.96338E-09	2.96269E-09	2.96063E-09	2.95720E-09	2.95200E-09
5.0E+20	1.47561E-10	1.47561E-10	1.47560E-10	1.47558E-10	1.47555E-10	1.47544E-10	1.47527E-10	1.47493E-10	1.47390E-10	1.47220E-10	1.46954E-10
1.0E+21	9.94256E-13	9.94254E-13	9.94247E-13	9.94235E-13	9.94212E-13	9.94143E-13	9.94028E-13	9.93797E-13	9.93106E-13	9.91954E-13	9.90737E-13
2.0E+21	4.51392E-17	4.51391E-17	4.51387E-17	4.51382E-17	4.51372E-17	4.51340E-17	4.51288E-17	4.51183E-17	4.50869E-17	4.50347E-17	4.49737E-17
5.0E+21	4.22395E-30	4.22394E-30	4.22391E-30	4.22386E-30	4.22377E-30	4.22347E-30	4.22298E-30	4.22200E-30	4.21907E-30	4.21473E-30	4.20909E-30
1.0E+22	8.14695E-52	8.14693E-52	8.14687E-52	8.14678E-52	8.14659E-52	8.14603E-52	8.14508E-52	8.14319E-52	8.13752E-52	8.12809E-52	8.11809E-52
2.0E+22	3.03073E-95	3.03072E-95	3.03070E-95	3.03066E-95	3.03059E-95	3.03038E-95	3.03003E-95	3.02933E-95	3.02722E-95	3.02371E-95	3.01955E-95
5.0E+22	1.56028E-225	1.56027E-225	1.56026E-225	1.56025E-225	1.56021E-225	1.56010E-225	1.55993E-225	1.55956E-225	1.55847E-225	1.55667E-225	1.55467E-225

O2 COLUMN DENSITY

Table B16. Total Photodissociation Rate Coefficients for the Process  $\text{CH}_4 + h\nu \rightarrow \text{CH}_3 + \text{H}$  and  $\text{CH}_4 + h\nu \rightarrow \text{CH}_2 + \text{H}_2$  for Wavelengths From 116 to 164 nm (Contd)

03 COLUMN DENSITY

	5.0E+16	1.0E+17	2.0E+17	5.0E+17	1.0E+18	2.0E+18	5.0E+18	1.0E+19	2.0E+19	5.0E+19
1.0E+13	2.97405E-06	1.00972E-06	1.47022E-07	6.68945E-09	3.08733E-10	1.04272E-11	2.81811E-13	1.70092E-15	8.96768E-20	1.65681E-32
2.0E+13	2.97404E-06	1.00971E-06	1.47020E-07	6.68929E-09	3.08726E-10	1.04267E-11	2.81800E-13	1.70086E-15	8.96737E-20	1.65676E-32
5.0E+13	2.97402E-06	1.00970E-06	1.47014E-07	6.68888E-09	3.08705E-10	1.04251E-11	2.81767E-13	1.70068E-15	8.96644E-20	1.65659E-32
1.0E+14	2.97397E-06	1.00967E-06	1.47005E-07	6.68799E-09	3.08670E-10	1.04235E-11	2.81711E-13	1.70037E-15	8.96489E-20	1.65630E-32
2.0E+14	2.97388E-06	1.00962E-06	1.46986E-07	6.68638E-09	3.08599E-10	1.04172E-11	2.81580E-13	1.69976E-15	8.96178E-20	1.65573E-32
5.0E+14	2.97362E-06	1.00947E-06	1.46929E-07	6.68149E-09	3.08388E-10	1.04015E-11	2.81262E-13	1.69793E-15	8.95247E-20	1.65402E-32
1.0E+15	2.97313E-06	1.00872E-06	1.46836E-07	6.67341E-09	3.08038E-10	1.03752E-11	2.80703E-13	1.69489E-15	8.93698E-20	1.65116E-32
2.0E+15	2.97231E-06	1.00872E-06	1.46850E-07	6.65742E-09	3.07343E-10	1.03230E-11	2.79588E-13	1.68883E-15	8.90607E-20	1.64548E-32
5.0E+15	2.96975E-06	1.00726E-06	1.46106E-07	6.61059E-09	3.05298E-10	1.01682E-11	2.76272E-13	1.67076E-15	8.81398E-20	1.62854E-32
1.0E+16	2.96565E-06	1.00493E-06	1.45243E-07	6.53631E-09	3.02018E-10	9.91629E-12	2.70837E-13	1.64108E-15	8.65261E-20	1.60068E-32
2.0E+16	2.95803E-06	1.00064E-06	1.43663E-07	6.40065E-09	2.95910E-10	9.43464E-12	2.60304E-13	1.58332E-15	8.35763E-20	1.54640E-32
5.0E+16	2.93901E-06	9.90083E-07	1.39868E-07	6.07711E-09	2.80612E-10	8.14992E-12	2.31232E-13	1.42213E-15	7.54172E-20	1.39435E-32
1.0E+17	2.91601E-06	9.77741E-07	1.35633E-07	5.72204E-09	2.62314E-10	6.44865E-12	1.90115E-13	1.18956E-15	6.34261E-20	1.17343E-32
2.0E+17	2.88619E-06	9.62535E-07	1.30789E-07	5.32920E-09	2.40182E-10	4.18544E-12	1.29258E-13	8.33362E-16	4.48667E-20	8.31044E-33
5.0E+17	2.83373E-06	9.36986E-07	1.23131E-07	4.71518E-09	2.08904E-10	1.51164E-12	4.20697E-14	2.88918E-16	1.58959E-20	2.95208E-33
1.0E+18	2.77549E-06	9.09088E-07	1.14694E-07	3.99244E-09	1.79477E-10	6.26779E-13	6.94862E-15	5.03308E-17	2.82533E-21	5.25979E-34
2.0E+18	2.69502E-06	8.71894E-07	1.03686E-07	2.99423E-09	1.39490E-10	4.00527E-13	2.10012E-16	1.57316E-18	8.95419E-23	1.66975E-35
5.0E+18	2.55052E-06	8.11447E-07	8.81038E-08	1.56412E-09	7.64515E-11	2.35014E-13	1.48820E-20	5.01132E-23	2.86337E-27	5.34200E-40
1.0E+19	2.39877E-06	7.56935E-07	7.80292E-08	7.53982E-09	3.59062E-11	1.15361E-13	4.41494E-21	1.61778E-30	9.23199E-35	1.72236E-47
2.0E+19	2.16097E-06	6.79243E-07	6.80571E-08	2.87603E-10	1.07921E-11	3.40741E-14	1.37660E-21	6.86985E-34	9.59700E-50	1.79046E-62
5.0E+19	1.59844E-06	5.01530E-07	4.95741E-08	8.04970E-11	8.25926E-13	1.34214E-15	4.88948E-23	2.50008E-35	6.55496E-60	2.01134E-107
1.0E+20	9.69103E-07	3.03930E-07	2.99520E-08	3.77365E-11	1.74347E-13	7.11941E-17	2.03812E-25	1.02089E-37	2.67860E-62	4.83842E-136
2.0E+20	3.56417E-07	1.11747E-07	1.09914E-08	1.15633E-11	2.23765E-14	8.91530E-18	6.13352E-28	1.71209E-42	4.47371E-67	8.08099E-141
5.0E+20	1.77430E-08	5.56222E-09	5.46641E-10	5.21449E-13	5.84820E-17	2.19873E-20	1.51205E-30	1.74615E-47	4.41294E-81	3.76484E-155
1.0E+21	1.19551E-10	3.74776E-11	3.68306E-12	3.49569E-15	4.4764E-20	9.97961E-25	6.86469E-35	7.92750E-52	1.05722E-85	4.79272E-179
2.0E+21	5.42760E-15	1.70148E-15	1.67210E-16	1.58699E-19	1.45465E-24	2.17916E-33	1.41492E-43	1.63398E-60	2.17910E-94	5.16854E-196
5.0E+21	5.07895E-28	1.59218E-28	1.56459E-29	1.48504E-32	1.26120E-37	1.14364E-47	1.23897E-69	1.43060E-86	1.90813E-120	4.52584E-222
1.0E+22	9.79602E-50	3.07092E-50	3.01790E-51	2.86428E-54	2.62542E-59	2.20581E-69	1.30819E-99	5.32267E-130	7.09839E-164	1.68365E-265
2.0E+22	3.64419E-93	1.14240E-93	1.12288E-94	1.06553E-97	9.76677E-103	8.20576E-113	4.86657E-143	2.03734E-193	9.82343E-251	3.13457E-353
5.0E+22	1.87610E-223	5.86132E-224	5.77979E-225	5.48558E-228	5.02813E-233	4.22449E-243	2.50541E-273	1.55808E-50	9.97526E-69	2.97413E-154

02 COLUMN DENSITY

Table B16. Total Photodissociation Rate Coefficients for the Process  $\text{CH}_4 + h\nu \rightarrow \text{CH}_3 + \text{H}$  and  $\text{CH}_4 + h\nu \rightarrow \text{CH}_2 + \text{H}_2$  for Wavelengths From 116 to 164 nm (Contd)

O3 COLUMN DENSITY											
	2.0E+13	5.0E+13	1.0E+14	2.0E+14	5.0E+14	1.0E+15	2.0E+15	5.0E+15	1.0E+16	2.0E+16	
1.0E+13	9.08194E-06	9.07579E-06	9.06555E-06	9.04511E-06	8.98408E-06	8.88328E-06	8.68510E-06	8.11710E-06	7.25294E-06	5.79465E-06	
2.0E+13	9.08192E-06	9.07577E-06	9.06554E-06	9.04510E-06	8.98406E-06	8.88326E-06	8.68509E-06	8.11708E-06	7.25293E-06	5.79464E-06	
5.0E+13	9.08187E-06	9.07573E-06	9.06549E-06	9.04505E-06	8.98401E-06	8.88321E-06	8.68504E-06	8.11704E-06	7.25289E-06	5.79460E-06	
1.0E+14	9.08179E-06	9.07564E-06	9.06541E-06	9.04497E-06	8.98393E-06	8.88313E-06	8.68496E-06	8.11696E-06	7.25281E-06	5.79454E-06	
2.0E+14	9.08163E-06	9.07548E-06	9.06524E-06	9.04480E-06	8.98377E-06	8.88297E-06	8.68480E-06	8.11680E-06	7.25267E-06	5.79441E-06	
5.0E+14	9.08113E-06	9.07499E-06	9.06475E-06	9.04431E-06	8.98328E-06	8.88248E-06	8.68432E-06	8.11634E-06	7.25224E-06	5.79403E-06	
1.0E+15	9.08031E-06	9.07417E-06	9.06393E-06	9.04349E-06	8.98246E-06	8.88167E-06	8.68352E-06	8.11557E-06	7.25152E-06	5.79340E-06	
2.0E+15	9.07869E-06	9.07254E-06	9.06231E-06	9.04187E-06	8.98085E-06	8.88007E-06	8.68193E-06	8.11405E-06	7.25009E-06	5.79214E-06	
5.0E+15	9.07390E-06	9.06775E-06	9.05752E-06	9.03709E-06	8.97609E-06	8.87534E-06	8.67727E-06	8.10957E-06	7.24589E-06	5.78844E-06	
1.0E+16	9.06620E-06	9.06006E-06	9.04983E-06	9.02941E-06	8.96844E-06	8.86774E-06	8.66977E-06	8.10236E-06	7.23914E-06	5.78251E-06	
2.0E+16	9.05178E-06	9.04565E-06	9.03543E-06	9.01503E-06	8.95411E-06	8.85351E-06	8.65573E-06	8.10888E-06	7.22652E-06	5.77144E-06	
5.0E+16	9.01504E-06	9.00892E-06	9.00873E-06	9.02941E-06	8.97838E-06	8.91762E-06	8.81727E-06	8.61999E-06	8.05459E-06	7.19451E-06	
1.0E+17	8.96886E-06	8.96276E-06	8.95260E-06	8.93232E-06	8.91766E-06	8.91755E-06	8.91755E-06	8.91755E-06	8.91755E-06	8.91755E-06	
2.0E+17	8.90571E-06	8.89964E-06	8.88953E-06	8.86935E-06	8.80909E-06	8.70957E-06	8.51393E-06	8.27097E-06	7.95327E-06	7.10056E-06	
5.0E+17	8.78855E-06	8.78254E-06	8.77253E-06	8.75255E-06	8.69287E-06	8.59433E-06	8.4061E-06	8.0061E-06	7.84552E-06	7.00142E-06	
1.0E+18	8.65430E-06	8.64836E-06	8.63847E-06	8.61872E-06	8.55976E-06	8.46238E-06	8.27097E-06	7.72252E-06	7.42252E-06	6.88866E-06	
2.0E+18	8.45984E-06	8.45401E-06	8.44430E-06	8.42492E-06	8.36703E-06	8.27144E-06	8.08355E-06	7.54522E-06	7.2692E-06	6.72692E-06	
5.0E+18	8.07597E-06	8.07037E-06	8.06105E-06	8.04245E-06	7.98690E-06	7.89516E-06	7.71484E-06	7.19828E-06	6.41325E-06	5.09131E-06	
1.0E+19	7.62587E-06	7.62057E-06	7.61175E-06	7.59414E-06	7.54156E-06	7.45473E-06	7.28406E-06	6.79516E-06	6.05224E-06	4.80145E-06	
2.0E+19	6.88190E-06	6.87711E-06	6.86914E-06	6.85324E-06	6.80573E-06	6.72730E-06	6.57313E-06	6.13150E-06	5.46043E-06	4.33069E-06	
5.0E+19	5.09443E-06	5.09088E-06	5.08498E-06	5.07320E-06	5.03802E-06	4.97993E-06	4.86576E-06	4.53870E-06	4.04172E-06	3.20510E-06	
1.0E+20	3.08932E-06	3.08717E-06	3.08359E-06	3.07644E-06	3.05511E-06	3.01988E-06	2.95063E-06	2.75228E-06	2.45087E-06	1.94347E-06	
2.0E+20	1.13635E-06	1.13556E-06	1.13424E-06	1.13162E-06	1.12377E-06	1.11081E-06	1.08533E-06	1.01237E-06	9.01491E-07	7.14841E-07	
5.0E+20	5.65726E-08	5.65333E-08	5.64677E-08	5.63369E-08	5.59461E-08	5.53009E-08	5.40327E-08	5.03999E-08	4.48799E-08	3.55873E-08	
1.0E+21	3.81183E-10	3.80917E-10	3.80476E-10	3.79594E-10	3.76961E-10	3.72614E-10	3.64069E-10	3.39591E-10	3.02397E-10	2.39785E-10	
2.0E+21	1.73057E-14	1.72936E-14	1.72736E-14	1.72335E-14	1.71140E-14	1.69166E-14	1.65287E-14	1.54174E-14	1.37288E-14	1.08862E-14	
5.0E+21	1.61940E-27	1.61827E-27	1.61640E-27	1.61265E-27	1.60146E-27	1.58469E-27	1.54669E-27	1.44270E-27	1.28469E-27	1.01869E-27	
2.0E+22	3.12341E-49	3.12124E-49	3.11762E-49	3.11040E-49	3.08882E-49	3.05330E-49	2.98318E-49	2.78261E-49	2.47785E-49	1.96480E-49	
5.0E+22	1.16193E-92	1.16113E-92	1.15978E-92	1.15709E-92	1.14907E-92	1.13561E-92	1.10977E-92	1.03515E-92	9.21779E-93	7.30921E-93	
2.0E+23	5.98187E-223	5.97771E-223	5.97078E-223	5.95694E-223	5.91562E-223	5.84740E-223	5.71330E-223	5.32918E-223	4.74550E-223	3.76293E-223	

O2 COLUMN DENSITY



Table B16. Total Photodissociation Rate Coefficients for the Process  $\text{CH}_4 + h\nu \rightarrow \text{CH}_3 + \text{H}$  and  $\text{CH}_4 + h\nu \rightarrow \text{CH}_2 + \text{H}_2$  for Wavelengths From 116 to 164 nm

O3 COLUMN DENSITY

	1.0E+10	2.0E+10	5.0E+10	1.0E+11	2.0E+11	5.0E+11	1.0E+12	2.0E+12	5.0E+12	1.0E+13
1.0E+13	9.08604E-06	9.08604E-06	9.08603E-06	9.08602E-06	9.08600E-06	9.08594E-06	9.08583E-06	9.08563E-06	9.08501E-06	9.08399E-06
2.0E+13	9.08602E-06	9.08602E-06	9.08601E-06	9.08600E-06	9.08598E-06	9.08592E-06	9.08582E-06	9.08561E-06	9.08500E-06	9.08397E-06
5.0E+13	9.08597E-06	9.08597E-06	9.08596E-06	9.08595E-06	9.08593E-06	9.08587E-06	9.08577E-06	9.08556E-06	9.08495E-06	9.08392E-06
1.0E+14	9.08589E-06	9.08589E-06	9.08588E-06	9.08587E-06	9.08585E-06	9.08579E-06	9.08569E-06	9.08548E-06	9.08487E-06	9.08384E-06
2.0E+14	9.08572E-06	9.08572E-06	9.08572E-06	9.08571E-06	9.08569E-06	9.08562E-06	9.08552E-06	9.08532E-06	9.08470E-06	9.08368E-06
5.0E+14	9.08523E-06	9.08523E-06	9.08522E-06	9.08521E-06	9.08519E-06	9.08513E-06	9.08503E-06	9.08482E-06	9.08421E-06	9.08318E-06
1.0E+15	9.08441E-06	9.08441E-06	9.08440E-06	9.08439E-06	9.08437E-06	9.08431E-06	9.08421E-06	9.08400E-06	9.08339E-06	9.08236E-06
2.0E+15	9.08279E-06	9.08278E-06	9.08278E-06	9.08277E-06	9.08275E-06	9.08269E-06	9.08258E-06	9.08238E-06	9.08176E-06	9.08074E-06
5.0E+15	9.07799E-06	9.07799E-06	9.07799E-06	9.07798E-06	9.07796E-06	9.07789E-06	9.07779E-06	9.07759E-06	9.07697E-06	9.07595E-06
1.0E+16	9.07029E-06	9.07029E-06	9.07028E-06	9.07027E-06	9.07025E-06	9.07019E-06	9.07009E-06	9.06988E-06	9.06927E-06	9.06825E-06
2.0E+16	9.05587E-06	9.05587E-06	9.05587E-06	9.05586E-06	9.05584E-06	9.05577E-06	9.05567E-06	9.05547E-06	9.05485E-06	9.05383E-06
5.0E+16	9.01912E-06	9.01912E-06	9.01912E-06	9.01911E-06	9.01909E-06	9.01902E-06	9.01892E-06	9.01872E-06	9.01811E-06	9.01708E-06
1.0E+17	8.97293E-06	8.97292E-06	8.97292E-06	8.97291E-06	8.97289E-06	8.97283E-06	8.97273E-06	8.97252E-06	8.97191E-06	8.97089E-06
2.0E+17	8.90976E-06	8.90975E-06	8.90975E-06	8.90974E-06	8.90972E-06	8.90966E-06	8.90956E-06	8.90935E-06	8.90875E-06	8.90773E-06
5.0E+17	8.79256E-06	8.79255E-06	8.79255E-06	8.79254E-06	8.79252E-06	8.79246E-06	8.79236E-06	8.79216E-06	8.79156E-06	8.79055E-06
1.0E+18	8.65826E-06	8.65826E-06	8.65825E-06	8.65824E-06	8.65822E-06	8.65816E-06	8.65806E-06	8.65787E-06	8.65727E-06	8.65628E-06
2.0E+18	8.46373E-06	8.46373E-06	8.46372E-06	8.46371E-06	8.46369E-06	8.46363E-06	8.46353E-06	8.46334E-06	8.46276E-06	8.46178E-06
5.0E+18	8.07970E-06	8.07970E-06	8.07969E-06	8.07968E-06	8.07966E-06	8.07961E-06	8.07952E-06	8.07933E-06	8.07877E-06	8.07784E-06
1.0E+19	7.62940E-06	7.62940E-06	7.62939E-06	7.62938E-06	7.62937E-06	7.62931E-06	7.62922E-06	7.62905E-06	7.62852E-06	7.62763E-06
2.0E+19	6.88509E-06	6.88508E-06	6.88508E-06	6.88507E-06	6.88505E-06	6.88501E-06	6.88493E-06	6.88477E-06	6.88429E-06	6.88349E-06
5.0E+19	5.09679E-06	5.09679E-06	5.09678E-06	5.09677E-06	5.09677E-06	5.09673E-06	5.09667E-06	5.09655E-06	5.09620E-06	5.09561E-06
1.0E+20	3.09075E-06	3.09075E-06	3.09075E-06	3.09074E-06	3.09074E-06	3.09072E-06	3.09068E-06	3.09061E-06	3.09039E-06	3.09003E-06
2.0E+20	1.13688E-06	1.13688E-06	1.13688E-06	1.13687E-06	1.13687E-06	1.13686E-06	1.13685E-06	1.13683E-06	1.13675E-06	1.13661E-06
5.0E+20	5.65989E-08	5.65989E-08	5.65988E-08	5.65988E-08	5.65986E-08	5.65982E-08	5.65976E-08	5.65963E-08	5.65923E-08	5.65858E-08
1.0E+21	3.81359E-10	3.81359E-10	3.81359E-10	3.81359E-10	3.81358E-10	3.81355E-10	3.81351E-10	3.81342E-10	3.81315E-10	3.81271E-10
2.0E+21	1.73137E-14	1.73137E-14	1.73137E-14	1.73137E-14	1.73136E-14	1.73135E-14	1.73133E-14	1.73129E-14	1.73117E-14	1.73097E-14
5.0E+21	1.62015E-27	1.62015E-27	1.62015E-27	1.62015E-27	1.62014E-27	1.62013E-27	1.62011E-27	1.62007E-27	1.61996E-27	1.61977E-27
1.0E+22	3.12486E-49	3.12486E-49	3.12486E-49	3.12485E-49	3.12485E-49	3.12483E-49	3.12479E-49	3.12472E-49	3.12450E-49	3.12414E-49
2.0E+22	1.16247E-92	1.16247E-92	1.16247E-92	1.16247E-92	1.16247E-92	1.16246E-92	1.16245E-92	1.16242E-92	1.16234E-92	1.16220E-92
5.0E+22	5.98464E-223	5.98464E-223	5.98464E-223	5.98463E-223	5.98462E-223	5.98457E-223	5.98451E-223	5.98437E-223	5.98395E-223	5.98326E-223

Table B15. Total Photodissociation Rate Coefficients for the Process  $\text{HNO}_3 + h\nu \rightarrow \text{OH} + \text{NO}_2$  for Wavelengths From 192 to 325 nm (Contd)

O3 COLUMN DENSITY			
	5.0E+18	1.0E+19	2.0E+19
1.0E+17	1.13617E-05	2.63273E-06	5.63548E-07
2.0E+17	1.13616E-05	2.63273E-06	5.63547E-07
5.0E+17	1.13616E-05	2.63272E-06	5.63547E-07
1.0E+18	1.13615E-05	2.63270E-06	5.63546E-07
2.0E+18	1.13613E-05	2.63266E-06	5.63545E-07
5.0E+18	1.13606E-05	2.63255E-06	5.63541E-07
1.0E+19	1.13596E-05	2.63236E-06	5.63535E-07
2.0E+19	1.13575E-05	2.63199E-06	5.63523E-07
5.0E+19	1.13512E-05	2.63089E-06	5.63486E-07
1.0E+20	1.13409E-05	2.62909E-06	5.63426E-07
2.0E+20	1.13210E-05	2.62559E-06	5.63309E-07
5.0E+20	1.13110E-05	2.62442E-06	5.63288E-07
1.0E+21	1.12486E-05	2.61386E-06	5.62947E-07
2.0E+21	1.11479E-05	2.59721E-06	5.62421E-07
5.0E+21	1.09320E-05	2.56332E-06	5.61404E-07
1.0E+22	1.04726E-05	2.48729E-06	5.58976E-07

O2 COLUMN DENSITY

Table B20. Total Photodissociation Rate Coefficients for the Process  $\text{HO}_2 + h\nu \rightarrow \text{O}_2 + \text{H}$  for Wavelengths From 180 to 274 nm (Contd)

		O3 COLUMN DENSITY							
		5.0E+18	1.0E+19	2.0E+19	5.0E+19	1.0E+20	2.0E+20	5.0E+20	1.0E+21
1.0E+17	2.07907E-05	2.61694E-06	6.76290E-08	2.73147E-12	1.93021E-19	1.13611E-33	2.83493E-76	3.46592-147	
2.0E+17	2.07901E-05	2.61591E-06	6.76288E-08	2.73146E-12	1.93020E-19	1.13610E-33	2.83492E-76	3.46592-147	
5.0E+17	2.07884E-05	2.61683E-06	6.76281E-08	2.73145E-12	1.93019E-19	1.13610E-33	2.83491E-76	3.46590-147	
1.0E+18	2.07857E-05	2.61671E-06	6.76269E-08	2.73142E-12	1.93017E-19	1.13609E-33	2.83489E-76	3.46587-147	
2.0E+18	2.07810E-05	2.61648E-06	6.76246E-08	2.73136E-12	1.93014E-19	1.13607E-33	2.83484E-76	3.46582-147	
5.0E+18	2.07695E-05	2.61584E-06	6.76178E-08	2.73119E-12	1.93003E-19	1.13601E-33	2.83471E-76	3.46565-147	
1.0E+19	2.07543E-05	2.61491E-06	6.76067E-08	2.73091E-12	1.92986E-19	1.13592E-33	2.83448E-76	3.46537-147	
2.0E+19	2.07301E-05	2.61326E-06	6.75849E-08	2.73035E-12	1.92951E-19	1.13573E-33	2.83403E-76	3.46482-147	
5.0E+19	2.06766E-05	2.60908E-06	6.75224E-08	2.72868E-12	1.92847E-19	1.13517E-33	2.83268E-76	3.46316-147	
1.0E+20	2.06103E-05	2.60322E-06	6.74242E-08	2.72592E-12	1.92674E-19	1.13425E-33	2.83043E-76	3.46040-147	
2.0E+20	2.05089E-05	2.59329E-06	6.72410E-08	2.72054E-12	1.92334E-19	1.13240E-33	2.82596E-76	3.45491-147	
5.0E+20	2.04746E-05	2.59002E-06	6.71908E-08	2.71987E-12	1.92320E-19	1.13240E-33	2.82596E-76	3.45491-147	
1.0E+21	2.02330E-05	2.56402E-06	6.66700E-08	2.70405E-12	1.91321E-19	1.12696E-33	2.81276E-76	3.43872-147	
2.0E+21	1.99118E-05	2.52725E-06	6.58848E-08	2.67907E-12	1.89725E-19	1.11818E-33	2.79132E-76	3.41247-147	
5.0E+21	1.92876E-05	2.45557E-06	6.43467E-08	2.63067E-12	1.86663E-19	1.10128E-33	2.74998E-76	3.36199-147	
1.0E+22	1.81656E-05	2.31546E-06	6.09523E-08	2.50741E-12	1.78360E-19	1.05394E-33	2.63347E-76	3.21992-147	
2.0E+22	1.64708E-05	2.10592E-06	5.58782E-08	2.32054E-12	1.65729E-19	9.81483E-34	2.45436E-76	3.00131-147	
5.0E+22	1.29553E-05	1.69200E-06	4.63024E-08	1.98438E-12	1.43372E-19	8.53578E-34	2.13714E-76	2.61328-147	
1.0E+23	8.11202E-06	1.06391E-06	3.31736E-09	1.71564E-13	1.31614E-20	5.67955E-34	1.42349E-76	1.73821-147	
2.0E+23	3.52091E-06	4.80146E-07	1.41310E-08	6.52939E-13	4.85590E-20	2.93040E-34	7.34125E-77	8.92785-148	
5.0E+23	5.60412E-07	9.47195E-08	3.31736E-09	1.71564E-13	1.31614E-20	5.67955E-34	1.42349E-76	1.73821-147	
1.0E+24	1.09755E-08	1.96109E-09	7.17647E-11	3.82061E-15	2.95631E-22	1.80327E-36	4.40430E-79	5.10966-150	
2.0E+24	8.94604E-10	1.68185E-10	6.17187E-12	3.23815E-16	2.47282E-23	1.48928E-37	3.56769E-80	4.02630-151	
5.0E+24	8.94366E-10	1.68179E-10	6.17183E-12	3.23815E-16	2.47282E-23	1.48928E-37	3.56769E-80	4.02630-151	
1.0E+25	8.94366E-10	1.68179E-10	6.17183E-12	3.23815E-16	2.47282E-23	1.48928E-37	3.56769E-80	4.02630-151	
2.0E+25	8.94366E-10	1.68179E-10	6.17183E-12	3.23815E-16	2.47282E-23	1.48928E-37	3.56769E-80	4.02630-151	

Table B21. EUV Solar Fluxes and Cross Sections

WAVELENGTH Å	PHOTON FLUX $\times 10^9$ PH/CM/SEC	O <sub>2</sub> $\times 10^{-16}$	N <sub>2</sub> $\times 10^{-16}$	O $\times 10^{-16}$	O <sub>2</sub> $\times 10^{-16}$	N <sub>2</sub> $\times 10^{-16}$	O $\times 10^{-16}$	O <sub>2</sub> $\times 10^{-16}$	N <sub>2</sub> $\times 10^{-16}$	O $\times 10^{-16}$	H $\times 10^{-16}$	HE $\times 10^{-16}$
1215.7	251.4000	.0100	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
1025.7	2.6670	1.5800	.0005	0.0000	.9800	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
991.0	.5994	1.6000	1.5000	0.0000	1.1000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
977.0	4.4070	4.0000	.7000	0.0000	2.5000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
972.5	.6066	32.0000	360.0000	0.0000	25.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
949.7	.3044	6.3000	5.2000	0.0000	4.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
944.5	.1340	3.2000	1.0000	0.0000	2.6000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
937.8	.1635	5.0000	10.0000	0.0000	3.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
933.4	.1433	18.0000	.2000	0.0000	8.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
930.7	.2631	26.0000	4.8000	0.0000	17.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
926.2	.1129	6.7000	2.0000	0.0000	6.7000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	.0284	7.4000	100.0000	0.0000	3.3000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	.1134	7.4000	50.0000	0.0000	3.3000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
911-1027	.3970	7.4000	10.0000	0.0000	3.3000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	.5388	7.4000	2.0000	0.0000	3.3000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	.3403	7.4000	.2000	0.0000	3.3000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
890-911	1.1064	9.3000	10.0000	3.0000	4.5000	0.0000	3.0000	0.0000	0.0000	3.0000	6.1000	0.0000
	2.5816	9.3000	2.0000	3.0000	4.5000	0.0000	3.0000	0.0000	0.0000	3.0000	6.1000	0.0000
904	.3625	11.0000	6.3000	3.0000	6.3000	0.0000	3.0000	0.0000	0.0000	3.0000	6.1200	0.0000
860-890	1.1852	7.0000	10.0000	2.9000	4.0000	0.0000	2.9000	0.0000	0.0000	2.9000	5.8000	0.0000
	1.7778	7.0000	2.0000	2.9000	4.0000	0.0000	2.9000	0.0000	0.0000	2.9000	5.8000	0.0000
830- 60	.5436	9.0000	10.0000	2.8000	4.0000	0.0000	2.8000	0.0000	0.0000	2.8000	5.2000	0.0000
	.8154	9.0000	2.0000	2.8000	4.0000	0.0000	2.8000	0.0000	0.0000	2.8000	5.2000	0.0000
835.3	.0950	10.0000	20.0000	2.6000	3.7000	0.0000	2.6000	0.0000	0.0000	2.6000	5.0000	0.0000
835.1	.0950	10.0000	41.0000	2.6000	3.7000	0.0000	2.6000	0.0000	0.0000	2.6000	5.0000	0.0000
834.5	.0950	11.0000	7.5000	2.6000	4.0000	0.0000	2.6000	0.0000	0.0000	2.6000	5.0000	0.0000
833.7	.0950	13.0000	6.0000	2.6000	5.1000	0.0000	2.6000	0.0000	0.0000	2.6000	5.0000	0.0000
833.3	.0950	15.0000	2.3000	2.6000	6.0000	0.0000	2.6000	0.0000	0.0000	2.6000	5.0000	0.0000
832.9	.0950	26.0000	7.0000	2.6000	10.0000	0.0000	2.6000	0.0000	0.0000	2.6000	5.0000	0.0000
832.8	.0950	26.0000	2.1000	2.6000	10.0000	0.0000	2.6000	0.0000	0.0000	2.6000	5.0000	0.0000
	.0654	19.0000	50.0000	2.9000	7.0000	0.0000	2.9000	0.0000	0.0000	2.9000	4.8000	0.0000
800-830	.1962	19.0000	10.0000	2.9000	7.0000	0.0000	2.9000	0.0000	0.0000	2.9000	4.8000	0.0000
	.3924	19.0000	2.0000	2.9000	7.0000	0.0000	2.9000	0.0000	0.0000	2.9000	4.8000	0.0000
	.0027	26.0000	100.0000	3.0000	10.0000	65.0000	3.0000	0.0000	65.0000	3.0000	4.3000	0.0000
770-800	.0539	26.0000	50.0000	3.0000	10.0000	33.0000	3.0000	0.0000	33.0000	3.0000	4.3000	0.0000
	.2129	26.0000	25.0000	3.0000	10.0000	16.0000	3.0000	0.0000	16.0000	3.0000	4.3000	0.0000
790.1	.3814	28.0000	25.0000	2.9000	10.0000	11.0000	2.9000	0.0000	11.0000	2.9000	4.4000	0.0000
787.7	.2107	24.0000	10.0000	2.9000	13.0000	8.0000	2.9000	0.0000	8.0000	2.9000	4.3000	0.0000
786.5	.1103	23.0000	44.0000	2.9000	11.0000	17.0000	2.9000	0.0000	17.0000	2.9000	4.3000	0.0000
780.3	.2289	28.0000	30.0000	2.0000	11.0000	35.0000	3.0000	0.0000	35.0000	3.0000	3.9000	0.0000
770.4	.2869	18.0000	12.0000	7.0000	11.0000	17.0000	3.0000	0.0000	17.0000	3.0000	4.0000	0.0000
740-770	.0128	19.0000	50.0000	3.0000	11.0000	35.0000	3.0000	0.0000	35.0000	3.0000	3.9000	0.0000
	.1698	19.0000	24.0000	3.3000	11.0000	17.0000	3.3000	0.0000	17.0000	3.3000	3.9000	0.0000
765.1	.1659	23.0000	67.0000	3.0000	12.0000	51.0000	3.0000	0.0000	51.0000	3.0000	4.0000	0.0000
760.4	.0934	20.0000	40.0000	2.9000	10.0000	22.0000	2.9000	0.0000	22.0000	2.9000	3.9000	0.0000
710-740	.0895	30.0000	23.0000	5.5000	22.0000	21.0000	5.5000	0.0000	21.0000	5.5000	3.5000	0.0000

Table B21. EUV Solar Fluxes and Cross Sections (Contd)

WAVELENGTH A	PHOTON FLUX $\times 10^8$ PH/CM /SEC	O2 $\times 10^{-18}$	N2 $\times 10^{-18}$	O $\times 10^{-18}$	O2 $\times 10^{-18}$	N2 $\times 10^{-18}$	D $\times 10^{-18}$	H $\times 10^{-18}$	HE $\times 10^{-18}$
680-710	.1290	24.0000	23.0000	6.5000	20.0000	21.0000	6.5000	3.1000	0.0000
703	.0673	26.0000	23.0000	6.5000	23.0000	21.0000	6.5000	3.1000	0.0000
630-680	.0004	22.0000	50.0000	6.0000	19.0000	50.0000	6.0000	3.4000	0.0000
	.0627	22.0000	24.0000	6.0000	19.0000	24.0000	6.0000	3.4000	0.0000
629.7	1.5203	30.0000	23.0000	9.0000	23.0000	23.0000	9.0000	2.4000	0.0000
625.3	.2103	25.0000	24.0000	9.0000	24.0000	23.0000	9.0000	2.4000	0.0000
609.8	.5302	27.0000	24.0000	9.0000	25.0000	24.0000	9.0000	2.1000	0.0000
599.6	.1600	28.0000	23.0000	9.0000	27.0000	22.0000	9.0000	2.0000	0.0000
584.3	1.2700	23.0000	23.0000	9.5000	23.0000	23.0000	9.5000	1.9000	0.0000
554	.7200	26.0000	25.0000	9.5000	25.0000	24.0000	9.5000	1.6000	0.0000
521.0	.0600	21.0000	24.0000	9.3000	21.0000	23.0000	9.3000	1.3000	0.0000
507	.1600	23.0000	23.0000	9.3000	22.0000	23.0000	9.3000	1.2000	0.0000
425-504	.4429	22.0000	23.0000	9.5000	22.0000	23.0000	9.5000	1.0000	0.0000
499.3	.1139	22.0000	23.0000	9.5000	22.0000	23.0000	9.5000	1.2000	0.0000
465.2	.2724	21.0000	23.0000	10.0000	21.0000	23.0000	10.0000	1.0000	0.0000
417	.0782	20.0000	21.0000	10.5000	20.0000	21.0000	10.5000	.7400	5.6000
370-460	.1715	20.0000	20.0000	10.0000	20.0000	20.0000	10.0000	.7600	5.6000
368.1	.6500	18.0000	17.0000	9.5000	18.0000	17.0000	9.5000	.5400	4.6000
365	.1500	18.0000	16.0000	9.5000	18.0000	16.0000	9.5000	.5000	4.6000
360.7	.3200	17.0000	16.0000	9.5000	17.0000	16.0000	9.5000	.4000	4.1000
335.4	.1600	17.0000	14.0000	9.5000	17.0000	14.0000	9.5000	.3000	3.5000
303.8	7.7000	17.0000	12.0000	8.5000	17.0000	12.0000	8.5000	.2500	2.7000
284.1	.2100	15.0000	11.0000	8.5000	15.0000	11.0000	8.5000	.3700	3.6000
270-370	1.1770	16.0000	13.0000	7.5000	16.0000	13.0000	7.5000	.1900	2.1000
230-270	2.3960	13.0000	10.0000	7.5000	22.0000	13.0000	15.0000	.1100	1.5000
205-230	.6035	10.0000	7.0000	6.5000	20.0000	14.0000	13.0000	.0740	1.0000
176-205	2.0881	6.4000	5.6000	4.0000	12.8000	11.0000	8.0000	.7300	.3800
153-176	1.2133	5.2000	4.4000	3.0000	10.4000	9.0000	6.0000	.0250	.0085
100-153	.2017	3.0000	2.7000	1.7000	7.5000	5.4000	5.1000	.0063	.1500
80-90	.0942	2.0000	1.2000	1.0000	6.0000	3.6000	3.0000	.0042	.1000
76.0	.1070	1.5000	.8900	.7500	4.5000	2.7000	2.3000	.0045	.1100
70-80	.0648	1.1000	.6700	.5500	4.4000	2.6000	2.3000	.0025	.0900
60-70	.0742	.8000	.4500	.3900	4.0000	1.8000	2.0000	.0012	.0200
50-60	.0643	.5100	.3000	.2500	3.1000	1.4000	1.5000	0.0000	.0190
40-50	.0284	.3100	.1800	.1600	2.2000	1.0000	1.1000	0.0000	.0050
10-40	.0040	.1500	.0900	.0800	1.5000	.9000	.8000	0.0000	0.0000
9	0.0000	.1000	.0650	.0500	3.9000	2.5000	2.0000	0.0000	0.0000
7	0.0000	.0520	.0300	.0260	2.6000	1.5000	1.3000	0.0000	0.0000
5	0.0000	.0200	.0120	.0100	1.4000	.8400	.7100	0.0000	0.0000
3	0.0000	.0046	.0028	.0023	.5400	.3300	.2700	0.0000	0.0000
1	0.0000	.0002	.0001	.0001	.0600	.0350	.2300	0.0000	0.0000

Table B22. Electron Impact Ionization Cross Sections

PROCESS	I	$c_0 f_0$	$\Omega$	$\nu$	$\gamma$	P
$e + N_2 \rightarrow N + N^+ + 2e$	25.0	0.380	0.96	2.0	1.0	1.2
$e + O_2 \rightarrow O + O^+(^4S) + 2e$	18.0	0.400	0.93	3.0	1.0	1.1
$e + O_2 \rightarrow O + O^+(^2D) + 2e$	22.0	0.250	0.93	3.0	1.0	1.1
$e + O \rightarrow O^+(^4S) + 2e$	14.0	0.290	0.85	1.0	0.3	1.2
$e + O \rightarrow O^+(^2D) + 2e$	17.0	0.360	0.85	1.0	0.3	1.2
$e + N_2 \rightarrow N_2^+ + 2e$	15.0	0.370	0.80	3.0	1.0	1.2
$e + O_2 \rightarrow O_2^+ + 2e$	12.0	0.058	0.80	2.0	1.0	1.1

Table B23. Rate Coefficients for Energetic Electron Impact Reactions

1. $N_2 + e \rightarrow N + N^+ + 2e$					
z(km)	Solar Zenith Angle				
	49.78°	61.50°	76.22°	97.16°	
95	0	0	0	0	
100	3.54E-12	7.83E-13	3.37E-15	0	
130	7.46E-10	5.79E-10	3.07E-10	0	
170	2.60E-09	2.25E-09	1.45E-09	0	
210	3.92E-09	3.69E-09	3.03E-09	0	
250	4.73E-09	4.61E-09	4.22E-09	0	
300	5.27E-09	5.21E-09	5.04E-09	0	
400	2.63E-09	2.60E-09	2.52E-09	0	
2. $O_2 + e \rightarrow O + O^+(^4S) + 2e$					
z(km)	Solar Zenith Angle				
	49.78°	61.50°	76.22°	97.16°	
95	0	0	0	0	
100	4.38E-12	9.68E-13	4.16E-15	0	
130	1.00E-09	7.49E-10	3.87E-10	0	
170	4.60E-09	3.84E-09	2.20E-09	0	
210	7.31E-09	6.81E-09	5.35E-09	0	
250	8.86E-09	8.59E-09	7.73E-09	0	
300	9.76E-09	9.61E-09	9.25E-09	0	
400	4.38E-09	4.81E-09	4.62E-09	0	

Table B23. Rate Coefficients for Energetic Electron Impact Reactions (Contd)

3. $O_2 + e \rightarrow O + O^+(^2D) + 2e$					
z(km)	Solar Zenith Angle				
	49.78°	61.50°	76.22°	97.16°	
95	0	0	0	0	
100	2.06E-12	4.56E-13	1.97E-15	0	
130	4.11E-10	3.22E-10	1.74E-10	0	
170	1.35E-09	1.17E-09	7.74E-10	0	
210	2.01E-09	1.90E-09	1.57E-09	0	
250	2.42E-09	2.36E-09	2.17E-09	0	
300	2.70E-09	2.67E-09	2.59E-09	0	
400	1.35E-09	1.33E-09	1.29E-09	0	
4. $O - e \rightarrow O^+(^4S) + 2e$					
z(km)	Solar Zenith Angle				
	49.78°	61.50°	76.22°	97.16°	
95	0	0	0	0	
100	5.90E-12	1.29E-12	5.53E-15	0	
130	2.08E-09	1.29E-09	5.73E-10	0	
170	2.37E-09	1.79E-09	7.26E-09	0	
210	4.26E-08	3.85E-08	2.70E-08	0	
250	5.09E-08	4.88E-08	4.22E-08	0	
300	5.22E-08	5.08E-08	4.82E-08	0	
400	2.61E-08	2.54E-08	2.41E-08	0	
5. $O + e \rightarrow O^+(^2D) + 2e$					
z(km)	Solar Zenith Angle				
	49.78°	61.50°	76.22°	97.16°	
95	0	0	0	0	
100	4.23E-12	9.30E-13	3.98E-15	0	
130	1.28E-09	8.51E-10	3.40E-10	0	
170	1.07E-08	8.35E-09	3.80E-09	0	
210	1.84E-08	1.68E-08	1.22E-08	0	
250	2.22E-08	2.13E-08	1.86E-08	0	
300	2.36E-08	2.31E-08	2.20E-08	0	
400	1.18E-08	1.15E-08	1.10E-08	0	

Table B23. Rate Coefficients for Energetic Electron Impact Reactions (Contd)

6. $N_2 + e \rightarrow N_2^+ + 2e$				
z(km)	Solar Zenith Angle			
	49.78°	61.50°	76.22°	97.16°
95	0	0	0	0
100	6.12E-12	1.34E-12	5.80E-15	0
130	1.55E-09	1.11E-09	5.52E-10	0
170	9.31E-09	7.51E-09	3.86E-09	0
210	1.54E-08	1.42E-08	1.07E-08	0
250	1.87E-08	1.80E-08	1.60E-08	0
300	2.02E-08	1.98E-08	1.90E-08	0
400	1.01E-08	9.91E-09	9.49E-09	0
7. $O_2 + e \rightarrow O_2^+ + 2e$				
z(km)	Solar Zenith Angle			
	49.78°	61.50°	76.22°	97.16°
95	0	0	0	0
100	1.81E-12	3.97E-13	1.70E-15	0
130	6.32E-10	3.94E-10	1.76E-10	0
170	7.14E-09	5.40E-09	2.19E-09	0
210	1.29E-08	1.17E-08	8.18E-09	0
250	1.55E-08	1.48E-08	1.28E-08	0
300	1.60E-08	1.53E-08	1.45E-08	0
400	7.90E-09	7.67E-09	7.27E-09	0
8. $N_2 + e \rightarrow N + N(^2D) + e$				
z(km)	Solar Zenith Angle			
	49.78°	61.50°	76.22°	97.16°
95	0	0	0	0
100	1.64E-11	3.59E-12	1.54E-14	0
130	6.27E-09	3.71E-09	1.60E-09	0
170	9.42E-08	6.93E-08	2.53E-08	0
210	1.82E-07	1.63E-07	1.11E-07	0
250	2.22E-07	2.12E-07	1.31E-07	0
300	2.11E-07	2.03E-07	1.91E-07	0
400	1.05E-07	1.01E-07	9.55E-08	0



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## Appendix C

### The Computer Code

The computer code used to develop the simulated atmosphere described in this report is presented in detail in this Appendix.

To conserve computer memory, the code was written in OVERLAYs. Once all the initialization is completed at the beginning of a run, there is no need to retain in memory all the code that accomplished this.

The code is written in FORTRAN IV for a CDC 6600 mainframe computer. It also utilizes a large block of extended core storage for saving the concentration arrays, the average velocity arrays, and the reaction rate coefficient arrays at the beginning of each time step. If extended core is not available, these sections of the code have to be rewritten to use whatever disk or, as a last resort, tape storage is available. Using disk or tape storage significantly increases the residence time of the code on the computer.

#### C.1. THE MAIN OVERLAY (0,0)

The main overlay is relatively short. It defines all the blank COMMON variables shared by all the overlays. It also defines the parameters that describe the simulation to be generated as well as the error criteria. It calls OVERLAYs (1,0) and (2,0).

## C1.1 Blank COMMON

There are 692 height steps between the lower and the upper boundaries in this model. The 424 height steps between the lower boundary and 120 km represent the region over which the negative ions and the cluster ions are calculated.

N is one of the dependent variable arrays. It contains the altitude distribution of the concentrations of the 26 species in the transport mode plus the arrays for  $O(^1D)$ ,  $N_2^+$ ,  $O(^2D)$ , and the electrons.

CONC is also a dependent variable array. It contains the height distributions for those species considered over the smaller altitude region.

U is another dependent variable array. Here are stored the values at each altitude of the average velocities of those species in the transport mode.

NZERO and UZERO are working arrays that contain the values of N and U for the particular species whose set of equations is being solved at any given time.

FORM and REMV contain the altitude arrays of the rate of chemical formation [P in Eq. (1)] and chemical removal [L in Eq. (1)] for the species whose equations are being solved.

E and F contain the altitude arrays of E and F in Eq. (28) for the species under consideration.

Z is the altitude array in kilometers.

DEDY is the array containing the fixed vertical turbulent diffusion coefficients.

TEMP is the array containing the fixed temperature profile.

DTEMDZ is the array of the values

$$\frac{1}{T(z)} \frac{dT(z)}{dz} \quad (C1)$$

DELTAZ is the array of height increments in centimeters.

SUNSET is the array containing the sunset solar zenith angle at each altitude.

GRAV is the sea level acceleration of gravity.

COSD = cos (declination)\*cos (latitude).

SIND = sin (declination)\*sin (latitude). Both COSD and SIND are used in computing the solar zenith angle.

TIME is the independent variable. Time is measured in seconds, with time = 0 as noontime of solution day 1.

CXI is the solar zenith angle in radians and is a function of the local time.

RADIUS is the radius of the earth in kilometers.

ISPECI is the total number of species included in the code.

KSPECI is the number of species in the transport mode.

NREAC is the number of temperature independent chemical reactions.

NREAC2 is the number of temperature dependent chemical reactions.

K is the number of height steps over which the equations are to be integrated.

KMIN1 = K - 1.

ITURB is the index of the height of the turbopause in the Z array.

CXINOOON is the noontime solar zenith angle.

SCXI is the local solar zenith angle in degrees.

## C1.2 Labeled COMMON

### C1.2.1. COMMON/ESM/

OLDN, OLDCON, and OLDU are the extended core arrays corresponding to N, CONC, and U respectively.

RATES is the extended core array containing the values of the height dependent reaction rate constants for the 88 temperature dependent reactions. These four variables are also defined in the LEVEL statement in all programs where they apply.

### C1.2.2 COMMON/TIMES/

DAYS is the variable that contains the number of solution days over which the equations will be solved.

DELT always contains the current value of the time step in seconds.

TMAX is the maximum value in seconds that the time step will be allowed to have. This value is 1800 seconds in code presented here.

TSET is the time in seconds after noontime of sunset at the lower boundary.

TRISE is the time in seconds after noontime of sunrise at the upper boundary.

### C1.2.3 COMMON/ALTITUD/

ZBOT is the altitude of the lower boundary in kilometers.

ZTOP is the altitude of the upper boundary in kilometers.

TURB is the altitude of the turbopause in kilometers.

ZTRANS is the altitude of the day-night transition height. During the day, it is set at 100 km, and, during the night, it is set at 400 km.

### C1.2.4 COMMON/RESTART/

ITERAMP is the number given to a particular solution file on the interrupt file (Appendix 4). These files are numbered sequentially from 1.

TOFF is the number of seconds that must be allowed the program to dump onto the interrupt file all the information needed to restart the code at the point when it was interrupted. The final solution of these sets of equations takes many hours of CDC and computer time. Because of this, the code is normally run for a few hours (usually 4), then stopped, and a dump is taken. Later, the code is restarted at this point, continued for another period of time, and another dump is taken.

This routine is repeated until the calculations reach a point where they repeat the solution over each diurnal cycle (usually about 20 days of problem time).

TYME is the time in seconds of the current computer run. The computer stops executing the code and dumps when

TYME - (time running) < TOFF.

TODAY is the date when the run was made and is printed out as XX/XX/XX.

#### C1.2.5 COMMON/OUTPUTS/

TIMOUT is a variable that gives the code the frequency in hours with which to send the solutions to the OUTPUT and the interrupt files. The solutions after every time step are not saved. Only those solutions occurring at TIMOUT hours and at interrupts are sent to OUTPUT and are preserved on Tape 4.

OPRINT is the variable containing the frequency in hours at which solutions are to be written on Tape 4. Except on interrupts, TIMOUT is incremented by OPRINT every time a solution set is written to Tape 4.

PRINT is a logical parameter under program control that determines whether writing to Tape 4 will take place after a solution is accepted (PRINT = .TRUE.) or will not (PRINT = .FALSE.).

#### C1.2.6 COMMON/ERRORS/

ERRMAX is the criterion for acceptance of a solution. When the relative change of all species at all altitudes over successive iterations is less than ERRMAX, the iteration is stopped and the solution for that time step accepted.

ERSPECI is the criterion for stopping the iteration of individual species. Since the solutions converge faster for some species than for others, a good deal of computer time can be saved by no longer iterating the equations for those species whose relative change is less than ERSPECI. Of course, ERSPECI must be much smaller than ERRMAX.

ITMAX is the maximum number of iterations to be allowed for any given solution. If any species have not converged after ITMAX iterations, the iterating is stopped and the last solutions computed are accepted. With ITMAX = 100, this situation has never arisen.

#### C1.2.7 COMMON/CONSTAN/

PI = 3.14159265359.

RADDEG = PI/180 is the conversion factor for degrees to radians.

DEGRAD = 180/PI is the conversion factor for radians to degrees.

RADSEC = PI/43200 is the conversion factor for changing local time in seconds to local hour angle in radians.

BOLTZ =  $1.38047 \times 10^{-16}$  ergs/K is Boltzmann's constant.

SIN2I is the square of the sine of the magnetic dip angle.

ATCON =  $1.660356 \times 10^{-24}$  is the mass of the hydrogen atom in grams.

#### C1.2.8 COMMON/JAYS/

The labeled COMMON/JAYS/ contains the photodissociation rate coefficients for reactions 192 through 205. The locations reserved in this labeled COMMON are initialized from file Tape 3 by PROGRAM INITIAL.

#### C1.2.9 COMMON/COLFRE/

The array D contains the invariant part of the collision frequencies  $\nu_{ij}$ .

$$D[J,I] = \frac{1}{2} (\sigma_I + \sigma_J)^2 \left[ 2\pi k \frac{(m_I + m_J)}{m_I m_J} \right]^{1/2}. \quad (C2)$$

#### C1.2.10 COMMON/ATCONS/

The arrays in the labeled COMMON/ATCONS/ all pertain to the atomic and molecular constants.

ATWT contains the atomic or molecular weights of the 26 species in the transport mode.

MASS=ATWT\*ATCON contains the mass in grams of the 26 species in the transport mode.

THERM contains the thermal diffusion factors for the 26 species in the transport mode. Where values are not known, the thermal diffusion factor is set to unity, which removes any thermal diffusion effect for that species.

SYMBOL contains the alphanumeric identification of each of the 56 species in the model.

POLAR contains the polarizabilities of the species in the transport mode. For species whose polarizabilities are not known, the value is set to zero to remove the polarizability effect.

#### C1.2.11 COMMON/RATECON/

The arrays in labeled COMMON/RATECON/ all pertain to the rate coefficients for the chemical reactions.

The arrays AK, BK, and CK contain the A's, B's, and C's of Eq. (A1) for the altitude dependent reaction rate coefficients.

The array DK contains the rate coefficients for the 215 chemical reactions at mean sea level altitude under consideration.

The array CYMB contains the alphanumeric equivalence of the 215 chemical reactions themselves.

## C1.2.12 COMMON/IONS/

The arrays in labeled COMMON/IONS/ all pertain to the ionization of the atmospheric gases.

WAVE contains the alphanumeric identification of the lines or wavelength bands in the EUV.

FLUX contains the solar flux in photons/cm<sup>2</sup>/sec/Å at the top of the atmosphere at each of the above lines or in each of the wavelength bands.

SIGMA contains the absorption and the ionization cross sections for O<sub>2</sub>, N<sub>2</sub>, and O, in that order.

R contains the rate coefficients for the eight energetic electron reactions at the four zenith angles and eight heights listed in Table B22.

The main overlay sets the values of the control parameters before calling OVERLAY (1,0). Upon return from OVERLAY (1,0), the initialization of the code for the run to be made is completed. The initial values of all of the dependent variables N, CONC, and U are then saved in extended core storage. Finally, OVERLAY (2,0) is called and retains control until the calculations are terminated.

## C2. OVERLAY (1,0) PROGRAM INITIAL

The purpose of OVERLAY (1,0) PROGRAM INITIAL is to initialize the code for the particular run to be made. In the dimension statement —

S contains the collision cross sections in cm<sup>2</sup> of each of the species in the transport mode. This information is required in the computation of the collision frequencies  $\nu_{ij}$ .

RMIX contains the ground level mixing ratios for the transport species.

SIG contains the photoionization cross sections for atomic nitrogen for the lines and bands given in array WAVE. These cross sections scaled by 10<sup>18</sup> are listed in the DATA statement of this overlay.

Following this DATA statement are the FUNCTION definitions. The first is for the sea level value for the acceleration of gravity as a function of the latitude  $\phi$ . It is given by<sup>C1</sup>

$$\text{GRAV}(\phi) = 978.0356 \{ 1 + 0.0052885 \sin^2(\phi) + 5.9 \times 10^{-6} \sin^2(2\phi) \}. \quad (\text{C3})$$

The second is for the radius of the earth as a function of the colatitude and the sea level acceleration of gravity. It is given by<sup>C1</sup>

C1. List, R.J., Ed. (1963) Smithsonian Meteorological Tables, Sixth Revised Edition, Washington, D.C.



altitude whose index is IALT. First, this subroutine computes the total concentration M as

$$Y(57) = \sum_{i=1}^{56} n_i.$$

Then it moves the rate coefficients for the 215 reactions at the altitude under consideration into the K region. Following this, it ensures that the photodetachment and photodissociation of the negative ions are removed if the code is in the nighttime. The remainder of the code computes the P and L for species KIND and stores them in the appropriate FORM and REMV regions, respectively. The bulk of this subroutine as well as SUBROUTINE CHEMPR were not hand-coded for obvious reasons. To avoid the very tedious task of hand-coding these routines every time the chemistry set or the species set is changed, a set of programs was written to perform the task of writing these codes. These programs can be found in Keneshea.<sup>3</sup>

### 3.11 SUBROUTINE RATECN

SUBROUTINE RATECN sets the reaction rate coefficients for all the photo-reactions at the altitude whose index is IALT. The first three DATA statements in this subroutine contain, respectively, the solar fluxes ( $\times 10^{-9}$  photons), the ionization cross sections ( $\times 10^{18} \text{ cm}^2$ ), and the effective absorption cross sections ( $\times 10^{18} \text{ cm}^2$ ) for  $\text{O}_2(^1\Delta_g)$  as given by Huffman.<sup>22</sup> The next two DATA statements contain the altitudes (km) and the solar zenith angles corresponding to the input arrays of the rate coefficients for the energetic electrons. Following this is the DATA statement specifying the rate coefficient for ionization by cosmic rays. The first executable statement of the program is the FUNCTION definition for the correction at altitude ZZ for the sea level acceleration of gravity.

The code first computes all the rate coefficients for the current altitude and stores them in the DK array. On the initial call to this subroutine, the fluxes and the cross sections given in the DATA statements are scaled to their proper orders of magnitude, and the rate coefficients for the energetic electron processes are replaced by their natural logarithms. Next, the noontime values of  $H \times F$  for  $\text{O}_2$ ,  $\text{N}_2$ , and O are computed and saved for later use in computing the scattered radiation. Here, H is the scale height of the species and F is the Chapman approximation used in computing the absorption. If the code is in the nighttime, then transfers are made to statements near the end of the code since all photo processes are ignored during the night. If the code is in the daytime, then the photo rate coefficients are determined for the immediate daytime conditions. If the code is in the

where, as before,  $\ell$  and  $\ell + 1$  represent values at the beginning and at the end of the time step, respectively. The profile of  $O(^1D)$  is computed once from Eq. (C21) each time that this subroutine is called, with  $P_k^\ell$  and  $L_k^\ell$  used instead of  $P_k^{\ell+1}$  and  $L_k^{\ell+1}$ . Also computed in this subroutine are the concentrations of : (1) all the positive ions not in the transport mode; (2) all the negative species; (3) all the positive cluster ions; and (4)  $HNO_2$  and  $NO_3$  between 50 and 120 km.

Eq. (C21) requires the value of the chemistry terms  $P$  and  $L$  at the end of the time step which in turn require the value of  $n$  at the end of the time step. Since this is the quantity being determined, Eq. (C21) will have to be iterated. Upon each iteration, the chemistry terms are computed with the latest values of  $n$ . When the solution has converged, the value of  $n$  at  $\ell + 1$  will have been achieved and the chemistry will have been computed with this value.

At the beginning of each iteration, the value of the concentration at the current altitude is saved temporarily in the array  $H$ . The new value is stored in the appropriate cell of the  $F$  array. To ensure a more rapid convergence of the solution, the value of the concentration after the current iteration is replaced by the average value

$$n = \frac{H + F}{2}$$

Then the relative difference

$$\frac{H - n}{H}$$

is computed for each species. If the relative change for each species over the current iteration is less than 20 percent, the solution is accepted for that height step and the iterations are started at the next higher altitude. If any species has a relative change greater than 20 percent, all the concentrations are iterated again.

This procedure is repeated until all species have relative changes at all altitudes of less than 20 percent. The total number of iterations allowed at each altitude is 100. This number has always been more than sufficient to generate a solution.

When the concentrations of all the required species have been computed between 50 and 120 km, this subroutine then computes the electron concentration between 10 km and the upper boundary from charge balance.

### C3.13 SUBROUTINE CHEM

SUBROUTINE CHEM computes the quantities  $P$  and  $L$  for species  $KIND$  at the

The variable TIMOUT is used to keep account of the next hour in problem time when a solution will be sent to the output file. The code ensures that this time will occur exactly by resetting the time step if the current time exceeds this time. The RESET and PRINT switches are set to .TRUE., and the value of TIMOUT is incremented by OPRINT to update it for the next printout. When this routine is exited, DELT contains the time increment in seconds over which the next solution will be made, TIME contains the total elapsed problem time in seconds, and CHI contains the solar zenith angle in radians at the end of the current time step.

### C3.12 SUBROUTINE CHEMION

SUBROUTINE CHEMION computes the concentrations of all species in the chemistry mode. This subroutine also computes the largest negative species from charge balance. Below 120 km, this could be a negative ion or the electrons. Above 120 km, it is always the electrons.

If the divergence of the flux in Eq. (1) is set to zero, then that equation can be written as

$$\frac{dn_i}{dt} = P_i - n_i L_i . \quad (C19)$$

Two convenient choices exist for solving these ordinary differential equations. They can be solved using the Kutta-Merson numerical integration scheme available in SUBROUTINE ODE, or they can be solved using simple finite differences. Since much more computer time is required to solve the equations by the Kutta-Merson scheme and since it is generally a minor species whose concentration is being computed, the more economical finite differences are used to solve Eq. (C19). Writing Eq. (C19) in finite difference notation at level k gives

$$\frac{n_k^{\ell+1} - n_k}{\Delta t} = P_k^{\ell+1} - n_k^{\ell+1} L_k^{\ell+1} . \quad (C20)$$

The concentration  $n_k^{\ell+1}$  at the end of the time step is then

$$n_k^{\ell+1} = \frac{n_k^{\ell} + \Delta t P_k^{\ell+1}}{1 + \Delta t L_k^{\ell+1}} \quad (C21)$$

### C3.8 SUBROUTINE ODE

SUBROUTINE ODE solves a set of N ordinary differential equations using the Kutta-Merson numerical integration scheme. This program is explained in detail elsewhere.<sup>2</sup> The solution is taken over the altitude range DZ starting at altitude SZ. The solutions are returned in array START.

### C3.9 SUBROUTINE RHS

SUBROUTINE RHS is called by SUBROUTINE ODE to supply to ODE the values of the right hand side of Eq. (42). The values are computed at altitude ZE using the intermediate values v computed in SUBROUTINE ODE. The results of the evaluation are returned in the array SLOPE. The intermediate values at altitude ZE are computed using the linear interpolation coefficients derived in SUBROUTINE VELOCITY.

### C3.10 SUBROUTINE COLFRE

SUBROUTINE COLFRE computes the sum of the collision frequencies (SNU) of species i with all the other species at the altitude whose index is j. It also computes the quantities  $\sum_j \nu_{ij} w_j$  required in Eq. (22) for species i. In addition, it sets the values of omega (OMEG) in Eq. (17). OMEG is computed from Eq. (10) if i represents an ion, and is set equal to unity if i represents a neutral species.

### C3.11 SUBROUTINE TIMER

Except for doubling of the time step after a successful integration and halving of the time step on an error, all changes to the time and the time step are done in SUBROUTINE TIMER. This subroutine decides whether or not the next integration will end at a print step. It also determines if the next time step will be in the daytime, nighttime, or in morning or evening twilight. The code advances normally in time until this subroutine determines that the sun is about to rise at the upper boundary or is about to set at the lower boundary. When either of these situations is about to happen, this subroutine adjusts the time step so that the next integration will end at the beginning of morning or evening twilight. During these twilight periods, the concentrations of some of the atmospheric species change rapidly. These changes force the code to reduce the time step to successively smaller and smaller values before a solution can be accepted. To avoid the large amount of computer time required to accomplish this, the code automatically reduces the time step to 10 seconds with the onset of morning or evening twilight. The LOGICAL switch SFT controls this. The time increment is then allowed to double in PROGRAM INTEG after each successful integration until it reaches TMAX.

$$\frac{n_{j+1}}{n_j} < 100.$$

If the ratio  $n_{j+1}/n_j > 100$ , the velocity is set to zero at that altitude.

### C3.7 SUBROUTINE VELOCITY

SUBROUTINE VELOCITY sets up the parameters required for computing the upper boundary value of the velocity of species  $i$ . In order to use any numerical integration scheme to solve Eq. (42) for the velocity  $w$  at the upper boundary, some means of interpolating values of  $n$ ,  $P$ ,  $L$ , and  $dn/dz$  between the upper boundary and one step below must be provided. What is used here is a simple linear interpolation:

$$\begin{cases} n_K = az_K + b \\ n_{K-1} = az_{K-1} + b \end{cases} \quad (C17)$$

Solving these equations for  $a$  and  $b$  gives

$$a = \frac{n_K - n_{K-1}}{\Delta z_K}.$$

and

$$b = \frac{n_{K-1} z_K - n_K z_{K-1}}{\Delta z_K}. \quad (C18)$$

In the function definitions at the beginning of SUBROUTINE VELOCITY,  $AF$  is the definition of  $a$  and  $BF$  is the definition of  $b$ . The subroutine then proceeds to compute the  $a$  and  $b$  coefficients for the equations  $n(AN, BN)$ ,  $P(AP, BP)$ , and  $L(AL, BL)$ . These are stored in labeled COMMON/RHSIDE/ for use by SUBROUTINE RHS later. This subroutine then calls SUBROUTINE ODE to solve the ordinary differential equations (Eq. (42)) for species  $i$  over the last height step.

the total concentration

$$N = \sum_{i=1}^{26} n_i,$$

the mean molecular weight in grams of the atmosphere

$$\bar{m} = \frac{\rho}{N}, \quad (C15)$$

and the mean mass velocity

$$w_0 = \frac{\sum_{i=1}^{26} \rho_i w_i}{\sum_{i=1}^{26} \rho_i} \quad (C16)$$

The negative ions and the positive cluster ions, which are always very minor species, are excluded from the above sums.

### C3.6 SUBROUTINE EFORU

For the species whose number is ICF, SUBROUTINE EFORU computes its E and F arrays of Eq. (28) if ICF is positive, or its average velocity array from Eq. (18) if ICF is negative.

The computation of the E and F arrays is fairly straightforward. At each altitude, the A(AJ), B(BJ), C(CJ), and D(DJ) values of Eq. (21) are computed. Then the E and F arrays are computed with the upper and lower boundary conditions imposed.

The specific velocities are also calculated in this subroutine since their evaluation requires much of the same coding as do the E and F arrays. Both computations call SUBROUTINE VELOCITY to obtain the upper boundary velocity for those species that are not assumed to be in diffusive equilibrium there. To avoid unrealistically large values of the velocities when the concentration is very small, the concentration of each species  $n_j$  and the ratio of  $n_{j+1}/n_j$  are investigated at each altitude. If  $n_j > 1.0 \times 10^{-10} \text{ cm}^{-3}$ , then its velocity at altitude  $j$  is computed. For values of  $n_j < 1.0 \times 10^{-10}$ , the velocity is computed if the ratio

Performing the integration results in

$$n = n_K \exp \left\{ - \frac{mg_0}{kT_K} \left[ \frac{(z - z_K)}{\left(\frac{z_K}{R} + 1\right) \left(\frac{z}{R} + 1\right)} \right] \right\} \quad (C12)$$

where the subscript K refers to quantities at the upper boundary. After the concentrations have been extrapolated to 500 km, the actual smoothing routine is called, where the profile is smoothed with a 7-point running mean. At this point, the code continues to loop back until all the required smoothing is accomplished. If no ion profile was smoothed, the subroutine is exited here. If at least one of the smoothed profiles was a positive ion profile, then the negative species must be readjusted to ensure charge neutrality in the atmosphere. Below 120 km, the largest negative species is recomputed from charge balance.

$$n_i = \sum_j n_j^+ - \sum_{j \neq i} n_j^- \quad (C13)$$

Above 120 km the electron concentration is recomputed from

$$n_e = \sum_j n_j^+$$

### C.3.4 SUBROUTINE SMOOTH

SUBROUTINE SMOOTH computes the smooth array B corresponding to the unsmoothed array A. Both arrays contain N points. M, which must be odd, is the number of points in the running mean. In this smoothing routine, the beginning and the end points are not changed.

### C.3.5 SUBROUTINE CO

At the altitude corresponding to the index j, SUBROUTINE CO computes the total ion density

$$n^+ = \sum_{i=1}^{20} n_i m_i \quad (C14)$$

assuming the concentration is in diffusive equilibrium above the upper boundary.

That is,

$$\frac{dp}{dz} = - \rho g \quad (C6)$$

or

$$\frac{d(nkT)}{dz} = - nmg \quad (C7)$$

which reduces to

$$\frac{1}{n} \frac{dn}{dz} + \frac{1}{T} \frac{dT}{dz} = - \frac{mg}{kT} \quad (C8)$$

It is also assumed that above 400 km

$$\frac{dT}{dz} = 0.$$

Therefore, Eq. (C8) becomes

$$\frac{1}{n} \frac{dn}{dz} = - \frac{mg}{kT} \quad (C9)$$

An approximation to the acceleration of gravity at any altitude  $Z$  can be written as

$$g = \frac{g_0}{\left(1 + \frac{z}{R}\right)^2} = \frac{g_0 R^2}{(R + z)^2} \quad (C10)$$

where  $g_0$  is the sea level value of the acceleration of gravity and  $R$  is the radius of the earth. Using Eq. (C10) and the assumption that the temperature is constant above the upper boundary, the solution to Eq. (C9) is

$$\ln \left( \frac{n}{n_0} \right) = - \frac{mg_0 R}{kT} \int_{z_0}^z \frac{dz}{(R + z)^2} \quad (C11)$$



have been computed for the species in the transport mode. It then calls SUBROUTINE CHEMION to compute the concentration profiles at the end of the current time step of all the remaining species. After all the new concentrations have been computed, the code then calls SUBROUTINE EFORU to compute the average velocities for those species in the transport mode.

Following this, a check is made to see if the solution for any species has converged at all altitudes. That is, is its largest relative change less than ERSPECI. If so, its IWHICH switch is set to zero and its ITER counter set to the current iteration number. The equations for this species will be skipped on the next iteration of the equation set.

A check is then made to see if the largest relative change among all the species is less than ERRMAX. If so, the iteration loop is exited and the solution accepted for this time step. If not, transfer is made back to the beginning of the DO 130 loop for the next iteration.

When the solution is accepted, the code then asks whether or not this solution should be sent to the output file. If printing has not been requested (PRINT=.FALSE.), transfer is made to that section of the code where the time step is doubled if possible, and the new concentrations and velocities are saved in extended core storage. Transfer is then made to STATEMENT 1000, where a new solution is generated over the next time step. If the solution is to be sent to the output file, the code then calculates all the subsidiary parameters to be printed out along with the concentrations and the average velocities. The code at this point is fairly explicit as to which quantities it is computing and sending to the output file. When all the information has been sent to the output file, the code then writes an interrupt file on Tape 4. This file contains all the information necessary to restart the code at this point at some later time. Since the development of a complete time dependent solution takes many hours of CDC 6600 CP time, it has to be accomplished in many short runs (about 4 hours each). The code is restarted from Tape 4 each time.

### 6.3 SUBROUTINE SMOOTHY

SMOOTHY controls the smoothing of those profiles that PROGRAM INTEG has determined should be smoothed. If no profiles are to be smoothed (NUM=0), then the subroutine is exited immediately upon entry. Because of the nature of the smoothing process, it is necessary to extrapolate the concentration profile above the upper boundary. The altitude above the upper boundary to which the extrapolation is done should be far enough away so that the effects of the smoothing at the top of the array are not felt at the upper boundary. In this code, the profiles are extrapolated to 500 km in 1=km=height steps. The extrapolation is accomplished

solution. This may be a new solution over the next time step or another try using a smaller time step because an error was encountered.

The code then saves the time, the solar zenith angle, the day-night transition height, and the day and night logical switches at the beginning of the time step. If an error is encountered later, these parameters will have to be reinitialized. The code then calls SUBROUTINE TIMER to compute the time and solar zenith angle at the end of the current time step. It then sets the JLOOK switch depending upon whether it is day or night. Following this, the IWHICH switches are all initialized to unity and the ITER locations to 999. Then, since the equations for helium will not be solved in this calculation, its IWHICH switch is set to zero.

The statement DO 130 is the beginning of the iteration loop. The loop beginning with the next statement is taken over all the species in the transport mode. The equations will be solved over the altitude extent for each species in succession. On the first pass through the loop, the quantities

$$\frac{1}{n_e} \frac{\partial n_e}{\partial Z} \approx \frac{1}{n_e} \frac{\Delta n_e}{\Delta Z} = \frac{n_{ej} - n_{ej-1}}{n_{ej} \Delta Z_j - 1} \quad (C5)$$

are computed and saved in the working array H. Next, the altitude dependent rate coefficients are computed using the current atmosphere and the values saved in extended core storage. If the JLOOK switch is on .TRUE., then the photodissociation rate coefficients are sent to the output file. If any of the concentration profiles need smoothing, this is done next and an acknowledgement is sent to the output file. To remain internally consistent, it is necessary now to recompute the velocity profiles for those species whose concentration profiles have been modified by smoothing. All the concentrations and velocities are then saved in extended core storage.

The code then brings into memory the values of the concentrations and velocities for the current species at the beginning of the time step. It then proceeds to compute a new concentration profile in the DO 100 loop. It also saves the largest relative change for this species in the BIGEST region. The relative change is defined as

$$\frac{n_j^{k+1} - n_j^k}{n_j^{k+1}}$$

The code then loops back to solve the continuity equation for the next species in turn. When the code exits at 105 CONTINUE, all the new concentration profiles

NSPEC is an array containing the order number from 1 to 56 of each species whose concentration is to be smoothed before the iteration procedure is started. The variable NUM indicates how many profiles are to be smoothed. If NUM=0, no smoothing will be done.

Two new labeled COMMONs are defined in PROGRAM INTEG.

### C3.1 Labeled COMMON/LOGIC/

All the parameters listed in Labeled COMMON/LOGIC/ are logical variables. NIGHT is .TRUE. whenever the entire altitude region between the upper and lower boundaries is in darkness. Otherwise, it is .FALSE..

DAY is .TRUE. whenever the entire altitude region between the upper and lower boundaries is in daylight. Otherwise, it is .FALSE..

Both NIGHT and DAY variables are .FALSE. when the sun is rising or setting and only part of the altitude region between the upper and lower boundaries is in darkness.

JLOOK is set to .TRUE. to send to the output file, before the iteration begins, a table of the altitude distribution of the  $O_2$  concentrations, the  $O_2$  column densities, the  $O_3$  concentrations, the  $O_3$  column densities, and the rate coefficients for all the photodissociation reactions. If JLOOK is .FALSE., this table is not printed.

RESET is set to .TRUE. in SUBROUTINE TIMER whenever the time step has been recomputed because the next solution will be sent to the output file and the interrupt file.

END is set to .TRUE. whenever the computations for the current run are to be terminated.

### C3.2 Labeled COMMON/COLUM/

The Labeled COMMON/COLUM/ contains information pertaining to the photodissociation rate coefficients.

O2COL is used to transfer the  $O_2$  column density from SUBROUTINE DISSOC to SUBROUTINE RATECN.

O3COL is used to transfer the  $O_3$  column density from SUBROUTINE DISSOC to SUBROUTINE RATECN.

DIS is the array where the photodissociation information is stored in SUBROUTINE RATECN for printing in PROGRAM INTEG. To avoid excessively long printouts, only every twelfth altitude value between the lower and the upper boundaries is stored in these arrays.

PROGRAM INTEG starts by initializing some of its variables. STATEMENT 1000 CONTINUE marks the beginning of the working code. After every successful or unsuccessful solution, the code will loop back to this statement to begin the next

and (9). This overlay uses two DIMENSION statements that contain the following variables:

PHI is an array EQUIVALENCED to the array U(1, 21) and is used as temporary storage of the total flux  $\phi$  of each species during the printout phase of the code. The array U(1, 21) would normally contain the velocity profile of helium, but, since this species is held invariant in these calculations, these memory locations are available for other uses.

DED is an array EQUIVALENCED to the array E in COMMON. It is used as temporary storage of the turbulent diffusion velocity of each species successively during the printout phase of the code.

DEDZ is an array EQUIVALENCED to the array NZERO and is used as temporary storage of the vertical gradient of the turbulent velocity for each species during the printout phase of the code.

VBAR is an array EQUIVALENCED to the array F and is used as temporary storage of the molecular diffusion velocity of each species during the printout phase of the code. The molecular diffusion velocity of a species is equal to its average velocity minus the mean mass velocity.

H is an array used in various places in the code for temporary storage of arrays.

OUTP contains four words each of which contains one hollerith character of the local time in hours. It is computed by SUBROUTINE HOUR.

IWHICH is an array of integer switches, one for each species in the transport mode. If a switch is set to 1, the equations for that species will be iterated. If the switch is set to 0, the equations for that species will not be iterated. If IWHICH (21) is set to 0 before entering the iteration loop, the concentration of helium will remain fixed at its initial value throughout the calculations since its equations will not be iterated.

ITER is an array that stores the number of iterations required by each of the sets of equations before a final solution was obtained for a given time step.

BIGEST is an array that contains the largest relative difference in each species concentration profile. It contains the maximum value of

$$\frac{n_j^{k+1} - n_j^k}{n_j^{k+1}}$$

in the array as  $j$  varies from the lower boundary to the upper boundary. This array is recomputed after each iteration.

given time. The first file, which is slightly different from all the others, must be prepared before this code is first run. It contains the initial conditions on all the dependent variables. (See the discussion on the initial conditions in Section 7.1.) Since this is an unformatted file, it must be written exactly as it is read here. First, it reads the date that the first file was written, the file number (1 in this case), and the height in kilometers of the turbopause. It then skips over six words in the file that are not necessary to the current calculations. Then it reads the number of altitude steps in the complete arrays ( $K = 692$ ), the number of altitude steps in the reduced arrays ( $K2 = 424$ ), and the altitude array in kilometers. After this, it reads the height step array, the fixed temperature array, the array  $1/T \, dT/dZ$ , and the fixed turbulent diffusion coefficient array. Next, it reads the initial velocities and initial concentrations.

In the following loop, the remainder of the interrupt files are skipped over and the tape is positioned at the beginning of a new file. At the completion of this loop, the locations containing the dependent variables will have been updated with the values obtained after the last successful solution. These values are then used as initial conditions for the next time step.

All files after file 1 on the interrupt tape are written in OVERLAY (2,0). Care must be taken not to write so many files on Tape 4 that it becomes full. Before this happens, a new Tape 4 must be made containing file 1 and the last file from the old Tape 4.

After the dependent variables have been initialized, the code initializes the solar zenith angle to the current time and computes the noontime solar zenith angle. It then reads from input Tape 5 and, where required, converts to proper units the wavelengths, solar fluxes, and absorption and ionization cross sections to be used in the photoionization calculations. Finally, from this same file, it reads the rate coefficient arrays for the energetic electron reactions. All that remains now is the calculation of the sunset (sunrise) solar zenith angles as a function of altitude. Also calculated are the times of sunset at the lower boundary and of sunrise at the upper boundary.

When all this initialization is complete, the concentration profiles corresponding to the initialized time are written to the output file. Finally, the current value of the variable TIMEOUT is written to the output file in case the frequency of the output of solutions is to be changed for the next run.

### C3. OVERLAY (2,0) PROGRAM INTEG

OVERLAY (2,0) contains all the programs that actually solve Fqs. (1), (7),

RADUS (GRAV,  $\phi$ )

$$= \frac{2 \cdot \text{GRAV}}{2.27 \times 10^{-9} \cos(2\phi) - 2 \times 10^{-2} \cos(4\phi) + 3.085426 \times 10^{-6}} \quad (\text{C4})$$

Next, the constants in labeled COMMON/CONSTAN/ are defined. After this, the constants for the particular solution to be generated are defined.

CLAT is the latitude in degrees.

DECL is the solar declination for the time of year when the calculations are to be made.

DIP is the magnetic dip angle appropriate to CLAT.

Next, the acceleration of gravity, the radius of the earth, and the constants required for later computing the solar zenith angles are computed. Information pertaining to the current calculations is then written to the output file (Tape 6).

The next section of this OVERLAY sets the chemical symbols along with the atomic or molecular weight, the mixing ratio, the collision cross section, the polarizability, and the thermal diffusion factor for the 26 transport species. Following this, the symbols for the species computed from chemistry only are written. The atomic or molecular weight of each species is then converted to mass in grams. The ground level mixing ratio of  $\text{N}_2$  is computed to ensure that the sum of all the mixing ratios is identically unity. The mixing ratios of the species are not necessary for the code described here. However, if other initial conditions are to be computed as discussed in Keneshea et al,<sup>8</sup> then the values of the mixing ratios are required.

The following section of INITIAL obtains input information from various sources. The list of chemical reactions with their rate coefficients must be prepared separately and saved for use here as the file called Tape 5. This information is coded according to the FORMAT defined in statements 770 or 771, depending upon whether the reaction is not height dependent (770) or is height dependent (771). As the reactions are read in, they are also sent to the OUTPUT file (Tape 6). After the reaction set is read in, the code reads in the photodissociation rate coefficient tables (Tables B4 through B20). All values in these tables are in log base 10. These tables also are computed and saved separately. Since these numbers are functions only of the  $\text{O}_2$  and  $\text{O}_3$  column densities, they are universal. They need be computed only once and can then be input to any calculation regardless of geographic location, season of the year, or time of day.

After the photodissociation rate coefficients are initialized, the invariant part of the collision frequencies  $\nu_{ij}$  are computed and saved in the D array.

The next section of the code reads the interrupt file Tape 4. This tape is structured in files, each containing the solution for all the dependent variables at a

morning or evening twilight periods and the current altitude is below the day-night transition altitude, then the computation of the rate coefficients is skipped. Otherwise, they are computed.

During the daytime, SUBROUTINE DISSOC is called for the computation of the photodissociation rate coefficients. These are then stored in the proper cells of the DK array. If the JLOOK switch is on .TRUE., these rate coefficients along with the concentrations and column densities of  $O_2$  and  $O_3$  are stored in the DIS region for later printing in the output file. Following this, the rate coefficients for the energetic electron reactions are computed. The values in the tables are interpolated to the current solar zenith angle and altitude. Next, the column densities of  $O_2$ ,  $N_2$ , and  $O$  at the current solar zenith angle are approximated. These column densities are then used to compute the EUV attenuated flux at each wavelength. The rate coefficients for the photoionization processes are then computed. All EUV radiation below 0.15 nm is considered to be X radiation, which is handled differently from the longer EUV radiation. The total x-ray ionization is computed and partitioned among the species according to Swider.<sup>19</sup> Finally, the total EUV rate coefficients are computed as well as the rate coefficients for the ionization of nitric oxide by Lyman alpha and the ionization of  $O_2(^1\Delta g)$ .

If the code is in the nighttime, the above computations are skipped and the code continues from this point. The contributions of the scattered radiations to the ionization rates are computed next. Finally, the contribution of cosmic rays is added into the rate coefficients and the subroutine is exited.

### C3.15 FUNCTION YINT

FUNCTION YINT performs interpolation where it is required. This function essentially computes a cubic spline fit to the parameter under consideration. It then returns the interpolated value in YINT corresponding to XII in the (X, Y) arrays.

### C3.16 SUBROUTINE CHAPMAN

SUBROUTINE CHAPMAN computes an approximation to the Chapman function, which is required in computing the attenuation of solar energy in its transmission through the atmosphere. The approximations computed are those given by Swider and Gardner.<sup>C2</sup>

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C2. Swider, W. Jr., and Gardner, M.E. (1967) On the Accuracy of Certain Approximations for the Chapman Function, AFCRL-67-0468, AD 658826.

### C3.17 SUBROUTINE DISSOC

SUBROUTINE DISSOC returns the value of the photodissociation rate coefficients appropriate to the current solar zenith angle and the altitude whose index is IALT. The rate coefficients for all species except nitric oxide are determined as follows: The column densities of  $O_2$  and  $O_3$  are first approximated for the current  $O_2$  and  $O_3$  concentration distributions in the code. A linear interpolation is then made in the appropriate photodissociation table to determine the current photodissociation rate coefficient for each of the photodissociation processes. Finally, using the data of Cieslik and Nicolet<sup>C3</sup> as given in the DATA statement of this subroutine, the photodissociation rate coefficient for nitric oxide is computed.

### C3.18 FUNCTION TRPLT2

FUNCTION TRPLT2 interpolates in the two-dimensional photodissociation rate coefficient tables. The two-dimensional array to be interpolated is fed to this function through the parameter ARRAY. The dimensions of ARRAY are (N, M). The indices of elements in ARRAY are IO2 and IO3. The increments required to perform the interpolation are DELO2 and DELO3.

### C3.19 FUNCTION TRPLT1

FUNCTION TRPLT1 interpolates in the one-dimensional photodissociation rate coefficient tables. The array to be interpolated is fed to the function through the parameter ARRAY. The index in ARRAY is IO3 and the interpolation increment is DELO3.

### C3.20 SUBROUTINE INDEX

SUBROUTINE INDEX computes an index I and an increment DEL corresponding to the column density COL. LIM is the lowest power of 10 of the column densities of  $O_2$  and  $O_3$  in the photodissociation tables under consideration.

### C3.21 SUBROUTINE CHEMPR

Each time SUBROUTINE CHEMPR is called, it sends to the output file the complete list of chemical reactions for the altitude whose index is IZ. It also sends the rate coefficient for each reaction and its forward rate. This subroutine is also written by the WRITER codes given in Keneshea.<sup>3</sup> The output from this subroutine is used to determine the relative importance of the chemical reactions in different altitude regions.

C3. Cieslik, S., and Nicolet, M. (1973) The aeronomic dissociation of nitric oxide, Planet. Space Sci. 21:925-938.



### C3.22 SUBROUTINE HOUR

SUBROUTINE HOUR converts the value of TIME, which is in accumulated seconds from the noontime of the day on which the simulation was started, to the local time in hours (0000 to 2359). The digits of the hour are returned in hollerith in successive words of the OUTP array.

[illegible]



```

1  OVERLAP(1.0)
2  PROGRAM INITIAL
3
4  DIMENSION S(25),RMIX(26),SIG(88)
5
6  COMMON N(692,30),CONC(424,26),U(692,26),NZERO(692),UZERO(692)
7
8  COMMON FORM(692),REMV(692),E(692),F(692),Z(692),
9  DEDY(692),TEMP(692),DIEMDZ(692),DELTAZ(692),SUNSET(692)
10
11 COMMON GRAV,COSD,SIND,TIME,CX1,RADIUS,ISPECI,KSPECI,NREAC,K,
12 K2,KMIN1,ITURB,CXINCOON,SCXI,NREAC2
13
14 COMMON/ATCONS/ATWT(26),MASS(26),THERM(26),SYMBOL(56),POLAR(26)
15
16 COMMON/TIMES/DAYS,DELT,TMAX,TSET,TRISE
17
18 COMMON/ALTITUD/ZBOT,ZTOP,TURB,ZTRANS
19
20 COMMON/RESTART/IFRAME,TOFF,TYME,TODAY
21
22 COMMON/OUTPUTS/TIMOUT,OPRINT,PRINT
23
24 COMMON/CONSTAN/PI,RADDEG,DEGRAD,RADSEC,BOLTZ,SIN21,ATCON
25
26 COMMON/JAYS/J192(26,25),J193(28,26),J194(22),J195(32,28),
27 J196(31,30),J197(27,28),J198(26,28),J200(19,15),
28 J201(26,27),J202(22),J203(30,29),J204(35,28),J205(22)
29
30 COMMON/IONS/WAVE(88),FLUX(88),SIGMA(9,88),R(8,4,8)
31
32 COMMON/RATECON/AK(88),BK(88),CK(88),DK(215),CYMB(6,215)
33
34 COMMON/COLFRE/D(26,26)
35
36 REAL N,MASS,J192,J193,J194,J195,J196,J197,J198,J200,J201,J202
37 REAL J203,J204,J205
38
39 THE FOLLOWING DATA STATEMENT CONTAINS THE PHOTOIONIZATION
40 CROSS SECTIONS FOR ATOMIC NITROGEN SCALED BY 1E18.
41 SEE "AERONOMY" BY BANKS AND KOCHARTS, PART A, P102-104.
42
43 DATA SIG/21*(0.),20*(10.0),2*(10.5),2*(10.4),10.75,4*(11.0),
44 11.8,11.9,2*(12.0),11.9,11.5,11.1,11.0,9.3,10.0,9.7,
45 8.5,8.8,2*(8.0),7.3,6.7,6.0,5.3,6.3,4.3,4.2,8.2,2,1.3,
46 0.58,0.45,0.36,0.32,0.23,0.16,0.093,0.04,0.03,0.015,
47 0.006,0.001,0.0001/
48
49 FUNCTION DEFINITION FOR SEA LEVEL ACCELERATION OF GRAVITY AS
50 A FUNCTION OF LATITUDE IN CM/SEC**2.
51
52 GRAVITY(ALAT)=978.0356*(1.0+0.0052885*(SIN(ALAT))**2
53 -5.9E-06*(SIN(2.0*ALAT))**2)
54
55 FUNCTION DEFINITION FOR RADIUS OF THE EARTH IN KILOMETERS AS
56 A FUNCTION OF LATITUDE AND SEA LEVEL GRAVITY.
57
58

```

```

60      1    RADIUS(GRAV,ALAT)=(12.0*GRAV+1.0E-5)/(2.27E-09*COS(2.0*ALAT)
C          -2.0E-12*COS(4.0*ALAT)+3.085462E-06)
C          1
C        CONSTANTS
C
C          P1=3.14159265359
RADDEG=PI/180.
65      DEGRAD=180./PI
RADSEC=PI/43200.
BOLTZ=1.38047E-16
C
C        SET CONSTANTS FOR PARTICULAR MODEL CALCULATION.
C
C          CLAT=30.0
DECL=-19.55
DIP=60.0
PHILAT=CLAT+RADDEG
GRAV=GRAVITY(PHILAT)
RADIUS=RADIUS(GRAV,PHILAT)
DECLAT=DECL+RADDEG
COSD=COS(DECLAT)*COS(PHILAT)
SIND=SIN(DECLAT)*SIN(PHILAT)
SINZI=(SIN(DIP+RADDEG))*2
WRITE(6,25) CLAT,DECL,DIP,GRAV,RADIUS
25      FORMAT(1H,5X,"LATITUDE OF MODEL =",OPF6.2," DEGREES."/
16X,"SOLAR DECLINATION =",F6.2," DEGREES."/6X,"MAGNETIC DIP ",
2"ANGLE =",F6.2," DEGREES."/6X,"ACCELERATION OF GRAVITY =",1PE12.5,
3" CM/SEC**2."/6X,"RADIUS OF THE EARTH =",E12.5," KM.")
C
C        SET ATOMIC AND MOLECULAR WEIGHTS, MIXING RATIOS, COLLISION CROSS
C        SECTIONS. THERMAL DIFFUSION FACTORS AND POLARIZABILITIES.
C
C          ATCON=1.66035E-24
DO 60 I=1,KSPECI
THERM(I)=1.0
POLAR(I)=0.0
RMIX(I)=0.0
60      CONTINUE
SYMBOL(1)=10H H+
ATWT(1)=1.00797
S(1)=3.04E-08
SYMBOL(2)=10H HE+
ATWT(2)=4.0026
S(2)=2.04E-08
SYMBOL(3)=10H O+
ATWT(3)=15.9994
S(3)=1.2E-08
SYMBOL(4)=10H C2+
ATWT(4)=31.9988
S(4)=3.3E-08
SYMBOL(5)=10H NO+
ATWT(5)=30.006132
S(5)=3.4E-08
SYMBOL(6)=10H N+
ATWT(6)=14.006732
S(6)=1.42E-08
SYMBOL(7)=10H O

```

120 THERM(1)=1.0E-08  
 POLAR(1)=1.0E-08  
 ATWT(1)=1.0E-08  
 RMIX(1)=1.0E-08  
 S(1)=2.65E-08  
 SYMBOL(8)=10H O2  
 THERM(8)=1.0E-08  
 POLAR(8)=1.0E-08  
 ATWT(8)=1.0E-08  
 RMIX(8)=1.0E-08  
 S(8)=3.40E-08  
 SYMBOL(9)=10H O3  
 ATWT(9)=47.9982  
 RMIX(9)=7.0E-06  
 S(9)=4.0E-08  
 SYMBOL(10)=10H OH  
 ATWT(10)=17.00737  
 RMIX(10)=1.0E-10  
 S(10)=3.0E-08  
 SYMBOL(11)=10H H  
 THERM(11)=1.0E-08  
 POLAR(11)=0.667  
 ATWT(11)=1.00797  
 RMIX(11)=1.6E-13  
 S(11)=3.04E-08  
 SYMBOL(12)=10H HD2  
 ATWT(12)=33.00677  
 RMIX(12)=1.0E-12  
 S(12)=4.0E-08  
 SYMBOL(13)=10H H2O  
 ATWT(13)=18.01534  
 RMIX(13)=5.0E-06  
 S(13)=3.5E-08  
 SYMBOL(14)=10H H2O2  
 ATWT(14)=34.01474  
 RMIX(14)=1.0E-10  
 S(14)=4.0E-08  
 SYMBOL(15)=10H H2  
 THERM(15)=1.0E-08  
 POLAR(15)=0.82  
 ATWT(15)=2.01594  
 RMIX(15)=4.5E-07  
 S(15)=2.97E-08  
 SYMBOL(16)=10H N  
 POLAR(16)=1.1  
 ATWT(16)=14.006732  
 RMIX(16)=1.0E-11  
 S(16)=1.42E-08  
 SYMBOL(17)=10H N2O  
 POLAR(17)=1.1  
 ATWT(17)=44.006732  
 RMIX(17)=1.0E-16  
 S(17)=1.42E-08  
 SYMBOL(18)=10H NO  
 POLAR(18)=1.74  
 ATWT(18)=30.006732  
 RMIX(18)=1.0E-11

116 IONEUT  
 117 IONEUT  
 118 IONEUT  
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 166 IONEUT  
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 168 IONEUT  
 169 IONEUT  
 170 IONEUT  
 171 IONEUT  
 172 IONEUT

S(18)=3.4E-08  
 SYMBOL(19)=10H NO2  
 ATWT(19)=46.005532  
 RMIX(19)=1.0E-11  
 S(19)=3.8E-08  
 SYMBOL(20)=10H O2+D  
 POLAR(20)=1.59  
 ATWT(20)=31.9963  
 RMIX(20)=2.0E-06  
 S(20)=3.3E-08  
 SYMBOL(21)=10H HELIUM  
 THERM(21)=1.0-0.36  
 POLAR(21)=0.21  
 ATWT(21)=4.0026  
 RMIX(21)=5.24E-06  
 S(21)=2.04E-08  
 SYMBOL(22)=10H ARGON  
 ATWT(22)=39.948  
 RMIX(22)=0.00934  
 S(22)=2.97E-08  
 SYMBOL(23)=10H N2  
 POLAR(23)=1.76  
 ATWT(23)=28.013464  
 RMIX(23)=0.78  
 S(23)=3.15E-08  
 SYMBOL(24)=10H N2O  
 POLAR(24)=3.00  
 ATWT(24)=44.012864  
 RMIX(24)=2.7E-07  
 S(24)=3.7E-08  
 SYMBOL(25)=10H CO2  
 POLAR(25)=2.63  
 ATWT(25)=44.00995  
 RMIX(25)=3.14E-04  
 S(25)=3.8E-08  
 SYMBOL(26)=10H CO  
 POLAR(26)=1.97  
 ATWT(26)=28.01055  
 RMIX(26)=1.0E-08  
 S(26)=3.0E-08

C THE FOLLOWING SPECIES ARE COMPUTED FROM CHEMISTRY ONLY.  
 C

SYMBOL(27)=10H O10  
 SYMBOL(28)=10H N2+  
 SYMBOL(29)=10H O+(2D)  
 SYMBOL(30)=10H E  
 SYMBOL(31)=10H O-  
 SYMBOL(32)=10H O2-  
 SYMBOL(33)=10H O3-  
 SYMBOL(34)=10H O4-  
 SYMBOL(35)=10H NO2-  
 SYMBOL(36)=10H NO3-  
 SYMBOL(37)=10H CO3-  
 SYMBOL(38)=10H CO4-  
 SYMBOL(39)=10H O4+  
 SYMBOL(40)=10H NO2+

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230 SYMBOL(42)=10H H3O+
231 SYMBOL(43)=10H H5O2+
232 SYMBOL(44)=10H H7O3+
233 SYMBOL(45)=10H H9O4+
234 SYMBOL(46)=10H H11O5+
235 SYMBOL(47)=10H H3O+.N2
236 SYMBOL(48)=10H H3O+.OH
237 SYMBOL(49)=10H H5O2+.CO2
238 SYMBOL(50)=10H O2+.H2O
239 SYMBOL(51)=10H NO+.H2O
240 SYMBOL(52)=10H NO+.2H2O
241 SYMBOL(53)=10H NO+.3H2O
242 SYMBOL(54)=10H NO+.CO2
243 SYMBOL(55)=10H HNO2
244 SYMBOL(56)=10H NO3
245 SUMMIX=0.
246 DO 2 I=1,KSPECI
247 MASS(I)=ATWT(I)*ATCOM
248 IF(I.EQ.23) GO TO 2
249 SUMMIX=SUMMIX+RMIX(I)
250 CONTINUE
251 RMIX(23)=1.0-SUMMIX
252
253 C
254 C READ CHEMICAL REACTIONS AND RATE CONSTANTS.
255 C
256 WRITE(6,650)
257 FORMAT(1H0,* THE CHEMICAL REACTIONS USED IN THIS RUN ARE:*)
258 DO 765 J=1,NREAC
259 READ(5,770) IREAC,(CYMB(I,J),I=1,6),DK(J)
260 FOPMAT(13,5A10,A5,1PE8.2)
261 WRITE(6,771) IREAC,(CYMB(I,J),I=1,6),DK(J)
262 FORMAT(2X,13,5A10,A5,1PE9.2)
263 765 CONTINUE
264 DO 35 J=1,NREAC2
265 READ(5,772) IREAC,(CYMB(I,NREAC+J),I=1,6),AK(J),BK(J),CK(J)
266 FORMAT(13,5A10,A5,1PE8.2,0PF5.2,1PE9.2)
267 WRITE(6,773) IREAC,(CYMB(I,NREAC+J),I=1,6),AK(J),BK(J),CK(J)
268 FORMAT(2X,13,5A10,A5,1PE9.2,0PF6.2,1PE10.2)
269 35 CONTINUE
270 C
271 C READ PHOTODISSOCIATION RATE COEFFICIENTS AS LOG BASE 10.
272 C
273 REMIND 3
274 READ(3) ((J193(L,M),L=1,28),M=1,26)
275 READ(3) ((J192(L,M),L=1,26),M=1,25)
276 READ(3) ((J196(L,M),L=1,31),M=1,30)
277 READ(3) ((J197(L,M),L=1,27),M=1,28)
278 READ(3) ((J195(L,M),L=1,32),M=1,28)
279 READ(3) ((J194(L),L=1,22)
280 READ(3) ((J200(L,M),L=1,19),M=1,15)
281 READ(3) ((J205(L),L=1,22)
282 READ(3) ((J201(L,M),L=1,26),M=1,27)
283 READ(3) ((N(L,M),L=1,26),M=1,25)
284 READ(3) ((J202(L),L=1,22)
285 READ(3) ((N(L,M),L=1,26),M=1,23)
286 READ(3) ((N(J,M),L=1,30),M=1,30)

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290	C	READ(3) ((J203(L,M),L=1,30),M=1,29)	110NEUT	287
	C	READ(3) ((J204(L,M),L=1,35),M=1,28)	110NEUT	288
		READ(3) ((N(L,M),L=1,37),M=1,20)	110NEUT	289
		READ(3) ((J198(L,M),L=1,26),M=1,28)	110NEUT	290
			110NEUT	291
			110NEUT	292
			110NEUT	293
			110NEUT	294
			110NEUT	295
295		D(J,1)=0.5*((S(1)+S(J))*2)*SQRT(2.0*PI*BOLTZ*((MASS(1)+MASS(J))	110NEUT	296
	22	1 / (MASS(1)+MASS(J)))	110NEUT	297
		CONTINUE	110NEUT	298
		IFRAME=IFRAME-1	110NEUT	299
		REWIND 4	110NEUT	300
300		READ(4) (DATEOF,IFRAME,TURB,(N(J,1),J=1,6),K,K2,(Z(J),J=1,K)	110NEUT	301
		READ(4) (DELTAZ(L),L=1,K)	110NEUT	302
		READ(4) (TEMP(L),L=1,K)	110NEUT	303
		READ(4) (OTEMDZ(L),L=1,K)	110NEUT	304
305		READ(4) (DEDY(L),L=1,K)	110NEUT	305
		DO 1 J=1,K	110NEUT	306
		DEDY(J)=3.0*DEDY(J)	110NEUT	307
	1	CONTINUE	110NEUT	308
		DO 5 L=1,KSPECI	110NEUT	309
310	5	READ(4) (U(J,L),J=1,K)	110NEUT	310
		CONTINUE	110NEUT	311
		DO 20 L=1,ISPECI	110NEUT	312
		IF(L.GT. 30) GO TO 10	110NEUT	313
		READ(4) (N(J,L),J=1,K)	110NEUT	314
		GO TO 20	110NEUT	315
315	10	READ(4) (CONC(J,L-30),J=1,K2)	110NEUT	316
	20	CONTINUE	110NEUT	317
		KMIN1=K-1	110NEUT	318
	13	READ(4)	110NEUT	319
		IF(EOF(4)) 14,13	110NEUT	320
320	14	IF(IFRAME.EQ. 0) GO TO 15	110NEUT	321
		DO 140 I=1,IFRAME	110NEUT	322
		READ(4) (DATEOF,IFRAME,TIME,SCX1,CX1,DELT,TIMOUT	110NEUT	323
		DO 18 L=1,KSPECI	110NEUT	324
325	18	READ(4) (U(J,L),J=1,K)	110NEUT	325
		CONTINUE	110NEUT	326
		DO 19 L=1,ISPECI	110NEUT	327
		IF(L.GT. 30) GO TO 11	110NEUT	328
		READ(4) (N(J,L),J=1,K)	110NEUT	329
		GO TO 19	110NEUT	330
330	11	READ(4) (CONC(J,L-30),J=1,K2)	110NEUT	331
	19	CONTINUE	110NEUT	332
	16	READ(4)	110NEUT	333
		IF(EOF(4)) 140,16	110NEUT	334
	140	CONTINUE	110NEUT	335
335	15	CX1=ACOS(COSD-COS(RADSEC*TIME)+SIND)	110NEUT	336
		CX1NOON=ACOS(COSD+SIND)	110NEUT	337
		SCX1=CX1*DEGRAD	110NEUT	338
		DO 4 J=1,K	110NEUT	339
		IF(Z(J).GT. TURB) GO TO 6	110NEUT	340
340	4	CONTINUE	110NEUT	341
	6	ITURB=J-1	110NEUT	342
	C		110NEUT	343

```

345 C READ WAVELENGTH, FLUX AND CROSS SECTION DATA FOR PHOTOIONIZATION.
346 C
347 READ(5,200) WAVELENGTH, FLUX(L), SIGMA(L), I=1,80, L=1,88)
348 FORMAT(BB,3F4.4)
349 READ(5,205) FLUX(U), J=84,88)
350 FORMAT(5E12)
351 DO 220 L=1,88
352 IF(L .GE. 84) GO TO 210
353 FLUX(L)=FLUX(L)*1.0E+09
354 DO 215 I=1,8
355 SIGMA(I,L)=SIGMA(I,L)*1.0E-18
356 CONTINUE
357 SIGMA(9,L)=SIG(L)*1.0E-18
358 CONTINUE
359 C READ RATE COEFFICIENTS FOR ENERGETIC ELECTRON REACTIONS.
360 C
361 READ(5,225) I((R(J,I,L),J=1,8),I=1,4),L=1,8)
362 FORMAT(1P4E12.5)
363 C
364 C COMPUTE SUNSET CHI ANGLES AS A FUNCTION OF ALTITUDE AND TIME
365 C OF SUNSET(TSET) AT THE LOWER BOUNDARY AND TIME OF SUNRISE AT THE
366 C UPPER BOUNDARY(TRISE). TIMES ARE IN SECONDS AFTER NOONTIME.
367 C
368 C GEORAD = GEOMETRIC RADIUS OF EARTH IN KM
369 C USE SWIDER PLANET SPACE SCI 1964,V12,P766, TABLE 1
370 C ASSUME EARTH LOCALLY SPHERICAL FOR SUNSET/SUNRISE
371 C (NEGLECT LATITUDE CHANGE WHERE RAYPATH TANGENT EARTH)
372 C
373 AE=6378.4
374 AP = 6356.9
375 GEORAD=AE/SORT(1.0+(((AE/AP)**2-1.0)*SIN(PHILAT)**2))
376 DO 3015 J=1,K
377 SUNSET(J)=(PI/2.0)+ACOS(1.0/((1.0+Z(J)/GEORAD)))
378 EPSILON=2.0*(-20)
379 TS=(ACOS((COS(SUNSET(J))-SIND)/COSD)/RADSEC)+EPSILON
380 TR=86400.-TS+2.0*EPSILON
381 CHIS=ACOS(COSD+COS(RADSEC*TS)*SIND)
382 IF(CHIS .GT. SUNSET(J)) GO TO 3027
383 EPSILON=2*EPSILON
384 GO TO 3025
385 CHIR=ACOS(COSD+COS(RADSEC*TR)*SIND)
386 IF(CHIR .GE. SUNSET(J)) GO TO 3026
387 IF(J .EQ. 1) TSET=TS
388 IF(J .EQ. K) TRISE=TR
389 CONTINUE
390 C
391 C WRITE OUT INITIAL PROFILES.
392 C
393 N1=1
394 N2=11
395 DO 100 L=1,2
396 WRITE(6,605) TIME, SCXI, IFRAME
397 WRITE(6,610) (SYMBOL(M),M=1,N2)
398 WRITE(6,620) (Z(J),N(J,M),M=1,N2),J=1,K,12)
399 WRITE(6,630) Z(K),N(K,M),M=1,N2)

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OVERLAY(1,0)
PROGRAM INTEL
C
C DIMENSION PH(17),DEDZ(1),DEDOZ(1),VBAR(1),H(692)
C DIMENSION OUTP(4),WHICH(26),ITER(26),BIGEST(26),NSPEC(56)
COMMON N(92),DOL,CONEC(424,26),U(692,26),NZERO(592),UZERO(692)
COMMON FORM(692),REMY(692),E(692),F(692),Z(692),
2 DEDY(692),TEMP(692),DTEMOZ(692),DELTAZ(692),SUNSET(692)
COMMON GRAV,DSD,SIND,TIME,CXI,RADIUS,ISPECI,MSPECI,NREAC,K,
1 K2,MINI,ITURB,CXINCON,SCXI,NREAC2
COMMON/ESX,UCON(692,30),OLDCON(424,26),OLDU(692,26),RATES(88,692)
COMMON/TTURB,DAYS,DELT,TMAX,TSET,TRISE
COMMON/ALTI,TUD,ZSC1,ZTOP,TURB,ZTRANS
COMMON/REL,TART//IFRAME,TOFF,TYME,TDAY
COMMON/OUTPUTS//TIMOUT,OPRINT,PRINT
COMMON/ERRORS/ERRMAX,ERSPECI,ITMAX
COMMON/LOGIC/NIGHT,DAY,JLOOK,RESET,END
COMMON/A/CONS/ATW(26),MASS(26),THERM(26),SYMBOL(56),POLAR(26)
COMMON/CONSTAN/PI,RADDEG,DEGRAD,RAUSEC,BOLTZ,EIN21,AYCON
COMMON/COLUM/D2COL,D3COL,D1S(19,59)
COMMON/RATECON/AK(88),BK(88),CK(88),DK(215),CYMB(6,215)
LEVEL 3, OLDN,OLDCON,OLDU,RATES
REAL N,NZERO,NEWN,MASS,MBAR,NTOTAL
LOGICAL JLOOK,NIGHT,DAY,RESET,PRINT,END,LASTINT,LASTIDA
EQUIVALENCE (U(1,21),H,PHI),(E,DED),(F,VBAR),(NZERO,DEDZ)
EQUIVALENCE (UZERO,DEDZ)
DATA NSWCH/1/
FUNCTION DEFINITION FOR CORRECTION TO ACCELERATION OF GRAVITY.
GRAVCOR(ZZ)=1.0/(1.0+ZZ/RADIUS)**2)
C
C IF ANY SMOOTHING IS TO BE DONE, SET NUM TO THE NUMBER OF SPECIES
C TO BE SMOOTHED AND PUT THEIR SPECI NUMBERS INTO THE NSPEC REGION.
C IF NO SMOOTHING IS TO BE DONE, SET NUM TO ZERO.
NUM=0
ENG=.FALSE.
DOCORE=0
DAYTIME=LAST_SUNSET(1)
NEGATIVE LOG CONASET(K)

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OVERLAY 12, 0
PROGRAM INTEL

DIMENSION PH1(17),DEDZ(1),DEDZ(1),DEDZ(1),VBAR(1),M(692)
DIMENSION OUT(4),WHICH(26),ITER(26),BIGEST(26),NSPEC(56)

COMMON N(692),D1,CONC(424,26),U(692,26),NZERO(592),UZERO(692)

COMMON FORM(692),REMY(692),E(692),F(692),Z(692),
      BODY(692),TEMP(692),ITEMOZ(692),DELTAZ(692),SUNSET(692)

COMMON GRAV(350),SIND,TIME,CXI,RADIUS,ISPECI,KSPECI,NREAC,K,
      K2,KMIN1,ITURB,CXINCON,SCXI,NREAC2

COMMON,ESM,OLDN(692,30),OLDCON(424,26),OLDU(692,26),RATES(88,692)

COMMON,TIME,RAYS,DELT,IMAX,ISSET,TRISE

COMMON,ALTITUO,Z821,Z10P,TURB,Z1TRANS

COMMON,REL,TART,IFRAME,TOFF,TIME,TDAY

COMMON,OUTPUS,TIMEOUT,OPRINT,PRINT

COMMON,ERPORS,ERRMAX,ERSPECI,ITMAX

COMMON,LOGIC/NIGHT,DAY,JLOOK,RESET,END

COMMON,ATCONS,ATW(26),MASS(26),THERM(26),SYMBOL(56),POLAR(26)

COMMON,CONSTAN/PI,RADDEG,DEGRAD,RADSEC,BOLTZ,FINZI,ATCON

COMMON,COLUM/D3COL,OCOL,D1S(15,59)

COMMON/RATECON/AK(88),BK(88),CK(88),DK(215),CYMB(6,215)

LEVEL 3, OLDN,OLDCON,OLDU,RATES
REAL N,NZERO,NEWN,MASS,MBAR,NTOTAL
LOGICAL JLOOK,NIGHT,DAY,RESET,PRINT,END,LASTIN,LASTDA
EQUIVALENCE (U(1,21),M,PHI),(E,DED),(F,VBAR),(NZERO,DEDZ)
EQUIVALENCE (NZERO,DEDZ)

DATA NSWCH/1/

NCTION DEFINITION FOR CORRECTION TO ACCELERATION OF GRAVITY.
GRAYCOR(ZZ)=1.0/(1.0+ZZ/RADIUS)**2)

ANY SMOOTHING IS TO BE DONE, SET NUM TO THE NUMBER OF SPECIES
BE SMOOTHED AND PUT THEIR SPECI NUMBERS INTO THE NSPEC REGION.
NO SMOOTHING IS TO BE DONE, SET NUM TO ZERO.

NUM=0
END=FALSE
JLOOK=FALSE
DAY=0,NIGHT=0,SUNSET(1)
NIGHT=0,TIMEOUT=0,CONSET(K)

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[illegible]

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      EDDYL=EDDY
      EDDY=EDDY(U)
      DT0Z=1.0/(DT+DZL)
      DZ0ZL=DZ/DZL
      IF(U.GT.11CRB) GO TO 15
      TIL=0.
      WBAR=0.
      DO 10 L=1,KSPECI
      EN=N(J,L)
      WBAR=WBAR+MASS(L)*EN
      TIL=TIL+EN
      CONTINUE
      WBAR=WBAR/TIL
      GAMBA=GAMBA
      GAMBA=1.0-(DNTDZ+GRAV*GCRN+WBAR/(BOLTZ*T))*DZ
      DT0Z=DELTDZ0Z
      IF(J.EQ.1) GO TO 20
      AU=DT0Z*(PU+UTKM+EDDY)
      BU=1.0-DZ0Z*(PU+U*DT+DTKM+GAM)+PUL*DTKM*DZ0ZL
      TIL=EDDY+GAMBA*EDDY+DZ0ZL*(IREMV(U)+PJ*SNUM*DELT/DZL)*DELT
      CU=DT0Z*(U+UJUL+DZ+DTKM*GAML*DZ0ZL)+EDDYL*GAMBA*L*DZ0ZL
      TIL=CU+SNUM*DELT/DZL)*DELT
      GO TO 35
10      C
15      C COMPUTE LOWER BOUNDARY VALUES OF E AND F USING THE LOWER
      C BOUNDARY CONDITIONS.
      C
20      EUL=0.
      IF((I.EQ.8).OR.(I.EQ.13).OR.(I.EQ.15).OR.(I.EQ.21)) GO TO 30
      IF((I.EQ.22).OR.(I.EQ.23)) GO TO 30
      FUL=(NZERO(1)+DELT*FORM(1))/(1.0+DELT*REMV(1))
      GO TO 70
30      FUL=N(1,1)
      GO TO 70
35      IF(J.EQ.K) GO TO 50
      DENOM=1.0/(BU-CU*EUL)
      EUL=AU*DENOM
      DU=NZERO(U)+DELT*FORM(U)
      FUL=(DU+CU*FUL)*DENOM
      GO TO 70
      C
100     C COMPUTE UPPER BOUNDARY VALUES OF E AND F USING THE UPPER
      C BOUNDARY CONDITIONS.
      C
50      DU=NZERO(K)+DELT*FORM(K)
56      VEL(1)=0.
      IF((I.EQ.4).OR.(I.EQ.5).OR.(I.EQ.9)) GO TO 57
      IF(I.EQ.11) GO TO 57
      IF(I.EQ.12).AND.(I.LE.15)) GO TO 57
      IF((I.EQ.19).OR.(I.EQ.19).OP.(I.EQ.20).OR.(I.EQ.22)) GO TO 57
      IF((I.EQ.27).AND.(I.LE.29)) GO TO 57
      CALL VELOCITY(I)
      IF(ICF.LT.0) GO TO 65
      IF(I.EQ.11) GO TO 80
      CALL GIBBSFREE(K,SNUM,OMEG)
      SS=SNUM*VEL(1)*SNUM
      FUL=(CU+CU*FUL)/(BU-AU*(GAM+SS*(DELT*(K)*WGT/(BOLTZ*TEMP(K))))))

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1      SUBROUTINE EFORU(ICF)
C
C      IF(1/ICF .GT. 0). COMPUTE THE E AND F ARRAYS.
C      IF(1/ICF .LT. 0). COMPUTE THE SPECIFIC VELOCITIES.
C
5      DIMENSION H(1)
C
C      COMMON N(692,30),CONC(424,26),U(692,26),NZERO(692),UZERO(692)
C
10     COMMON FORM(692),REMV(692),E(692),F(692),Z(692),
2      DEDY(692),TEMP(692),DTENDZ(692),DELTAZ(692),SUNSET(692)
C
C      COMMON GRAV,COSD,SIND,TIME,CXI,RADIUS,ISPECI,KSPECI,NREAC,K,
1      K2,KMINI,ITURB,CXINCON,SCXI,NREAC2
C
15     COMMON/TIMES/DAYS,DELT,TMAX
C
C      COMMON/ALTTUD/ZBOT,ZTOP,TURB,TURBVAR
C
20     COMMON/BOUNDARY/VEL(26)
C
C      COMMON/CONSTAN/PI,RADDEG,DEGRAD,RADSEC,BOLTZ,SINZI,ATCON
C
25     COMMON/ATCONS/ATWT(26),MASS(26),THERM(26),SYMBOL(56),POLAR(26)
C
C      REAL N,NZERO,MASS
C      EQUIVALENCE (U(1,21),H)
C
30     I=ICF
      IF(I .GT. 0) GO TO 1
      I=-I
      WGT=MASS(I)
      GMOVK=GRAV*WGT/BOLTZ
      DTKOVM=DELT*BOLTZ/WGT
      DZ=1.5E+04
      DO 75 J=1,K
      ZE=Z(J)
      T=TEMP(J)
      DZL=DZ
      DZ=DELTAZ(J)
      DLNTDZ=DTENDZ(J)
      IF(I .GT. 6) GO TO 6
      DLNTDZ=2.0*DLNTDZ
      GCRN=1.0/((1.0+ZE/RADIUS)**2)
      DTKTML=DTKTM
      DTKTM=DTKOVM*T
      GAML=GAM
      GAM=1.0-(THERM(I)*DLNTDZ+GCRN*GMOVK/T)*DZ
      IF(I .GT. 6) GO TO 11
      GAM=GAM-H(J)*DZ
      PJL=PJ
      SNWL=SNWL
      CALL COLFRE(I,J,SNL,SNWL,OMEG)
      PU=1.0/(1.0+SNL*OMEG*DELT)
      UJL=UJ
      UU=UZE+UJ
      IF(1/ICF .LT. 0) GO TO 60

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GIONEUT 757
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GIONEUT 811
GIONEUT 812
GIONEUT 813

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1      SUBROUTINE CO(J,RHO,NTOTAL,MBAR,VO)
C
C      THIS SUBROUTINE COMPUTES THE TOTAL MASS DENSITY, RHO, THE TOTAL
C      CONCENTRATION, NTOTAL, THE MEAN MOLECULAR WEIGHT, MBAR, AND THE
5      MEAN MASS VELOCITY, VO, AT ALTITUDE WHERE THE INDEX IS J.
C
C      COMMON N(692,30),CONC(424,26),U(692,26),NZERO(692),UZERO(692)
C
C      COMMON FORM(692),REMV(692),E(692),F(692),Z(692),
10      DE%(692),TEMP(692),STEMOZ(692),DELTAZ(692),SUNSET(692)
C
C      COMMON GRAV,COSD,SIND,TIME,CXI,RADIUS,ISPECI,KSPECI,NREAC,K,
15      K2,KMIN1,ITURB,CXINCON,SCXI,NREAC2
C
C      COMMON,NTCONS/ATWT(26),MASS(26),THERM(26),SYMBOL(56),POLAR(26)
C
C      REAL N,MBAR,NTOTAL,MASS
C
C      RHO=0.
C      NTOTAL=0.
C      RHOC=0.
20      DO 5 M=1,KSPECI
C      EN=N(J,M)
C      ENM=MASS(M)*EN
C      RHC=RHO+ENM
C      NTOTAL=NTOTAL+EN
25      IF(M.EQ.21) GO TO 5
C      RHOC=RHOC+ENM*U(J,M)
C      CONTINUE
C      MBAR=RHO/NTOTAL
C      VO=RHOC/RHO
30      RETURN
C      END

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GIONEUT 724  
 GIONEUT 725  
 GIONEUT 726  
 GIONEUT 727  
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 GIONEUT 756

1		SUBROUTINE SMOOTH(A,N,M,B)	GIONEUT 675
	C		GIONEUT 676
	C	THIS SUBROUTINE SMOOTHS ARRAY A OF N POINTS WITH AN M POINT	GIONEUT 677
5	C	RUNNING MEAN. THE SMOOTHED ARRAY IS STORED IN B.	GIONEUT 678
	C		GIONEUT 679
	C	DIMENSION A(1),B(1)	GIONEUT 680
		IF(M.EQ.0) GO TO 10	GIONEUT 681
10		I=(M-1)/2	GIONEUT 682
		K=N-M+1	GIONEUT 683
		C=M	GIONEUT 684
		DO 2 J=1,K	GIONEUT 685
		S=0.	GIONEUT 686
		JJ=J+M-1	GIONEUT 687
15		DO 1 L=J,JJ	GIONEUT 688
	1	S=S+A(L)	GIONEUT 689
		JAY=J+I	GIONEUT 690
	2	B(JAY)=S/C	GIONEUT 691
		I1=0	GIONEUT 692
20		K=M-2	GIONEUT 693
	3	C=K	GIONEUT 694
		S=0.	GIONEUT 695
		DO 4 J=1,K	GIONEUT 696
25	4	S=S+A(J)	GIONEUT 697
		JAY=I-I1	GIONEUT 698
		B(JAY)=S/C	GIONEUT 699
		K=K-2	GIONEUT 700
		I1=I1+1	GIONEUT 701
30		IF(K.NE.1) GO TO 3	GIONEUT 702
		I1=1	GIONEUT 703
		K=N-M+3	GIONEUT 704
		C=M-2	GIONEUT 705
	5	S=0.	GIONEUT 706
		DO 6 J=K,N	GIONEUT 707
35	6	S=S+A(J)	GIONEUT 708
		JAY=N-I+I1	GIONEUT 709
		B(JAY)=S/C	GIONEUT 710
		K=K+2	GIONEUT 711
		C=C-2.	GIONEUT 712
40		I1=I1+1	GIONEUT 713
		IF(K.NE.N) GO TO 5	GIONEUT 714
		B(1)=A(1)	GIONEUT 715
		B(N)=A(N)	GIONEUT 716
		RETURN	GIONEUT 717
45	10	DO 20 J=1,N	GIONEUT 718
		B(J)=A(J)	GIONEUT 719
	20	CONTINUE	GIONEUT 720
		RETURN	GIONEUT 721
		END	GIONEUT 722
			GIONEUT 723



60	C	RETURN		GIONEUT 627
	C	ADJUST THE LARGEST NEGATIVE SPECIES CONCENTRATIONS TO		GIONEUT 628
	C	INSURE CONSERVATION OF CHARGE.		GIONEUT 629
	C			GIONEUT 630
	C			GIONEUT 631
25		DO 50 J=1,K2		GIONEUT 632
		SUMP=0.		GIONEUT 633
65		SUMM=0.		GIONEUT 634
		DO 30 I=1,6		GIONEUT 635
		SUMP=SUMP+N(J,I)		GIONEUT 636
30		CONTINUE		GIONEUT 637
		DO 35 I=28,29		GIONEUT 638
70		SUMP=SUMP+N(J,I)		GIONEUT 639
		CONTINUE		GIONEUT 640
35		DO 40 I=9,24		GIONEUT 641
		SUMP=SUMP+N(J,I)		GIONEUT 642
40		CONTINUE		GIONEUT 643
		BIG=N(J,30)		GIONEUT 644
75		JBIG=1		GIONEUT 645
		DO 70 I=1,8		GIONEUT 646
		IF (CONC(J,I) .LE. BIG) GO TO 70		GIONEUT 647
80		BIG=CONC(J,I)		GIONEUT 648
		JBIG=JBIG+1		GIONEUT 649
70		CONTINUE		GIONEUT 650
		DO 75 I=1,9		GIONEUT 651
		IF (I .EQ. JBIG) GO TO 75		GIONEUT 652
85		IF (I .EQ. 1) SUMM=SUMP+N(J,30)		GIONEUT 653
		IF (I .NE. 1) SUMM=SUMM+CONC(J,I-1)		GIONEUT 654
75		CONTINUE		GIONEUT 655
		BAL=SUMP-SUMM		GIONEUT 656
		IF (BAL .LT. 0.) STOP 7		GIONEUT 657
90		IF (JBIG .EQ. 1) N(J,30)=BAL		GIONEUT 658
		IF (JBIG .NE. 1) CONC(J,JBIG-1)=BAL		GIONEUT 659
50		CONTINUE		GIONEUT 660
		KK=K2+1		GIONEUT 661
		DO 65 J=KK,K		GIONEUT 662
95		SUMP=0.		GIONEUT 663
		DO 55 I=1,6		GIONEUT 664
		SUMP=SUMP+N(J,I)		GIONEUT 665
55		CONTINUE		GIONEUT 666
		DO 60 I=28,29		GIONEUT 667
100		SUMP=SUMP+N(J,I)		GIONEUT 668
		CONTINUE		GIONEUT 669
60		N(J,30)=SUMP		GIONEUT 670
65		CONTINUE		GIONEUT 671
		RETURN		GIONEUT 672
105		END		GIONEUT 673
				GIONEUT 674

```

1      SUBROUTINE SMOOTHY(NUM,NSPEC)
2
3      THIS SUBROUTINE SMOOTHS SPECIFIED PROFILES WITH AN "IRUN" POINT
4      RUNNING MEAN.
5
6      DIMENSION NSPEC(1),ZNEW(792),DENS(792),SMUTHN(1)
7
8      COMMON N(692,30),CONC(424,26),U(692,26),NZERO(692),UZERO(692)
9
10     COMMON FORM(692),REMV(692),E(692),F(692),Z(692),
11     DEDY(692),TEMP(692),DTEMZ(692),DELTAZ(692),SUNSET(692)
12
13     COMMON GRAV,COSD,SIND,TIME,CXI,RADIUS,ISPECI,KSPECI,NREAC,K,
14     K2,KMINI,ITURB,CXINCON,SCXI,NREAC2
15
16     COMMON/ATCONS/ATWT(26),MASS(26),THERM(26),SYMBOL(56),POLAR(26)
17
18     COMMON/CONSTAN/PI,RADDEG,DEGRAD,RADSEC,BOLTZ,SIN2I,ATCON
19
20     REAL N,NZERO,MASS
21
22     EQUIVALENCE (NZERO,DENS), (FORM,SMUTHN)
23     EQUIVALENCE (E,ZNEW)
24
25     DATA IRUN,7/
26
27     IF (NUM .EQ. 0) RETURN
28
29     GOVKT=(GRAV*(1.0/((1.0+400./RADIUS)*2)))/(BOLTZ*TEMP(K))
30     R=6.35107E+08
31     DO 5 J=1,692
32       ZNEW(J)=Z(J)
33       CONTINUE
34     DO 6 J=693,792
35       ZNEW(J)=ZNEW(692)+FLOAT(J-692)
36       CONTINUE
37     DO 15 I=1,NUM
38       L=NSPEC(I)
39       DO 7 J=1,692
40         DENS(J)=N(J,L)
41         CONTINUE
42
43     C  EXTRAPOLATE THE CONCENTRATION OF SPECIES L TO 500 KM ASSUMING
44     C  DIFFUSIVE EQUILIBRIUM ABOVE THE UPPER BOUNDARY.
45
46     DO 8 J=693,792
47       DENS(J)=DENS(692)*EXP(-(GOVKT*MASS(L)*(ZNEW(J)-400.)*1.025)
48       1/((1.0+400./RADIUS)*2.0)*((ZNEW(J)-1.0E5/R)+1.0)))
49       CONTINUE
50     CALL SMOOTH(DENS,792,IRUN,SMUTHN)
51
52     DO 10 J=1,K
53       N(J,L)=SMUTHN(J)
54       CONTINUE
55     DO 20 I=1,NUM
56       I=NSPEC(I) !LT. 7) GO TO 25
57       CONTINUE
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GIONEUT 570
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515	228	FORMAT(110,*,DAY IS *,L1,5X,NIGHT IS *,L1,5X,*DAY-NIGHT*,	G1ONEUT	515
		1* TRANSITION HEIGHT IS *,F7.2)	G1ONEUT	516
		IF(END) GO TO 270	G1ONEUT	517
		CALL MOVLEV(U,OLDU,17992)	G1ONEUT	518
		CALL MOVLEV(N,OLDN,20760)	G1ONEUT	519
520		CALL MOVLEV(CONC,OLDCON,11024)	G1ONEUT	520
		CALL SECOND(T1)	G1ONEUT	521
		GO TO 1000	G1ONEUT	522
			G1ONEUT	523
			G1ONEUT	524
525	230	CXI=OLDCXI	G1ONEUT	525
		SCXI=CXI*DEGRAD	G1ONEUT	526
		TIME=TIME-DELT	G1ONEUT	527
		DELT=OLDELT	G1ONEUT	528
530		ZTRANS=OLDZIR	G1ONEUT	529
		IF(PRINT) TIMEOUT=TIMEOUT-OPRINT	G1ONEUT	530
		PRINT=TRUE.	G1ONEUT	531
		END=TRUE.	G1ONEUT	532
		LM=1	G1ONEUT	533
535		GO TO 235	G1ONEUT	534
			G1ONEUT	535
			G1ONEUT	536
			G1ONEUT	537
			G1ONEUT	538
540		C ENTER HERE ON CALCULATION OF A NEGATIVE CONCENTRATION.	G1ONEUT	539
			G1ONEUT	540
			G1ONEUT	541
			G1ONEUT	542
			G1ONEUT	543
545	245	KFAIL=2	G1ONEUT	544
		J=K	G1ONEUT	545
		GO TO 255	G1ONEUT	546
	250	KFAIL=3	G1ONEUT	547
		J=L	G1ONEUT	548
			G1ONEUT	549
			G1ONEUT	550
550	255	WRITE(6,256)KFAIL,SYMBOL(I),Z(J),NEWN,N(J,I),TIME,DELT,SCXI,	G1ONEUT	551
		TITRATE	G1ONEUT	552
	258	FORMAT(113,A10,OPF7.1,1P5E20.12,15)	G1ONEUT	553
			G1ONEUT	554
			G1ONEUT	555
			G1ONEUT	556
555		C ENTER HERE ON ERROR FROM SUBROUTINE CHEMION.	G1ONEUT	557
			G1ONEUT	558
			G1ONEUT	559
			G1ONEUT	560
560	254	TIME=OLDTIME	G1ONEUT	561
		END=.FALSE.	G1ONEUT	562
		CXI=OLDCXI	G1ONEUT	563
		DELT=DELT*0.5	G1ONEUT	564
		IF(RESET) GO TO 257	G1ONEUT	565
		IF(DELT.LT. 2.0*(-40)) 265,258	G1ONEUT	566
	257	RESET=.FALSE.	G1ONEUT	567
		TIMEOUT=TIMEOUT-OPRINT	G1ONEUT	568
	258	LM=2	G1ONEUT	569
	235	NIGHT=LASTNT		
		DAY=LASTDA		
		CALL MOVLEV(OLDN,N,20760)		
		CALL MOVLEV(OLDCON,CONC,11024)		
		CALL MOVLEV(OLDU,U,17992)		
		IF(LM.EQ.1) 162,1000		
565	265	WRITE(6,345) TIME		
	345	FORMAT(30H THE INCREMENT IS VANISHING AT1P5E12.5,5H SEC.)		
		GO TO 230		
	270	CONTINUE		
		END		

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460      340      WRITE(6,340)
          FORMAT(1H1)
          WRITE(6,196) TIME,SCXI,IFRAME,IDAY,(OUTP(J),J=1,4)
          WRITE(6,310)
          FORMAT(* ALT(KM) NO+/O2+ RATIO MEAN MOL WT MASS DENSITY*,
1* TOTAL NUMBER MEAN MASS VEL K-EDDY*)
          DO 325 J=1,K,12
          CALL CO(J,RHO,NTOTAL,MBAR,VMEAN)
          MBAR=MBAR/ATCON
          RNOTO2=N(J,5)/N(J,4)
          WRITE(6,330) Z(J),RNOTO2,MBAR,RHO,NTOTAL,VMEAN,DEDY(J)
          CONTINUE
          CALL CO(KMIN1,RHO,NTOTAL,MBAR,VMEAN)
          MBAR=MBAR/ATCON
          RNOTO2=N(KMIN1,5)/N(KMIN1,4)
          WRITE(6,330) Z(KMIN1),RNOTO2,MBAR,RHO,NTOTAL,VMEAN,DEDY(KMIN1)
          CALL CO(K,RHO,NTOTAL,MBAR,VMEAN)
          MBAR=MBAR/ATCON
          RNOTO2=N(K,5)/N(K,4)
          WRITE(6,330) Z(K),RNOTO2,MBAR,RHO,NTOTAL,VMEAN,DEDY(K)
          FORMAT(OPF8.2,1PE13.5,OPF10.3,4(3X,1PE13.5))
          330
          C
          C PRINT LIST OF CHEMICAL REACTIONS WITH THE RATE OF EACH AT
          C SELECTED ALTITUDES.
          C
          CALL CHEMPR(1)
          CALL CHEMPR(253)
          CALL CHEMPR(337)
          CALL CHEMPR(457)
          CALL CHEMPR(K)
          DELT=AMIN1(2.0*DELT,TMAX)
          IF(.NOT. PRINT) GO TO 161
          160
          C
          C WRITE INTERRUPT FILE ON TAPE 4.
          C
          WRITE(4) TODAY,IFRAME,TIME,SCXI,CXI,DELT,TIMOUT
          DO 2224 L=1,KSPECI
          WRITE(4) (U(J,L),J=1,K)
          CONTINUE
          2224
          DO 280 L=1,ISPECI
          IF(L.GT. 30) GO TO 281
          WRITE(4) (N(J,L),J=1,K)
          GO TO 280
          281
          WRITE(4) (CONC(J,L-30),J=1,K2)
          280
          CONTINUE
          ENDFILE 4
          CALL CLOCK(A1)
          WRITE(6,315) A1,IFRAME
          315
          FORMAT(1H0,A17,* FRAME NO. *,14,* HAS BEEN WRITTEN ON THE*,
1* INTERRUPT TAPE.*)
          161
          CALL HOUR(TIME,OUTP)
          CALL CLOCK(A1)
          WRITE(6,227) A1,TIME,DELT,SCXI,ITRATE,(OUTP(J),J=1,4),DTIME
          227
          FORMAT(1H0,A10,* TIME =*,1PE12.5,* SEC. TIME INCREMENT =*,
1E12.5,* CHI =*,OPF7.2,* ITERATIONS =*,14,* HOUR =*,4A1,
2* CP TIME =*,F10.2,* SEC.*)
          WRITE(6,228) DAY,NIGHT,ZTRANS

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400	1*NUMBER	CHEMISTRY	6X,*	ALT	NUMBER	*,	GIONEUT	401
	2*CHEMISTRY	CHEMISTRY*					GIONEUT	402
201	FORMAT(*	KM	DENSITY	FORMATION	REMOVAL*,BX,*	KM	*,	GIONEUT
	1*DENSITY	FORMATION	REMOVAL*,BX,*	KM	DENSITY*,		GIONEUT	403
	2*FORMATION	REMOVAL*					GIONEUT	404
405	WRITE(6,200)						GIONEUT	405
	WRITE(6,201)						GIONEUT	406
	WRITE(6,202)						GIONEUT	407
410	1	WRITE(6,202)		(Z(J),CONC(J,I-3),E(J),H(J),Z(J),CONC(J,I-2),F(J),			GIONEUT	408
				UZERO(J),Z(J),CONC(J,I-1),FORM(J),REMV(J),J=1,K2,12)			GIONEUT	409
	1	WRITE(6,202)		Z(K2),CONC(K2,I-3),E(K2),H(K2),Z(K2),CONC(K2,I-2),			GIONEUT	410
	1			F(K2),UZERO(K2),Z(K2),CONC(K2,I-1),FORM(K2),REMV(K2)			GIONEUT	411
	202	FORMAT(3,OPF7.2,1P3E10.3,6X)					GIONEUT	412
210	CONTINUE						GIONEUT	413
	I=25						GIONEUT	414
	DO 237 LL=1,2						GIONEUT	415
415	DO 211 J=1,K2						GIONEUT	416
	CALL CHEM(I+30,J)						GIONEUT	417
	REMV(J)=REMV(J)*CONC(J,I)						GIONEUT	418
211	CONTINUE						GIONEUT	419
	IF(LL.EQ. 2) GO TO 240						GIONEUT	420
420	DO 236 J=1,K2						GIONEUT	421
	NZERO(J)=FORM(J)						GIONEUT	422
	UZERO(J)=REMV(J)						GIONEUT	423
236	CONTINUE						GIONEUT	424
	I=I+1						GIONEUT	425
237	CONTINUE						GIONEUT	426
240	DO 241 J=1,K2						GIONEUT	427
425	E(J)=0.						GIONEUT	428
	F(J)=0.						GIONEUT	429
	H(J)=0.						GIONEUT	430
430	DO 312 I=1,6						GIONEUT	431
	E(J)=E(J)+N(J,I)						GIONEUT	432
312	CONTINUE						GIONEUT	433
	E(J)=E(J)+N(J,28)+N(J,29)						GIONEUT	434
	DO 313 I=9,24						GIONEUT	435
435	E(J)=E(J)+CONC(J,I)						GIONEUT	436
	CONTINUE						GIONEUT	437
313	DO 314 I=1,8						GIONEUT	438
	F(J)=F(J)+CONC(J,I)						GIONEUT	439
314	CONTINUE						GIONEUT	440
440	H(J)=F(J)/N(J,30)						GIONEUT	441
	CONTINUE						GIONEUT	442
	WRITE(6,340)						GIONEUT	443
	WRITE(6,196)			TIME,SCXI,IFRAME,IDAY,(OUTP(J),J=1,4)			GIONEUT	444
445	WRITE(6,212)			SYMBOL(55),SYMBOL(56)			GIONEUT	445
	FORMAT(10X,A10,' PROFILE*,20X,A10,' PROFILE*)						GIONEUT	446
	WRITE(6,213)						GIONEUT	447
213	FORMAT(*	ALT	NUMBER	CHEMISTRY	NUMBER	*,	GIONEUT	448
	1*CHEMISTRY	CHEMISTRY	TOTAL	IONS	LAMBDA*,		GIONEUT	449
	WRITE(6,214)						GIONEUT	450
450	FORMAT(*	KM	DENSITY	FORMATION	REMOVAL	KM	DENSITY	*,
	1*FORMATION	REMOVAL	POSITIVE	NEGATIVE*)			GIONEUT	451
	WRITE(6,215)			(Z(J),CONC(J,25),NZERO(J),UZERO(J),Z(J),CONC(J,26),			GIONEUT	452
	1FORM(J),REMV(J),E(J),F(J),H(J),J=1,K2,12)						GIONEUT	453
	WRITE(6,215)			Z(K2),CONC(K2,25),NZERO(K2),UZERO(K2),Z(K2),			GIONEUT	454
	CONC(K2,26),FORM(K2),REMV(K2),E(K2),F(K2),H(K2)						GIONEUT	455
455	FORMAT(3,OPF7.2,1P3E10.3,OPF7.2,1P3E10.3,3E12.5)						GIONEUT	456
215							GIONEUT	457



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230 IF(ITMAX.EQ.1) GO TO 139
    IF(ITRATE.EQ.1) GO TO 130
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175      C      CALL EFORU(I)
      C      COMPUTE HEIGHT PROFILES AT (T+DELTA T) USING THE RECURSION
      C      RELATION  $N(J)=N(J+1)*E(J)+F(J)$ .
      C
      C      NEWN=F(K)
      C
      C      IF(NEWN.GT. 0.) GO TO 10
      C      IF(N(K,I).GT. 1.0E-02) GO TO 245
      C      NEWN=N(K,I)
      C      IF(ITRATE.EQ. 1) GO TO 70
      C      IF(MEAN.LT. 1.0) GO TO 70
      C      RELE=ABS(NEWN-N(K,I))/NEWN
      C      BIGEST(I)=RELE
      C      N(K,I)=NEWN
      C      DO 100 J=1,KMIN1
      C      L=K-J
      C      NEWN=E(L)*N(L+1,I)+F(L)
      C      IF(NEWN.GT. 0.) GO TO 11
      C      IF(N(L,I).GT. 1.0E-02) GO TO 250
      C      NEWN=N(L,I)
      C      IF(ITRATE.EQ. 1) GO TO 95
      C      IF(NEWN.LT. 1.0) GO TO 95
      C      RELE=ABS(NEWN-N(L,I))/NEWN
      C      IF(BIGEST(I).LT. RELE) BIGEST(I)=RELE
      C      N(L,I)=NEWN
      C      100 CONTINUE
      C      105 CONTINUE
      C
      C      COMPUTE THOSE SPECIES TO BE DETERMINED FROM CHEMISTRY ONLY.
      C
      C      CALL CHEMION
      C
      C      IF(END) GO TO 254
      C
      C      GO GET THE VELOCITIES FOR SPECIES IN THE TRANSPORT MODE.
      C
      C      DO 110 I=1,KSPECI
      C      IF(I.EQ. 21) GO TO 110
      C      CALL MOVLEV(OLDU(1,I),UZERO,K)
      C      CALL CHEM(I,KMIN1)
      C      CALL CHEM(I,K)
      C      IF(I.NE. 1) GO TO 108
      C      DO 107 J=2,K
      C      H(J)=(1.0-(N(J-1,30)/N(J,30)))/DELTAT(J-1)
      C      107 CONTINUE
      C      H(1)=H(2)
      C      108 CALL EFORU(-1)
      C
      C      TEST FOR TERMINATION OF CALCULATIONS.
      C
      C      CALL SWITCH(NSWCH,NSTATUS)
      C      IF(NSTATUS.NE.2) GOTO 230
      C      CALL SECOND(TA)
      C      IF((TYNE-TA).LT.TOFF) GOTO 230
      C      110 CONTINUE
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135 DO 625 J=1,50
136   WRITE(6,610) (DIS(15,J),DIS(16,J),DIS(17,J),LL=7,14)
137   CONTINUE
138   LOOKUP=FASE
139   IF (IP .EQ. 1) GO TO 6
140   IF (IP .EQ. 2) GO TO 6
141   IF (IP .EQ. 3) GO TO 6
142   IF (IP .EQ. 4) GO TO 6
143   CALL SMOOTHY(NUM,NSPEC)
144   WRITE(6,2)
145   FORMAT(1H0,*, THE FOLLOWING SPECIES PROFILES HAVE BEEN*,
146   1* SMOOTHED.*)
147   DO 4 I1=1,NUM
148   LENSPEC(I1)
149   WRITE(6,3) SYMBOL(L)
150   FORMAT(10X A10)
151   CONTINUE
152   C
153   C RECOMPUTE THE VELOCITY PROFILES FOR THOSE SPECIES WHOSE
154   C CONCENTRATION PROFILES HAVE BEEN SMOOTHED.
155   C
156   IP=0
157   DO 29 IM=1,NUM
158   I1=NSPEC(IM)
159   IP=IP+1
160   IF (IP .NE. 1) GO TO 40
161   CALL MOVLEV(OLDU(1,I1),UZERO,K)
162   CALL CHEM(I1,KMIN)
163   CALL CHEM(I1,K)
164   IF (IM .NE. 1) GO TO 28
165   DO 27 J=2,K
166   H(J)=(1.0-(N(J-1,30)/N(J,30)))/DELTAZ(J-1)
167   CONTINUE
168   H(1)=H(2)
169   CALL EFORU(-I1)
170   CONTINUE
171   CALL MOVLEV(U,OLDU,17992)
172   CALL MOVLEV(N,OLDN,20760)
173   CALL MOVLEV(CONC,OLDCON,11024)
174   IF (IWHICH(1) .EQ. 0) GO TO 105
175   CALL MOVLEV(OLDN(1,1),NZERO,K)
176   CALL MOVLEV(OLDU(1,1),UZERO,K)
177   C
178   C GO GET CHEMISTRY FORMATION AND REMOVAL RATES FOR SPECIES I.
179   C
180   DO 30 J=1,K
181   CALL CHEM(I,J)
182   C
183   C TEST FOR TERMINATION OF CALCULATIONS.
184   C
185   CALL SSATCH(NSWITCH,INSTATUS)
186   IF (INSTATUS .NE. 2) GO TO 230
187   CALL SECOND(TUSED)
188   IF ((TIME-TUSED) .LT. TOFF) GO TO 230
189   CONTINUE
190   C
191   C GO GET E AND V ARRAYS.

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115	1	-CJ*EJL)	GIONEUT	871
		EJL=0.	GIONEUT	872
		GO TO 70	GIONEUT	873
	80	FJL=(NZERO(K)+FORM(K)*DELT)/(1.0+REMV(K)*DELT)	GIONEUT	874
		EJL=0.	GIONEUT	875
120		GO TO 70	GIONEUT	876
	C		GIONEUT	877
	C	COMPUTE THE SPECIFIC VELOCITY ARRAY FOR SPECIES ICF.	GIONEUT	878
	C		GIONEUT	879
	60	IF(J.EQ.K) GO TO 56	GIONEUT	880
125		AJ=N(J+1,I)/N(J,I)	GIONEUT	881
		IF(N(J,I).GT.1.0E-10) GO TO 61	GIONEUT	882
		IF(AJ.LT.100.) GO TO 61	GIONEUT	883
		U(J,I)=0.	GIONEUT	884
		GO TO 75	GIONEUT	885
130	61	U(J,I)=PJ*(UJ-(DTKM/DZ)*(AJ-GAM)+DELT*SNUW)	GIONEUT	886
		GO TO 75	GIONEUT	887
	65	U(K,I)=VEL(I)	GIONEUT	888
		GO TO 75	GIONEUT	889
	70	E(J)=EJL	GIONEUT	890
135		F(J)=FJL	GIONEUT	891
	75	CONTINUE	GIONEUT	892
		RETURN	GIONEUT	893
		END	GIONEUT	894

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1      SUBROUTINE COLFRE(I,J,SNU,SNUM,OMEG)
2
3      C THIS SUBROUTINE COMPUTES THE SUM OF THE COLLISION FREQUENCIES
4      C AND THE SUM OF THE COLLISION FREQUENCIES TIMES THE VELOCITIES.
5      C SEE BANKS AND KOCHARTS, "AERONOMY", CHAPTER 9.
6
7      COMMON N(692,30),CONC(424,26),U(692,26),NZERO(692),UZERO(692)
8
9      COMMON FORM(692),REMI(692),E(692),F(692),Z(692),
10     DEDY(692),TEMP(692),DTEMDD(692),DELTAZ(692),SUNSET(692)
11
12     COMMON GRV,COSD,SIND,TIME,CX1,RADIUS,ISPECI,KSPECI,NREAC,K,
13     K2,KMIN1,ITURB,CXINCON,SCX1,NPEAC2
14
15     COMMON/ATCONS/ATWT(26),MASS(26),THERM(26),SYMBOL(56),POLAR(26)
16
17     COMMON/CONSTAN/PI,RADDEG,DEGRAD,RADSEC,BOLTZ,SIN2I,ATCON
18
19     COMMON/CCLFRE/D(26,26)
20
21     REAL N,MASS
22
23     DATA GAUS/0.25/,CHARG/4.803E-10/
24
25     SNU = 0.
26     SNUM = 0.
27     OMEG = 1.0
28     AMUI = ATWT(I)
29     T = TEMP(J)
30     ST = SORT(T)
31     T1 = 1.0/(T*.1.5)
32     T2 = 300.0/T
33     T3 = SORT(T2.0*T)
34     DO 50 L=1,KSPECI
35     AMUL = ATWT(L)
36     PRAG = 1.0/(SORT((AMUI*AMUL)/(AMUI+AMUL)))
37     IF (L .LE. 6) GO TO 15
38     IF (L .LE. 6) GO TO 25
39
40     C COMPUTE NEUTRAL-NEUTRAL COLLISION FREQUENCIES.
41
42     ANU = N(J,L)*D(T,L)*ST
43     SNU = SNU + ANU
44     IF (L .EQ. 21) GO TO 50
45     SNUM = SNUM + ANU*U(J,L)
46     GO TO 50
47     IF (L .GT. 6) GO TO 24
48
49     C COMPUTE ION-ION COLLISION FREQUENCIES.
50
51     ANU = 1.3*N(J,L)*RMAS*T1
52     GO TO 26
53
54     C COMPUTE ION-NEUTRAL COLLISION FREQUENCIES.
55
56     T1 = 1
57     GO TO 17

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24      11=L
27      ALF=POLAR(11)
60      IF(ALF .EQ. 0.) GO TO 50
C
C      AVERAGE ION-NEUTRAL COLLISION FREQUENCY FOR MOMENTUM TRANSFER.
C      BANKS AND KOCHARTS, EQUATION 9.73.
C
65      ANU=2.6E-09*N(J,L)*SQRT(ALF)*RMAS
      IF((1.EQ.1).AND.(L.EQ.7)).OR.((1.EQ.7).AND.(L.EQ.1))) GO TO 1
      IF((1.EQ.1).AND.(L.EQ.11)).OR.((1.EQ.11).AND.(L.EQ.1))) GO TO 11
      IF((1.EQ.2).AND.(L.EQ.8)).OR.((1.EQ.8).AND.(L.EQ.2))) GO TO 2
      IF((1.EQ.2).AND.(L.EQ.21)).OR.((1.EQ.21).AND.(L.EQ.2))) GO TO 21
      IF((1.EQ.2).AND.(L.EQ.23)).OR.((1.EQ.23).AND.(L.EQ.2))) GO TO 3
      IF((1.EQ.3).AND.(L.EQ.7)).OR.((1.EQ.7).AND.(L.EQ.3))) GO TO 31
      IF((1.EQ.3).AND.(L.EQ.8)).OR.((1.EQ.8).AND.(L.EQ.3))) GO TO 4
      IF((1.EQ.3).AND.(L.EQ.11)).OR.((1.EQ.11).AND.(L.EQ.3))) GO TO 5
      IF((1.EQ.4).AND.(L.EQ.18)).OR.((1.EQ.18).AND.(L.EQ.4))) GO TO 6
      IF((1.EQ.4).AND.(L.EQ.8)).OR.((1.EQ.8).AND.(L.EQ.4))) GO TO 61
      IF((1.EQ.6).AND.(L.EQ.8)).OR.((1.EQ.8).AND.(L.EQ.6))) GO TO 7
      IF((1.EQ.6).AND.(L.EQ.16)).OR.((1.EQ.16).AND.(L.EQ.6))) GO TO 71
      BNU=ANU*(AMUL/(AMU1+AMUL))
      SNU=SNU+BNU
      IF(1 .EQ. L) GO TO 50
      IF(L .EQ. 21) GO TO 50
      SNU=SNU+BNU*U(J,L)
      GO TO 50
26
C
C      AVERAGE COLLISION FREQUENCY FOR CHARGE EXCHANGE REACTION H+ - O.
C
85      ENG=3.8E-10*N(J,L)
      GO TO 8
C
C      AVERAGE REDUCED CHARGE EXCHANGE COLLISION FREQUENCY FOR H+ - H.
C
90      ANU=ANU+1.0E-10*T3*N(J,L)
      GO TO 26
C
C      AVERAGE COLLISION FREQUENCY FOR CHARGE EXCHANGE REACTION HE+ + O2.
C
95      ENG=2.0E-10*N(J,L)
      GO TO 8
C
C      AVERAGE REDUCED CHARGE EXCHANGE COLLISION FREQUENCY FOR HE+ + HE.
C
100     ANU=ANU+3.0E-11*T3*N(J,L)
      GO TO 26
C
C      AVERAGE COLLISION FREQUENCY FOR CHARGE EXCHANGE REACTION HE+ + N2.
C
105     ENG=3.5E-10*N(J,L)
      GO TO 8
C
C      AVERAGE REDUCED CHARGE EXCHANGE COLLISION FREQUENCY FOR O+ + O.
C
110     ANU=ANU+1.6E-11*T3*N(J,L)
      GO TO 26
C
C      AVERAGE COLLISION FREQUENCY FOR CHARGE EXCHANGE REACTION O+ + O2.

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GIONEUT 1007
GIONEUT 1008

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115	C	4	ENG=2.0E-11*(T2**0.4)*N(J,L) GO TO 8	GIONEUT 1009 GIONEUT 1010 GIONEUT 1011 GIONEUT 1012 GIONEUT 1013 GIONEUT 1014 GIONEUT 1015 GIONEUT 1016 GIONEUT 1017 GIONEUT 1018 GIONEUT 1019 GIONEUT 1020 GIONEUT 1021 GIONEUT 1022 GIONEUT 1023 GIONEUT 1024 GIONEUT 1025 GIONEUT 1026 GIONEUT 1027 GIONEUT 1028 GIONEUT 1029 GIONEUT 1030 GIONEUT 1031 GIONEUT 1032 GIONEUT 1033 GIONEUT 1034 GIONEUT 1035 GIONEUT 1036 GIONEUT 1037 GIONEUT 1038 GIONEUT 1039 GIONEUT 1040 GIONEUT 1041 GIONEUT 1042 GIONEUT 1043 GIONEUT 1044
120	C	5	AVERAGE COLLISION FREQUENCY FOR CHARGE EXCHANGE REACTION O+ + H. ENG=6.8E-10*N(J,L) GO TO 8	
125	C	6	AVERAGE COLLISION FREQUENCY FOR CHARGE EXCHANGE REACTION O2+ + NO. ENG=4.4E-10*N(J,L) GO TO 8	
130	C	61	AVERAGE REDUCED CHARGE EXCHANGE COLLISION FREQUENCY FOR O2+ + O2. ANU=ANU+1.1E-11*T3*N(J,L) GO TO 26	
135	C	71	AVERAGE REDUCED CHARGE EXCHANGE COLLISION FREQUENCY FOR N+ + N. ANU=ANU+1.7E-11*T3*N(J,L) GO TO 25	
140	C	7	AVERAGE COLLISION FREQUENCY FOR CHARGE EXCHANGE REACTION N+ + O2. ENG=5.5E-10*(T2**0.17)*2.0*N(J,L) ANU=ANU+1.73725*ENG GO TO 26 CONTINUE IF(I.GT. 6) RETURN G1=((GAUS*CHARG)/(MASS(1)*3.0E10))**2 G2=SNU**2 OMEG=(G1+G2)/(G1*SIN2I+G2) RETURN END	
145		50		
150				

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1      SUBROUTINE VELOCITY(I)
C
C
C      THIS SUBROUTINE COMPUTES THE VELOCITIES AT THE UPPER BOUNDARY
C      BY SOLVING OVER THE TOPMOST HEIGHT STEP THE ORDINARY DIFFERENTIAL
C      EQUATION RESULTING FROM SETTING DN/DI=0 IN THE CONTINUITY EQUATION.
C
C      COMMON N(692,30),CONC(424,26),U(692,26),NZERO(692),UZERO(692)
C
C      COMMON FORM(692),REMV(692),E(692),F(692),Z(692),
2      DEDY(692),TEMP(692),DTEMZ(692),DELTAZ(692),SUNSET(692)
C
C      COMMON GRAV,COSD,SIND,TIME,CX1,RADIUS,ISPECI,KSPECI,NREAC,K,
1      K2,KMIN1,ITURB,CXINNOON,SCXI,NREAC2
C
C      COMMON/BOUNDARY/VEL(26)
C
C      COMMON/RHSIDE/AN,BN,AP,BP,AL,BL
C
C      REAL N
20     AF(D1,D2,DZ)=(D1-D2)/DZ
        BF(D1,D2,D3,D4,DZ)=(D2*D3-D1*D4)/DZ
C
        ZE=Z(KMIN1)
        START=U(KMIN1,I)
        DZ=DELTAZ(K)
        D1=N(K,I)
        D2=N(KMIN1,I)
        D3=Z(K)*1.0E+05
        D4=Z(KMIN1)*1.0E+05
        AN=AF(D1,D2,DZ)
        BN=BF(D1,D2,D3,D4,DZ)
        D1=FORM(K)
        D2=FORM(KMIN1)
        AP=AF(D1,D2,DZ)
        BP=BF(D1,D2,D3,D4,DZ)
        D1=REMV(K)=N(K,I)
        D2=REMV(KMIN1)=N(KMIN1,I)
        AL=AF(D1,D2,DZ)
        BL=BF(D1,D2,D3,D4,DZ)
        CALL ODE(1,START,ZE,DZ)
        VEL(I)=START
        RETURN
        END
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1      SUBROUTINE ODE(N,START,SZ,DZ)
C
C      SUBPROGRAM TO SOLVE A SET OF ORDINARY DIFFERENTIAL EQUATIONS OF
C      SIZE N USING THE KUTTA-MERSON SCHEME.
C
5      DIMENSION V(7,2),START(2),SLOPE(2)
C
C      DATA IPASS/0/
C
10     IF(IPASS.NE.0) GO TO 1
C1=1.0/3.0
C2=1.0/6.0
C3=1.0/8.0
C4=3.0/8.0
C5=1.0/2.0
C6=3.0/2.0
C7=2.0/3.0
IPASS=1
15     DO 5 J=1,N
20     V(3,J)=V(1,J)-START(J)
5      CONTINUE
ZE=SZ
DO 55 I=1,5
CALL RHS(ZE,SLOPE,N,V)
DO 6 J=1,N
V(2,J)=SLOPE(J)
6      CONTINUE
GO TO(10,15,20,25,30),I
10     DO 11 J=1,N
V(4,J)=V(2,J)*DZ
30     V(1,J)=V(3,J)+C1*V(4,J)
11     CONTINUE
GO TO 40
15     DO 16 J=1,N
V(1,J)=V(3,J)+C2*V(4,J)+C2*V(2,J)*DZ
35     CONTINUE
GO TO 55
20     DO 21 J=1,N
V(5,J)=V(2,J)*DZ
40     V(1,J)=V(3,J)+C3*V(4,J)+C4*V(5,J)
21     CONTINUE
GO TO 45
25     DO 26 J=1,N
V(6,J)=V(2,J)*DZ
45     V(1,J)=V(3,J)+C5*V(4,J)+C6*V(5,J)+2.0*V(6,J)
26     CONTINUE
GO TO 50
30     DO 31 J=1,N
V(1,J)=V(3,J)+C7*V(4,J)+C7*V(6,J)+C2*V(2,J)*DZ
31     CONTINUE
GO TO 55
40     ZE=SZ-C1*DZ*1.0E-05
45     ZE=SZ-C5*DZ*1.0E-05
50     ZE=SZ-C7*DZ*1.0E-05
55

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GIONEUT 1146  
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GIONEUT 1148  
GIONEUT 1149  
GIONEUT 1150  
GIONEUT 1151

55 CONTINUE  
DO 60 J=1,N  
START(J)=V(1,J)  
60 CONTINUE  
RETURN  
END

60

GIONEUT 1152  
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 GIONEUT 1166  
 GIONEUT 1167  
 GIONEUT 1168

SUBROUTINE RHS(ZE,SLOPE,N,V)  
 C THIS SUBROUTINE COMPUTES THE RIGHT HAND SIDE OF THE ORDINARY  
 C DIFFERENTIAL EQUATION FOR THE VELOCITY AT THE UPPER BOUNDARY.  
 C  
 C DIMENSION V(7,2),SLOPE(2)  
 C  
 C COMMON/RHSIDE/AN,BN,AP,BP,AL,BL  
 C  
 C EF(D1,D2,D3)=D1\*D2\*1.0E+05+D3  
 C  
 C EN=EF(AN,ZE,BN)  
 C EP=EF(AP,ZE,BP)  
 C EL=EF(AL,ZE,BL)  
 C SLOPE(1)=(EP-EL-V(1,1)\*AN)/EN  
 C RETURN  
 C END

```

1      SUBROUTINE TIMER                                G1ONEUT 1169
C      THIS SUBROUTINE CONTROLS THE TIME AND THE TIME STEP. G1ONEUT 1170
C      C      COMMON N(692,30),CONC(424,26),U(692,26),NZERO(692,1),UZERO(692,1) G1ONEUT 1171
C      C      COMMON FORM(692),RENV(692),E(692),F(692),Z(692), G1ONEUT 1172
C      C      DEDY(692),TEMP(692),DTEMZ(692),DELTZ(692),SUNSET(692) G1ONEUT 1173
C      C      COMMON GRAV,COSD,SIND,TIME,CHI,RADIUS,ISPECI,KSPECI,NREAC,K, G1ONEUT 1174
C      C      K2,KMIN1,ITURB,CXINOOB,SCXI,NREAC2 G1ONEUT 1175
C      C      COMMON/TIMES/DAYS,DELT,TMAX,TSET,TRISE G1ONEUT 1176
C      C      COMMON/OUTPUTS/TIMOUT,OPRINT,PRINT G1ONEUT 1177
C      C      COMMON/CONSTAN/PI,RADDEG,DEGRAD,RADSEC,BOLTZ,SIN2I,ATCON G1ONEUT 1178
C      C      COMMON/LOGIC/NIGHT,DAY,JLOOK,RESET,END G1ONEUT 1179
C      C      LOGICAL NIGHT,DAY,JLOOK,RESET,END,PRINT,SET G1ONEUT 1180
C      C      COMMON/ALTIM/ZBOT,ZTOP,TURB,ZTRANS G1ONEUT 1181
C      C      DATA SET/.FALSE./ G1ONEUT 1182
C      C      IF(.NOT. SET) GO TO 1 G1ONEUT 1183
C      C      SET=.FALSE. G1ONEUT 1184
C      C      DELT=IS G1ONEUT 1185
C      C      RESET=.FALSE. G1ONEUT 1186
C      C      TSEC=TIME*DELT G1ONEUT 1187
C      C      THRS=TSEC/3600. G1ONEUT 1188
C      C      IF(TIMOUT.EQ.0.) GO TO 8 G1ONEUT 1189
C      C      IF(THRS.LT.TIMOUT) GO TO 10 G1ONEUT 1190
C      C      IF(THRS.EQ.TIMOUT) GO TO 8 G1ONEUT 1191
C      C      TSEC=TIMOUT*3600 G1ONEUT 1192
C      C      THRS=TIMOUT G1ONEUT 1193
C      C      DELT=TSEC/TIME G1ONEUT 1194
C      C      RESET=.TRUE. G1ONEUT 1195
C      C      PRINT=.TRUE. G1ONEUT 1196
C      C      TIMOUT=TIMOUT+OPRINT G1ONEUT 1197
C      C      IF(.NOT. NIGHT) JLOOK=.TRUE. G1ONEUT 1198
C      C      GO TO 11 G1ONEUT 1199
C      C      10 PRINT=.FALSE. G1ONEUT 1200
C      C      11 OLDMOD=AMOD(TIME,8.64E+04) G1ONEUT 1201
C      C      CHINU=ACOS(COSD*COS(TSEC*RADSEC)+SIND) G1ONEUT 1202
C      C      DETERMINE WHETHER DAY, NIGHT, OR TWILIGHT. G1ONEUT 1203
C      C      IF(NIGHT .AND. CHINU .GT. SUNSET(K)) GO TO 15 G1ONEUT 1204
C      C      IF(NIGHT .AND. CHINU .LT. SUNSET(K)) GO TO 5 G1ONEUT 1205
C      C      IF(DAY .AND. CHINU .LT. SUNSET(1)) GO TO 13 G1ONEUT 1206
C      C      IF(DAY .AND. CHINU .GT. SUNSET(1)) GO TO 9 G1ONEUT 1207
C      C      IF(CHINU .GT. SUNSET(K)) NIGHT=.TRUE. G1ONEUT 1208
C      C      IF(CHINU .LT. SUNSET(1)) DAY=.TRUE. G1ONEUT 1209
C      C      IF(CHINU .GT. SUNSET(1)) DAY=.FALSE. G1ONEUT 1210
C      C      IF(CHINU .LT. SUNSET(1)) DAY=.TRUE. G1ONEUT 1211
C      C      IF(CHINU .GT. SUNSET(1)) DAY=.FALSE. G1ONEUT 1212
C      C      IF(CHINU .LT. SUNSET(1)) DAY=.TRUE. G1ONEUT 1213
C      C      IF(CHINU .GT. SUNSET(1)) DAY=.FALSE. G1ONEUT 1214
C      C      IF(CHINU .LT. SUNSET(1)) DAY=.TRUE. G1ONEUT 1215
C      C      IF(CHINU .GT. SUNSET(1)) DAY=.FALSE. G1ONEUT 1216
C      C      IF(CHINU .LT. SUNSET(1)) DAY=.TRUE. G1ONEUT 1217
C      C      IF(CHINU .GT. SUNSET(1)) DAY=.FALSE. G1ONEUT 1218
C      C      IF(CHINU .LT. SUNSET(1)) DAY=.TRUE. G1ONEUT 1219
C      C      IF(CHINU .GT. SUNSET(1)) DAY=.FALSE. G1ONEUT 1220
C      C      IF(CHINU .LT. SUNSET(1)) DAY=.TRUE. G1ONEUT 1221
C      C      IF(CHINU .GT. SUNSET(1)) DAY=.FALSE. G1ONEUT 1222
C      C      IF(CHINU .LT. SUNSET(1)) DAY=.TRUE. G1ONEUT 1223
C      C      IF(CHINU .GT. SUNSET(1)) DAY=.FALSE. G1ONEUT 1224
C      C      IF(CHINU .LT. SUNSET(1)) DAY=.TRUE. G1ONEUT 1225

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60	C	FIND ALTITUDE OF DAY-NIGHT TRANSITION.	GIONEUT 1226
	C	IF (DAY .OR. NIGHT) GO TO 26	GIONEUT 1227
		DO 6 J=1,K	GIONEUT 1228
		IF (CHINU .LE. SUNSET(J)) GO TO 7	GIONEUT 1229
6		CONTINUE	GIONEUT 1230
7		ZTRANS=1	GIONEUT 1231
65		GO TO 26	GIONEUT 1232
	C		GIONEUT 1233
	C	RESET THE TIME STEP SO THAT THE NEXT TIME INCREMENT WILL BEGIN	GIONEUT 1234
	C	EXACTLY AT SUNRISE AT THE UPPER BOUNDARY.	GIONEUT 1235
	C		GIONEUT 1236
70	5	DEL=TRISE-OLDMOD	GIONEUT 1237
		TSEC=TIME+DEL	GIONEUT 1238
		CHINU=SUNSET(K)	GIONEUT 1239
		SET=.TRUE.	GIONEUT 1240
		NIGHT=.FALSE.	GIONEUT 1241
75		GO TO 13	GIONEUT 1242
	C		GIONEUT 1243
	C	RESET THE TIME STEP SO THAT THE NEXT TIME INCREMENT WILL BEGIN	GIONEUT 1244
	C	EXACTLY AT SUNSET AT THE LOWER BOUNDARY.	GIONEUT 1245
	C		GIONEUT 1246
80	9	DEL=TSSET-OLDMOD	GIONEUT 1247
		TSEC=TIME+DEL	GIONEUT 1248
		CHINU=SUNSET(1)	GIONEUT 1249
		SET=.TRUE.	GIONEUT 1250
		DAYS=.FALSE.	GIONEUT 1251
85	13	ZTRANS=50.	GIONEUT 1252
		GO TO 26	GIONEUT 1253
	15	ZTRANS=400.	GIONEUT 1254
	26	CH1=CHINU	GIONEUT 1255
		TIME=TSEC	GIONEUT 1256
90		RETURN	GIONEUT 1257
		END	GIONEUT 1258
			GIONEUT 1259

[illegible]

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1111 IF (J.EQ.1) N(J,I+20)=DEN
1112 IF (J.GT.3) DEN=1.00E+05
1113 N(J,I)
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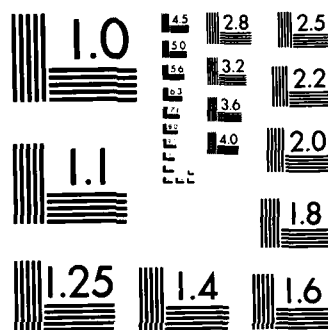
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115	81	FORMAT(*, FAILURE AT ALTITUDE*, OPFB.2.,* FOR SPECIES*, A10, 1P2E13.5) END=.TRUE. RETURN CONTINUE	GIONEUT 1374 GIONEUT 1375 GIONEUT 1376 GIONEUT 1377 GIONEUT 1378 GIONEUT 1379 GIONEUT 1380 GIONEUT 1381 GIONEUT 1382 GIONEUT 1383 GIONEUT 1384 GIONEUT 1385 GIONEUT 1386 GIONEUT 1387 GIONEUT 1388 GIONEUT 1389 GIONEUT 1390 GIONEUT 1391 GIONEUT 1392 GIONEUT 1393 GIONEUT 1394 GIONEUT 1395 GIONEUT 1396 GIONEUT 1397 GIONEUT 1398 GIONEUT 1399 GIONEUT 1400 GIONEUT 1401 GIONEUT 1402 GIONEUT 1403 GIONEUT 1404 GIONEUT 1405 GIONEUT 1406 GIONEUT 1407 GIONEUT 1408 GIONEUT 1409 GIONEUT 1410 GIONEUT 1411 GIONEUT 1412 GIONEUT 1413 GIONEUT 1414
120	45 C C	COMPUTE THE MAJOR POSITIVE IONS AND ELECTRONS ABOVE 120 KM.  KB=K2+1 CALL MOVLEV(OLDN(1,28),E,K) CALL MOVLEV(OLDN(1,29),F,K) DO 105 J=KB,K DO 100 I=1,500 DO 110 I=1,2 H(I)=N(J,I+27) CALL CHEM(I+27,J) IF(I.EQ.1) DENS=E(J) IF(I.EQ.2) DENS=F(J) H(I+3)=DENS+DELT*FORM(J)/((1.0+DELT*REMV(J)) CONTINUE DO 91 I=1,2 N(J,I+27)=H(I+3) CONTINUE DO 95 I=1,2 IF(H(I).EQ.0.) GO TO 95 IF(ABS(1.0-(N(J,I+27)/H(I))) .GT. 0.1) GO TO 100 CONTINUE GO TO 105 CONTINUE CONTINUE DO 55 J=KB,K SUMP=0. DO 50 I=1,5 SUMP=SUMP+N(J,I) CONTINUE DO 51 I=28,29 SUMP=SUMP+N(J,I) CONTINUE N(J,30)=SUMP CONTINUE RETURN END	
125			
130			
135	110 91		
140	95		
145	100 105		
150	50 51		
155	55		

[illegible]



AD-A157 122 A COMPUTER CODE FOR A ONE-DIMENSIONAL DYNAMIC MODEL OF THE MESOSPHERES AND (U) AIR FORCE GEOPHYSICS LAB 3/3  
UNCLASSIFIED HANSCOM AFB MA T J KENESHA ET AL. 07 MAR 84  
AFGL-TR-84-0183 F/G 4/1 NL



MICROCOPY RESOLUTION TEST CHART  
NBS-1963-A

60 RMOV=(Y(8)\*(+K(45)+K(46)))+Y(23)\*(+K(47)+K(48))+K(49)\*Y(18))  
 FARM=(+K(191)\*Y(21))  
 GO TO 100  
 3 CONTINUE  
 65 RMOV=(+K(40)\*Y(11)+K(127)\*Y(25)+K(153)\*Y(30)+K(168)\*Y(23)+K(169)\*Y(18))  
 FARM=(+K(41)\*Y(1)+K(185)+K(211))+Y(8)\*(+K(45)\*Y(2)+K(209))  
 GO TO 100  
 4 CONTINUE  
 70 RMOV=(+K(33)\*Y(18)+K(34)\*Y(16)+K(35)\*Y(19)+K(152)\*Y(30)+K(162)\*Y(8)+Y(57))  
 FARM=(Y(8)\*(+K(43)+K(44))+K(46)\*Y(2)+K(126)\*Y(29)+K(167)\*Y(2)+K(169)\*Y(3)+K(186)+K(214))+Y(39)\*(+K(36)\*Y(7)+K(163)\*Y(57)+K(16)+Y(20))+K(127)\*Y(3)\*Y(25)+K(207)\*Y(20))  
 GO TO 100  
 5 CONTINUE  
 75 RMOV=(Y(30)\*(+K(150)+K(151))+K(165)\*Y(25)\*Y(23)+K(166)\*Y(13)\*Y(57))  
 FARM=(Y(18)\*(+K(33)\*Y(4)+K(50)\*Y(40)+K(188))+Y(7)\*(+K(38)\*Y(28)+K(139)\*Y(28))+K(34)\*Y(4)\*Y(16)+K(42)\*Y(6)\*Y(8)+K(168)\*Y(3)\*Y(23))  
 GO TO 100  
 6 CONTINUE  
 80 RMOV=(Y(8)\*(+K(42)+K(43)+K(44))+K(154)\*Y(30))  
 FARM=(Y(2)\*(+K(47)\*Y(23)+K(48)\*Y(18))+K(189)\*Y(16)+K(208)\*Y(23))  
 GO TO 100  
 7 CONTINUE  
 85 RMOV=(Y(57)\*Y(7)\*(+K(128)+K(128))+K(129)\*Y(8)+K(139)\*Y(16)+K(143)+Y(18)+K(148)\*Y(26))+Y(14)\*(+K(132)+K(133))+Y(28)\*(+K(38)+K(39))+Y(32)\*(+K(100)+K(101))+Y(34)\*(+K(107)+K(108))+K(2)\*Y(10)+K(3)\*Y(12)+K(4)\*Y(19)+K(20)\*Y(55)+K(31)\*Y(30)+K(36)\*Y(39)+K(41)\*Y(1)+K(97)\*Y(131)+K(106)\*Y(33)+K(111)\*Y(37)+K(115)\*Y(38)+K(121)\*Y(36)+K(130)\*Y(19)+K(131)\*Y(15)+K(185)+K(206)+K(211)+K(212))  
 FARM=(Y(8)\*(+K(14)\*Y(17)+K(42)\*Y(6)+K(45)\*Y(2)+K(126)\*Y(29)+K(137)+Y(16)+K(169)\*Y(3)+K(192)+K(192)+K(193)+K(209)+K(210))+Y(30)\*Y(4)+Y(15)\*(+K(152)+K(152))+Y(15)\*(+K(150)+K(151))+K(153)\*Y(3)+K(156)\*Y(40))+Y(16)\*(+K(9)+Y(19)+K(34)\*Y(4)+K(138)\*Y(18))+Y(9)\*(+K(98)\*Y(31)+K(1194))+Y(18)\*(+K(49)\*Y(2)+K(199))+K(12)\*Y(10)+K(16)\*Y(27)\*Y(57)+K(40)\*Y(3)\*Y(11)+K(96)\*Y(31)+K(120)\*Y(36)+K(125)\*Y(29)\*Y(23)+K(2104)\*Y(25))  
 GO TO 100  
 8 CONTINUE  
 100 RMOV=(Y(8)\*Y(30)\*(+K(160)+K(160))+Y(31)\*(+K(179)+K(179))+Y(32)\*Y(180)+K(180))+Y(6)\*(+K(42)+K(43)+K(44))+Y(57)\*(+K(129)\*Y(7)+K(1316)\*Y(11)+K(162)\*Y(4))+Y(2)\*(+K(45)+K(46))+K(14)\*Y(17)+K(32)\*Y(23)+Y(30)+K(126)\*Y(29)+K(137)\*Y(16)+K(167)\*Y(28)+K(169)\*Y(3)+K(186)+K(1192)+K(193)+K(209)+K(210)+K(214))  
 FARM=(Y(7)\*Y(34)\*(+K(107)+K(108)+K(108))+Y(9)\*(+K(130)+K(130))+K(12)\*Y(10)+K(3)\*Y(12)+K(4)\*Y(19)+K(97)\*Y(31)+K(101)\*Y(32)+K(106)\*Y(3)+K(115)\*Y(38)+K(121)\*Y(36)+K(128)\*Y(7)\*Y(57)+K(133)\*Y(14))+Y(9)\*Y(12)\*(+K(145)+K(145))+K(7)\*Y(11)+K(8)\*Y(16)+K(102)\*Y(32)+K(116)\*Y(38)+K(119)\*Y(35)+K(124)\*Y(31)+K(140)\*Y(10)+K(142)\*Y(18)+K(161)\*Y(130)+K(194))+Y(20)\*(+K(132)\*Y(32)+K(103)+K(103))+Y(39)\*(+K(164)+K(164))+K(18)\*Y(57)+K(19))+Y(12)\*(+K(5)\*Y(11)+K(13)\*Y(10)+K(144)\*Y(12)+K(198))+Y(8)\*(+K(160)+Y(30)+K(179)\*Y(31)+K(180)\*Y(32))+Y(13)\*Y(50)\*(+K(53)+K(54))+K(37)\*Y(39))+Y(4)\*(+K(33)\*Y(18)+K(35)\*Y(19))+Y(25)\*(+K(109)+Y(34)+K(182)\*Y(33))+Y(57)\*(+K(163)+Y(39)+K(183)\*Y(3)+K(111)\*Y(16))+Y(19)+K(99)\*Y(32)+K(105)\*Y(33)+K(114)\*Y(38)+K(20514))

115 1-Y(56))  
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9 CONTINUE  
RMOV=(Y(31)\*+K(98)+K(124))+K(7)\*Y(11)+K(8)\*Y(16)+K(102)\*Y(32)+K(116)\*Y(38)+K(119)\*Y(35)+K(130)\*Y(7)+K(140)\*Y(10)+K(142)\*Y(18)+K(145)  
1-Y(12)+K(161)\*Y(30)+K(194)+K(195))  
FARM=(Y(7)\*+K(36)\*Y(39)+K(100)\*Y(32)+K(129)\*Y(8)\*Y(57))+K(104)\*Y(133))  
GO TO 100  
10 CONTINUE  
RMOV=(Y(10)\*+K(12)+K(12))+K(2)\*Y(7)+K(13)\*Y(12)+K(21)\*Y(55)+K(140)  
1)\*Y(9)+K(141)\*Y(14)+K(147)\*Y(26))  
FARM=(Y(37)\*+K(64)\*Y(41)+K(68)\*Y(42)+K(72)\*Y(43)+K(76)\*Y(44)+K(80)  
1)\*Y(45)+K(92)\*Y(48)+K(94)\*Y(49))+Y(30)\*+K(24)\*Y(41)+K(25)\*Y(42)+K(26)\*Y(43)+K(27)\*Y(44)+K(28)\*Y(45)+K(29)\*Y(47))+Y(11)\*Y(12)\*+K(6)  
1)+K(6))+K(7)\*Y(9)+K(135)\*Y(14)+K(146)\*Y(19))+Y(13)\*Y(27)\*+K(15)+  
1)+K(15))+K(54)\*Y(50)+K(61)\*Y(47)+K(196))+Y(36)\*+K(63)\*Y(41)+K(67)\*Y(42)+K(71)\*Y(43)+K(75)\*Y(44)+K(79)\*Y(45))+Y(7)\*+K(3)\*Y(12)+K(20)\*  
1)+Y(55)+K(131)\*Y(15)+K(132)\*Y(14))+Y(14)\*+K(197)+K(197))+K(17)\*Y(27)  
1)\*Y(15)+K(145)\*Y(12)\*Y(9)+K(202)\*Y(55))  
GO TO 100  
11 CONTINUE  
RMOV=(Y(12)\*+K(5)+K(6))+Y(14)\*+K(134)+K(135))+K(7)\*Y(9)+K(40)\*Y(13)+K(136)\*Y(17)+K(146)\*Y(19)+K(190))  
FARM=(Y(35)\*+K(62)\*Y(41)+K(66)\*Y(42)+K(70)\*Y(43)+K(74)\*Y(44)+K(78)  
1)\*Y(45))+Y(7)\*+K(12)\*Y(10)+K(41)\*Y(11)+K(131)\*Y(15))+Y(30)\*+K(29)\*  
1)+K(30)\*Y(49)+K(155)\*Y(11)+K(17)\*Y(27)\*Y(15)+K(147)\*Y(26)\*Y(10)  
1)+K(196)\*Y(13)+K(198)\*Y(12))  
GO TO 100  
12 CONTINUE  
RMOV=(Y(11)\*+K(5)+K(6))+Y(12)\*+K(144)+K(144))+K(3)\*Y(7)+K(13)\*Y(110)+K(145)\*Y(9)+K(198))  
FARM=(Y(38)\*+K(69)\*Y(42)+K(73)\*Y(43)+K(77)\*Y(44)+K(81)\*Y(45)+K(93)  
1)\*Y(48)+K(95)\*Y(49))+Y(14)\*+K(132)\*Y(7)+K(134)\*Y(11)+K(141)\*Y(10)  
1)+K(65)\*Y(42)\*Y(32)+K(136)\*Y(11)\*Y(8)\*Y(57)+K(140)\*Y(10)\*Y(9))  
GO TO 100  
13 CONTINUE  
RMOV=(Y(57)\*+K(52)\*Y(44)+K(166)\*Y(5)+K(170)\*Y(41)+K(172)\*Y(42)+K(1173)\*Y(43)+K(177)\*Y(51)+K(178)\*Y(52))+Y(48)\*+K(58)\*Y(23)+K(60))+Y(150)\*+K(53)+K(54))+K(15)\*Y(27)+K(37)\*Y(39)+K(55)\*Y(53)+K(56)\*Y(54)  
1)+K(59)\*Y(49)+K(61)\*Y(47)+K(196))  
FARM=(Y(30)\*+K(52)\*+K(158)+K(158))+K(25)\*Y(42)+K(29)\*Y(47)+K(157)  
1)\*Y(51))+Y(10)\*+K(12)\*Y(10)+K(13)\*Y(12)+K(21)\*Y(55)+K(141)\*Y(14))+  
1)+K(64)\*Y(41)+K(84)\*Y(51)+K(92)\*Y(48))+Y(57)\*+K(174)\*Y(43)+  
1)+K(175)\*Y(44)+K(176)\*Y(45))+Y(14)\*+K(133)\*Y(7)+K(135)\*Y(11))+Y(32)  
1)\*+K(65)\*Y(42)+K(65)\*Y(42))+Y(35)\*+K(62)\*Y(41)+K(82)\*Y(51))+Y(36)  
1)\*+K(63)\*Y(41)+K(83)\*Y(51))+K(93)\*Y(48)\*Y(38))  
FARM=FARM+2\*Y(42)\*+K(66)\*Y(35)+K(67)\*Y(36)+K(68)\*Y(37)  
1)+K(69)\*Y(38))+Y(49)\*+K(30)\*Y(30)+K(94)\*Y(37)+K(95)\*Y(238))+Y(52)\*+K(85)\*Y(35)+K(86)\*Y(36)+K(87)\*Y(37))  
3)+K(26)\*Y(43)\*Y(30))+3\*Y(43)\*+K(70)\*Y(35)+K(71)\*  
4)+K(36)+K(72)\*Y(37)+K(73)\*Y(38))+Y(53)\*+K(88)\*Y(35)  
5)+K(89)\*Y(36)+K(90)\*Y(37)+K(159)\*Y(30)+K(27)\*Y(44)  
6)\*Y(30))+4\*Y(44)\*+K(74)\*Y(35)+K(75)\*Y(36)+K(76)\*Y(37)+K(77)\*Y(39))+K(128)\*Y(45)\*Y(30))+5\*Y(45)\*+  
6)+K(78)\*Y(35)+K(79)\*Y(36)+K(80)\*Y(37)+K(81)\*Y(38))  
GO TO 100

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14 CONTINUE
RMOV=(Y(7)*(+K(132)+K(133))+Y(11)*(+K(134)+K(135))+K(141)*Y(10)+K(
1197))
FARM=(+K(91)*Y(48)*Y(36)+K(144)*Y(12)*Y(12))
GO TO 100
175
15 CONTINUE
RMOV=(+K(17)*Y(27)+K(131)*Y(7))
FARM=(Y(30)*(+K(24)*Y(41)+K(25)*Y(42)+K(26)*Y(43)+K(27)*Y(44)+K(28
1)*Y(45))+Y(11)*(+K(5)*Y(12)+K(134)*Y(14)))
GO TO 100
180
16 CONTINUE
RMOV=(Y(19)*(+K(9)+K(10)+K(11))+K(8)*Y(9)+K(34)*Y(4)+K(137)*Y(8)+K
1(138)*Y(18)+K(139)*Y(7)*Y(57)+K(189))
FARM=(Y(30)*(+K(22)+K(22))+K(149)*Y(17)+K(150)*Y(5)+K(154)*
1Y(6))+Y(23)*(+K(47)*Y(2)+K(168)*Y(3)+K(208)+K(215))+Y(7)*(+K(1)*Y(
117)+K(38)*Y(28))+K(43)*Y(6)*Y(8)+K(199)*Y(18))
GO TO 100
185
17 CONTINUE
RMOV=(+K(1)*Y(7)+K(14)*Y(8)+K(149)*Y(30))
FARM=(Y(28)*Y(30)*(+K(23)+K(23))+K(39)*Y(7))+K(44)*Y(6)*Y(8)+K(15
11)*Y(5)+Y(30)+K(215)*Y(23))
GO TO 100
190
18 CONTINUE
RMOV=(+K(33)*Y(4)+K(49)*Y(2)+K(50)*Y(40)+K(117)*Y(38)+K(122)*Y(56)
1+K(138)*Y(16)+K(142)*Y(9)+K(143)*Y(7)*Y(57)+K(184)*Y(37)+K(188)+K(
1199))
FARM=(Y(16)*Y(19)*(+K(10)+K(10))+K(8)*Y(9)+K(137)*Y(8)+K(139)*Y(7
1)*Y(57))+Y(30)*(+K(156)*Y(40)+K(157)*Y(51)+K(158)*Y(52)+K(159)*Y(5
13))+Y(19)*(+K(4)*Y(7)+K(146)*Y(11)+K(200))+Y(35)*(+K(82)*Y(51)+K(8
15)*Y(52)+K(88)*Y(53))+K(14)*Y(17)+Y(8)+K(202)*Y(55)+K(205)*Y(56))
GO TO 100
200
19 CONTINUE
RMOV=(Y(16)*(+K(9)+K(10)+K(11))+K(4)*Y(7)+K(35)*Y(4)+K(112)*Y(37)+
1K(146)*Y(11)+K(200))
FARM=(Y(36)*Y(51)*(+K(83)+K(83))+Y(52)*(+K(86)+K(86))+Y(53)*(+K(8
19)+K(89))+K(63)*Y(41)+K(67)*Y(42)+K(71)*Y(43)+K(75)*Y(44)+K(79)*Y(
145))+Y(35)*(+K(62)*Y(41)+K(66)*Y(42)+K(70)*Y(43)+K(74)*Y(44)+K(78)
1)+Y(45)+K(82)*Y(51)+K(85)*Y(52)+K(88)*Y(53)+K(118))+Y(18)*Y(56)*Y(
1K(122)+K(122))+K(50)*Y(40)+K(142)*Y(9)+K(143)*Y(7)*Y(57)+Y(37)*Y(
1K(84)*Y(51)+K(87)*Y(52)+K(90)*Y(53))+Y(55)*Y(20)+Y(7)+K(21)*Y(10
1)))
GO TO 100
205
20 CONTINUE
RMOV=(+K(18)*Y(57)+K(19)+K(103)*Y(32)+K(164)*Y(39)+K(207))
FARM=(+K(195)*Y(9))
GO TO 100
210
21 CONTINUE
RMOV=(+K(191))
FARM=(Y(2)*Y(8)*(+K(45)+K(46))+Y(23)*Y(47)+K(48)+K(49)*Y(18)))
GO TO 100
215
22 CONTINUE
RMOV=0.
FARM=0.
GO TO 100
220
23 CONTINUE
RMOV=(Y(2)*Y(47)+K(48)*Y(23)*Y(171)+Y(41)+K(171)*Y(41))+K(125
1)*Y(29)+K(168)*Y(3)+K(187)+K(208)+K(213)+K(215))
GO TO 100
225

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230 FARM=(Y(16)\*(+K(11)\*Y(19)+K(138)\*Y(18))+K(157)\*Y(46)\*Y(25)+K(167)\*Y  
1(28)\*Y(8)+K(171)\*Y(41)\*Y(23)+K(201)\*Y(24))  
GO TO 100  
24 CONTINUE  
235 RMOV=(+K(201))  
FARM=(+K(9)\*Y(16)+Y(19))  
GO TO 100  
25 CONTINUE  
RMOV=(+K(51)\*Y(42)+Y(57)+K(57)\*Y(46)+K(109)\*Y(34)+K(127)\*Y(3)+K(16  
15)\*Y(5)+Y(23)+K(181)\*Y(32)\*Y(8)+K(182)\*Y(33)+K(203)+K(204))  
FARM=(Y(37)\*(+K(64)\*Y(41)+K(68)\*Y(42)+K(72)\*Y(43)+K(76)\*Y(44)+K(80  
1)\*Y(45)+K(84)\*Y(51)+K(87)\*Y(52)+K(90)\*Y(53)+K(110)+K(111)\*Y(7)+K(1  
12)\*Y(19)+K(184)\*Y(18)+Y(38)\*(+K(69)\*Y(42)+K(73)\*Y(43)+K(77)\*Y(44  
1)+K(81)\*Y(45)+K(113)+K(114)+K(116)+Y(9)+K(117)\*Y(18))+Y(13)\*(+K(56  
1)\*Y(54)+K(59)\*Y(49)+K(60)\*Y(48))+Y(26)\*(+K(147)\*Y(10)+K(148)\*Y(7)\*  
1Y(57))+K(30)\*Y(45)\*Y(30)+K(91)\*Y(48)\*Y(36))  
FARM=FARM+2.0\*(Y(37)\*K(92)\*Y(48)+K(54)\*Y(49))+Y(38)\*(  
1K(93)\*Y(48)+K(95)\*Y(49))  
GO TO 100  
26 CONTINUE  
RMOV=(+K(147)\*Y(10)+K(148)\*Y(7)\*Y(57))  
FARM=(Y(25)\*(+K(127)\*Y(3)+K(203)+K(204)))  
GO TO 100  
27 CONTINUE  
RMOV=(+K(15)\*Y(13)+K(16)\*Y(57)+K(17)\*Y(15))  
FARM=(+K(193)\*Y(8)+K(195)\*Y(9)+K(200)\*Y(19)+K(201)\*Y(24)+K(203)\*Y(  
125))  
GO TO 100  
28 CONTINUE  
RMOV=(Y(7)\*(+K(38)+K(39))+Y(30)\*(+K(22)+K(23))+K(167)\*Y(8))  
FARM=(Y(23)\*(+K(48)\*Y(2)+K(125)\*Y(29)+K(187)+K(213)))  
GO TO 100  
29 CONTINUE  
RMOV=(+K(125)\*Y(23)+K(126)\*Y(8))  
FARM=(Y(7)\*(+K(206)+K(212))+K(210)\*Y(8))  
GO TO 100  
30 CONTINUE  
RMOV=(Y(5)\*(+K(150)+K(151))+Y(18)\*(+K(32)\*Y(23)+K(160)\*Y(8))+Y(28)\*  
1(+K(22)+K(23))+K(24)\*Y(41)+K(25)\*Y(42)+K(26)\*Y(43)+K(27)\*Y(44)+K(2  
18)\*Y(45)+K(29)\*Y(47)+K(30)\*Y(49)+K(31)\*Y(7)+K(152)\*Y(4)+K(153)\*Y(3  
1)+K(154)\*Y(6)+K(155)\*Y(1)+K(156)\*Y(40)+K(157)\*Y(51)+K(158)\*Y(52)+K  
1(159)\*Y(53)+K(161)\*Y(9))  
FARM=(Y(7)\*(+K(97)\*Y(31)+K(100)\*Y(32)+K(185)+K(206))+Y(20)\*(+K(103  
1)\*Y(32)+K(207))+Y(23)\*K(187)+K(96)\*Y(31)+K(99)\*Y(32)+K(1  
104)\*Y(33)+K(114)\*Y(38)+K(118)\*Y(35)+K(123)\*Y(36)+K(186)\*Y(8)+K(188  
1)\*Y(18)+K(189)\*Y(16)+K(190)\*Y(11)+K(191)\*Y(21))  
FARM=FARM+Y(23)\*K(208)+K(213))+Y(8)\*K(209)+K(210)+K(214))  
1+Y(7)\*K(211)+K(212))  
GO TO 100  
31 CONTINUE  
RMOV=(Y(9)\*(+K(98)+K(124))+K(96)+K(97)\*Y(7)+K(179)\*Y(8)\*Y(8))  
FARM=(Y(7)\*(+K(31)\*Y(30)+K(101)\*Y(32)+K(108)+Y(34))+K(105)\*Y(33)+K  
1(110)\*Y(37)+K(161)\*Y(9)\*Y(30))  
GO TO 100  
32 CONTINUE  
RMOV=(Y(7)\*(+K(103)+K(101))+Y(8)\*(+K(180)\*Y(8)+K(181)\*Y(25))+K(65)  
1+Y(42)+K(99)+K(102)\*Y(9)+K(103)+Y(20))  
GO TO 100

FARM=(Y(7)\*(-K(106)\*Y(33)+K(111)\*Y(37))+Y(8)\*(-K(32)\*Y(23)+  
 1K(160)\*Y(8)))+K(113)\*Y(38)+K(124)\*Y(31)\*Y(9)+K(183)\*Y(34)\*Y(57))  
 GO TO 100  
 33 CONTINUE  
 RMOV=(-K(104)+K(105)+K(106)\*Y(7)+K(182)\*Y(25))  
 FARM=(Y(9)\*(-K(98)\*Y(31)+K(102)\*Y(32)+K(116)\*Y(38))+K(107)\*Y(34)\*Y  
 1(7)+K(179)\*Y(31)\*Y(8)\*Y(8))  
 GO TO 100  
 34 CONTINUE  
 RMOV=(Y(7)\*(-K(107)+K(108))+K(109)\*Y(25)+K(183)\*Y(57))  
 FARM=(-K(180)\*Y(32)\*Y(8)\*Y(8))  
 GO TO 100  
 35 CONTINUE  
 RMOV=(-K(62)\*Y(41)+K(66)\*Y(42)+K(70)\*Y(43)+K(74)\*Y(44)+K(78)\*Y(45)  
 1+K(82)\*Y(51)+K(85)\*Y(52)+K(88)\*Y(53)+K(118)+K(119)\*Y(9))  
 FARM=(Y(36)\*(-K(120)+K(121)\*Y(7)+K(184)\*Y(37)\*Y(18))  
 GO TO 100  
 36 CONTINUE  
 RMOV=(-K(63)\*Y(41)+K(67)\*Y(42)+K(71)\*Y(43)+K(75)\*Y(44)+K(79)\*Y(45)  
 1+K(83)\*Y(51)+K(86)\*Y(52)+K(89)\*Y(53)+K(91)\*Y(48)+K(120)+K(121)\*Y(7  
 1)+K(123))  
 FARM=(-K(112)\*Y(37)\*Y(19)+K(117)\*Y(38)\*Y(18)+K(119)\*Y(35)\*Y(9))  
 GO TO 100  
 37 CONTINUE  
 RMOV=(-K(64)\*Y(41)+K(68)\*Y(42)+K(72)\*Y(43)+K(76)\*Y(44)+K(80)\*Y(45)  
 1+K(84)\*Y(51)+K(87)\*Y(52)+K(90)\*Y(53)+K(92)\*Y(48)+K(94)\*Y(49)+K(110  
 1)+K(111)\*Y(7)+K(112)\*Y(19)+K(184)\*Y(18))  
 FARM=(-K(115)\*Y(38)\*Y(7)+K(182)\*Y(33)\*Y(25))  
 GO TO 100  
 38 CONTINUE  
 RMOV=(-K(69)\*Y(42)+K(73)\*Y(43)+K(77)\*Y(44)+K(81)\*Y(45)+K(93)\*Y(48)  
 1+K(95)\*Y(49)+K(113)+K(114)+K(115)\*Y(7)+K(116)\*Y(9)+K(117)\*Y(18))  
 FARM=(Y(25)\*(-K(109)\*Y(34)+K(181)\*Y(32)\*Y(8))  
 GO TO 100  
 39 CONTINUE  
 RMOV=(-K(36)\*Y(7)+K(37)\*Y(13)+K(163)\*Y(57)+K(164)\*Y(20))  
 FARM=(-K(162)\*Y(4)\*Y(8)\*Y(57))  
 GO TO 100  
 40 CONTINUE  
 RMOV=(-K(50)\*Y(18)+K(156)\*Y(30))  
 FARM=(-K(35)\*Y(4)\*Y(19))  
 GO TO 100  
 41 CONTINUE  
 RMOV=(-K(24)\*Y(30)+K(62)\*Y(35)+K(63)\*Y(36)+K(64)\*Y(37)+K(170)\*Y(13  
 1)\*Y(57)+K(171)\*Y(23)\*Y(23))  
 FARM=(-K(54)\*Y(50)\*Y(13))  
 GO TO 100  
 42 CONTINUE  
 RMOV=(Y(57)\*(-K(51)\*Y(25)+K(172)\*Y(13)+K(25)\*Y(30)+K(65)\*Y(32)+K(1  
 66)\*Y(35)+K(67)\*Y(36)+K(68)\*Y(37)+K(69)\*Y(38))  
 FARM=(Y(13)\*(-K(60)\*Y(48)+K(61)\*Y(47)+K(170)\*Y(41)\*Y(57))+K(174)\*Y  
 1(43)\*Y(57))  
 GO TO 100  
 43 CONTINUE  
 RMOV=(Y(57)\*(-K(173)+Y(13)+K(174))+K(26)\*Y(30)+K(70)\*Y(35)+K(71)\*Y  
 1(36)+K(72)\*Y(37)+K(73)\*Y(36))  
 FARM=(Y(13)\*(-K(55)\*Y(53)+K(59)\*Y(49)+K(172)\*Y(42)\*Y(57))+K(175)\*Y

345	1(44)*Y(57)) GO TO 100 44 CONTINUE RMOV=(Y(57)*(+K(52)*Y(13)+K(175))+K(27)*Y(30)+K(74)*Y(35)+K(75)*Y(136)+K(76)*Y(37)+K(77)*Y(38)) FARM=(Y(57)*(+K(173)*Y(43)+K(176)*Y(45))) GO TO 100	GIONEUT 1757 GIONEUT 1758 GIONEUT 1759 GIONEUT 1760 GIONEUT 1761 GIONEUT 1762 GIONEUT 1763 GIONEUT 1764 GIONEUT 1765 GIONEUT 1766 GIONEUT 1767 GIONEUT 1768 GIONEUT 1769 GIONEUT 1770 GIONEUT 1771 GIONEUT 1772 GIONEUT 1773 GIONEUT 1774 GIONEUT 1775 GIONEUT 1776 GIONEUT 1777 GIONEUT 1778 GIONEUT 1779 GIONEUT 1780 GIONEUT 1781 GIONEUT 1782 GIONEUT 1783 GIONEUT 1784 GIONEUT 1785 GIONEUT 1786 GIONEUT 1787 GIONEUT 1788 GIONEUT 1789 GIONEUT 1790 GIONEUT 1791 GIONEUT 1792 GIONEUT 1793 GIONEUT 1794 GIONEUT 1795 GIONEUT 1796 GIONEUT 1797 GIONEUT 1798 GIONEUT 1799 GIONEUT 1800 GIONEUT 1801 GIONEUT 1802 GIONEUT 1803 GIONEUT 1804 GIONEUT 1805 GIONEUT 1806 GIONEUT 1807 GIONEUT 1808 GIONEUT 1809 GIONEUT 1810 GIONEUT 1811 GIONEUT 1812 GIONEUT 1813
350	45 CONTINUE RMOV=(+K(28)*Y(30)+K(78)*Y(35)+K(79)*Y(36)+K(80)*Y(37)+K(81)*Y(38)+K(176)*Y(57)) FARM=(+K(52)*Y(44)+Y(13)*Y(57)) GO TO 100	
355	46 CONTINUE RMOV=(+K(57)*Y(25)) FARM=(+K(171)*Y(41)*Y(23)*Y(23)) GO TO 100	
360	47 CONTINUE RMOV=(+K(29)*Y(30)+K(61)*Y(13)) FARM=(+K(53)*Y(50)*Y(13)) GO TO 100	
365	48 CONTINUE RMOV=(Y(13)*(+K(58)*Y(23)+K(60))+K(91)*Y(36)+K(92)*Y(37)+K(93)*Y(18)) FARM=(+K(57)*Y(46)*Y(25)) GO TO 100	
370	49 CONTINUE RMOV=(+K(30)*Y(30)+K(59)*Y(13)+K(94)*Y(37)+K(95)*Y(38)) FARM=(+K(51)*Y(42)*Y(25)*Y(57)+K(58)*Y(48)*Y(13)*Y(23)) GO TO 100	
375	50 CONTINUE RMOV=(+K(53)*Y(13)+K(54)*Y(13)) FARM=(+K(37)*Y(39)*Y(13)) GO TO 100	
380	51 CONTINUE RMOV=(+K(82)*Y(35)+K(83)*Y(36)+K(84)*Y(37)+K(157)*Y(30)+K(177)*Y(13)*Y(57)) FARM=(Y(13)*(+K(56)*Y(54)+K(166)*Y(5)*Y(57))) GO TO 100	
385	52 CONTINUE RMOV=(+K(85)*Y(35)+K(86)*Y(36)+K(87)*Y(37)+K(158)*Y(30)+K(178)*Y(13)*Y(57)) FARM=(+K(177)*Y(51)*Y(13)*Y(57)) GO TO 100	
390	53 CONTINUE RMOV=(+K(55)*Y(13)+K(88)*Y(35)+K(89)*Y(36)+K(90)*Y(37)+K(159)*Y(30)+K(178)*Y(57)) FARM=(+K(178)*Y(52)*Y(13)*Y(57)) GO TO 100	
395	54 CONTINUE RMOV=(+K(56)*Y(13)) FARM=(+K(165)*Y(5)*Y(25)*Y(23)) GO TO 100	
	55 CONTINUE RMOV=(+K(20)*Y(7)+K(21)*Y(10)+K(202)) FARM=(+K(55)*Y(53)*Y(13)+K(91)*Y(48)*Y(36)) GO TO 100	
	56 CONTINUE	



GIONEUT	1814
GIONEUT	1815
GIONEUT	1816
GIONEUT	1817
GIONEUT	1818
GIONEUT	1819

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RMOV=(+K(122)*Y(18)+K(205))
FARM=(+K(123)*Y(36))
FORM(IALT)=FARM
REMV(IALT)=RMOV
RETURN
END

```

400	100
405	

```

1      SUBROUTINE RATECN(IALT)
C
C      THIS SUBROUTINE COMPUTES THE IONIZATION RATES.  ON THE INITIAL
C      ENTRY IT COMPUTES AND SAVES H*F AT NOON FOR O2, N2, AND O.
C
5      DIMENSION SX(6),QE(6),EX(6),PHI(16),SIGI(16),SIGEFF(16)
C      DIMENSION DISOC(14),XIN(8),YIN(8),ZS(8),CHIS(4)
C
C      COMMON N(692,30),CONC(424,26),U(692,26),NZERO(692),UZERO(692)
C
10     COMMON FORM(692),REMV(692),E(692),F(692),Z(692),
C      2 DEDY(692),TEMP(692),DTEMDZ(692),DELTAZ(692),SUNSET(692)
C
C      COMMON GRAV,COSD,SIND,TIME,CXI,RADIUS,ISPECI,KSPECI,NREAC,K,
C      1 K2,KWIN1,ITURB,CXINDON,SCXI,NREAC2
C
15     COMMON IONS/WAVE(88),FLUX(88),SIGMA(9,88),R(8,4,8)
C
C      COMMON/CONSTAN/PI,RADDEG,DEGRAD,RADSEC,BOLTZ,SIN21,ATCON
C
20     COMMON/RATECON/AK(88),BK(88),CK(88),DK(215),CYMB(6,215)
C
C      COMMON/ATCONS/ATWT(26),MASS(26),THERM(26),SYMBOL(56),POLAR(26)
C
C      COMMON/LOGIC/NIGHT,DAY,JLOOK,RESET,END
C
25     COMMON/COLUM/02COL,03COL,DIS(19,59)
C
C      REAL N2NOON,N,MASS,LYALFA,LYBETA
C
30     COMMON/ALTITUD/ZBOT,ZTOP,ZTURB,ZTRANS
C
C      LOGICAL NIGHT,DAY,JLOOK
C
C      THE FOLLOWING THREE DATA STATEMENTS CONTAIN THE SOLAR FLUX (X10-9)
35     C THE IONIZATION CROSS SECTIONS AND THE EFFECTIVE ABSORPTION CROSS
C      SECTIONS (X10+18) FOR O2(1DG).
C
C      DATA PHI/0.123,0.202,0.18,0.06,0.16,0.208,0.432,0.092,0.626,0.59,
40     1 0.08,0.08,0.11,1.63,2.29,0.13/
C
C      DATA SIGI/2.0,3.0,4.0,3.6,4.0,10.0,4.0,4.0,5.0,3.0,5.0,3.8,
45     1 5.5,5.0,5.0/
C
C      DATA SIGEFF/0.186,0.186,0.04,0.021,1.0,0.1,1.0,0.12,1.0,2.0,0.4,
50     1 0.7,0.2,1.15,1.12,1.0/
C
C      THE FOLLOWING TWO DATA STATEMENTS CONTAIN THE ALTITUDES AND THE
C      SOLAR ZENITH ANGLE ARRAYS CORRESPONDING TO THE INPUT ARRAYS OF
C      THE RATE COEFFICIENTS FOR THE ENERGETIC ELECTRONS.
C
C      DATA ZS/95.,100.,130.,170.,210.,250.,300.,400./
C
C      DATA CHIS/49.77,61.50,76.22,109.7976/
C
55     DATA COSMIC/1.EE-7/
C      DATA IPASS/1/

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 GIONEUT 1875  
 GIONEUT 1876

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C          GRAVCOR(ZZ)=1.0/((1.0+ZZ/RADIUS)**2)
C
60      T1=TEMP(IALT)
      ZZ=Z(IALT)
      T2=T1/300.
      O2COL=0.
      O3COL=0.
      DO 1 J=1,NREAC2
      A1=AK(J)
      B1=BK(J)
      C1=CK(J)
      IF(B1.NE. 0.) A1=A1*(T2**B1)
      IF(C1.NE. 0.) A1=A1*EXP(C1/T1)
      DK(J+NREAC)=A1
1      CONTINUE
      IF(IPASS.NE. 1) GO TO 30
      DO 26 L=1,16
      PHI(L)=PHI(L)*1.0E+09
      SIGI(L)=SIGI(L)*1.0E-18
      SIGEFF(L)=SIGEFF(L)*1.0E-18
26      CONTINUE
      IPASS=2
      DO 5 L=1,8
      DO 5 I=1,4
      DO 5 J=1,8
      IF(R(J,I,L).EQ. 0.) GO TO 3
      R(J,I,L)=ALOG(R(J,I,L))
      GO TO 5
3      R(J,I,L)=-300.
5      CONTINUE
C      SAVE H*F AT NOONTIME FOR O2, O, AND N2.
C
30      GRAVITY=GRAV*GRAVCOR(ZZ)
      T=BOLTZ*TEMP(IALT)/GRAVITY
      DO 20 I=1,3
      IF(I.EQ. 1) F(I)=MASS(8)
      IF(I.EQ. 2) F(I)=MASS(23)
      IF(I.EQ. 3) F(I)=MASS(7)
      SCALE=T/F(I)
      CALL CHAPMAN(CXINNOON,ZZ,RADIUS,SCALE,APPROX)
      PR=SCALE*APPROX
      IF(I.EQ. 1) O2NOON=PR
      IF(I.EQ. 2) N2NOON=PR
      IF(I.EQ. 3) OONOON=PR
20      CONTINUE
      IF(NIGHT) GO TO 95
      IF(DAY ) GO TO 10
      IF(ZZ.LT. ZTRANS) GO TO 11
C
C      GO GET PHOTODISSOCIATION RATE COEFFICIENTS.
C
10      CALL DISSOC(DISOC,IALT)
      DK(192)=DISOC(2)
      DK(193)=DISOC(1)
      DK(194)=DISOC(6)

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 GIONEUT 1933

115	DK(195)=DISOC(5)	GIONEUT	1934
	DK(196)=DISOC(3)	GIONEUT	1935
	DK(197)=DISOC(4)	GIONEUT	1936
	DK(198)=DISOC(12)	GIONEUT	1937
120	DK(199)=DISOC(13)	GIONEUT	1938
	DK(200)=DISOC(7)	GIONEUT	1939
	DK(201)=DISOC(8)	GIONEUT	1940
	DK(202)=DISOC(9)	GIONEUT	1941
125	DK(203)=DISOC(10)	GIONEUT	1942
	DK(204)=DISOC(11)	GIONEUT	1943
	DK(205)=DISOC(14)	GIONEUT	1944
	IF(.NOT. JLOOK) GO TO 52	GIONEUT	1945
	IF(IALT.EQ. 1) GO TO 35	GIONEUT	1946
	IF(IALT.EQ. K) GO TO 40	GIONEUT	1947
130	IF(MOD(IALT-1,12).NE. 0) GO TO 52	GIONEUT	1948
	IA=IALT/12+1	GIONEUT	1949
	GO TO 45	GIONEUT	1950
	IA=IALT/12+2	GIONEUT	1951
135	DO 50 J=1,14	GIONEUT	1952
	DIS(J,IA)=DK(J+191)	GIONEUT	1953
	CONTINUE	GIONEUT	1954
	DIS(15,IA)=Z(IALT)	GIONEUT	1955
	DIS(16,IA)=N(IALT,8)	GIONEUT	1956
	DIS(17,IA)=O2COL	GIONEUT	1957
	DIS(18,IA)=N(IALT,9)	GIONEUT	1958
140	DIS(19,IA)=O3COL	GIONEUT	1959
	IF(ZZ.LT. ZTRANS) GO TO 95	GIONEUT	1960
	C	GIONEUT	1961
	C	GIONEUT	1962
	C	GIONEUT	1963
145	IF(ZZ.LT. ZS(1)) GO TO 280	GIONEUT	1964
	DO 200 I=1,4	GIONEUT	1965
	IF(SCXI.EQ. CHIS(I)) GO TO 240	GIONEUT	1966
	IF(SCXI.LT. CHIS(I)) GO TO 210	GIONEUT	1967
150	CONTINUE	GIONEUT	1968
	DO 220 J=1,8	GIONEUT	1969
	IF(ZZ.EQ. ZS(J)) GO TO 270	GIONEUT	1970
155	CONTINUE	GIONEUT	1971
	DO 235 L=1,8	GIONEUT	1972
	DO 225 J=1,8	GIONEUT	1973
	XIN(J)=ZS(J)	GIONEUT	1974
	YIN(J)=R(J,I-1,L)	GIONEUT	1975
160	CONTINUE	GIONEUT	1976
	A1=YINT(ZZ,XIN,YIN,0)	GIONEUT	1977
	B1=YINT(ZZ,XIN,YIN,8)	GIONEUT	1978
	DO 230 J=1,8	GIONEUT	1979
	YIN(J)=R(J,I,L)	GIONEUT	1980
	CONTINUE	GIONEUT	1981
	A1=YINT(ZZ,XIN,YIN,0)	GIONEUT	1982
	B1=YINT(ZZ,XIN,YIN,8)	GIONEUT	1983
165	A1=(SCXI-CHIS(I-1))/(CHIS(I)-CHIS(I-1))	GIONEUT	1984
	DK(L+207)=EXP(B1-A1*(B1-C1))	GIONEUT	1985
	CONTINUE	GIONEUT	1986
	GO TO 55	GIONEUT	1987
170	DO 245 J=1,8	GIONEUT	1988
	IF(ZZ.EQ. ZS(J)) GO TO 260	GIONEUT	1989
	CONTINUE	GIONEUT	1990

```

175      DO 255 L=1,8
180      DO 250 J=1,8
190      XIN(J)=ZS(J)
200      YIN(J)=R(J,I,L)
210      CONTINUE
220      A1=YINT(ZZ,XIN,YIN,0)
230      DK(L+207)=EXP(YINT(ZZ,XIN,YIN,8))
240      CONTINUE
250      GO TO 55
260      DO 265 L=1,8
270      DK(L+207)=EXP(R(J,I,L))
280      CONTINUE
290      GO TO 55
300      DO 275 L=1,8
310      A1=(SCXI-CHIS(I-1))/(CHIS(I)-CHIS(I-1))
320      DK(L+207)=EXP(R(J,I-1,L)-A1*(R(J,I-1,L)-R(J,I,L)))
330      CONTINUE
340      GO TO 55
350      DO 285 L=1,8
360      DK(L+207)=0.
370      CONTINUE
380      C
390      C COMPUTE N*H*F FOR O2, N2, AND O AT SOLAR ZENITH ANGLE CXI.
400      C
410      C
420      C
430      C
440      C
450      C
460      C
470      C
480      C
490      C
500      C
510      C
520      C
530      C
540      C
550      C
560      C
570      C
580      C
590      C
600      C
610      C
620      C
630      C
640      C
650      C
660      C
670      C
680      C
690      C
700      C
710      C
720      C
730      C
740      C
750      C
760      C
770      C
780      C
790      C
800      C
810      C
820      C
830      C
840      C
850      C
860      C
870      C
880      C
890      C
900      C
910      C
920      C
930      C
940      C
950      C
960      C
970      C
980      C
990      C

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230      75 CONTINUE
      80 GO TO 90
      DO 85 I=1,6
      SX(I)=SX(I)+SIGMA(I+3,L)*AFLUX
      85 CONTINUE
      86 GO TO 90
      86 SFLUX=AFLUX
      90 CONTINUE
      C
      C PARTITION THE X-RAY IONIZATION ACCORDING TO SWIDER, REVIEWS OF
      C GEOPHYSICS, 7, PG 573, 1969.
      C
      240      AX=N(IALT,8)+0.5*N(IALT,7)
      BX=1.0/(1.0+(N(IALT,23)/(1.15*AX)))
      CX=0.71*N(IALT,8)/AX
      XTOTAL=SX(1)*N(IALT,8)+SX(2)*N(IALT,23)+SX(3)*N(IALT,7)
      1      +SX(4)*N(IALT,11)+SX(5)*N(IALT,21)+SX(6)*N(IALT,16)
      SX(1)=BX*CX*XTOTAL
      SX(2)=0.61*(1.0-BX)*XTOTAL
      SX(3)=(1.0-CX)*8X*XTOTAL
      SX(6)=0.19*(1.0-BX)*XTOTAL
      C
      C COMPUTE TOTAL EUV AND X-RAY IONIZATION RATE COEFFICIENT FOR EACH ION.
      C
      250      DK(185)=QE(3)+SX(3)/N(IALT,7)
      DK(186)=QE(1)+SX(1)/N(IALT,8)
      DK(187)=QE(2)+SX(2)/N(IALT,23)
      DK(189)=QE(6)+SX(6)/N(IALT,16)
      DK(190)=QE(4)+SX(4)
      DK(191)=QE(5)+SX(5)
      C
      C COMPUTE IONIZATION RATE COEFFICIENT FOR NO BY LYMAN ALPHA.
      C
      260      DK(188)=2.08E-18*SFLUX
      C
      C COMPUTE IONIZATION RATE COEFFICIENT FOR O2(1DG) FOR WAVELENGTHS
      C 1027-1117 A.
      C
      265      DO 92 L=1,16
      SFLUX=SIGEFF(L)*EX(1)
      IF(SFLUX.GT.650.) GO TO 92
      DK(207)=DK(207)+PHI(L)*SIGI(L)*EXP(-SFLUX)
      92 CONTINUE
      C
      C ADD CONTRIBUTIONS FROM SCATTERED RADIATIONS AT LYMAN ALPHA,
      C LYMAN BETA, HE(I)(584A), AND HE(II)(304A).
      C
      275      AA=N(IALT,8)*O2NOON
      AB=N(IALT,23)*N2NOON
      AC=N(IALT,7)*ONCOON
      POWER=AA*SIGMA(1,1)
      LAPON=C
      IF(POWER.GT.650.) GO TO 91
      EXPON=EXP(-POWER)
      VALFA=1.0E-02*2.0E-18*FLUX(1)*EXPON
      POWER=AA*SIGMA(1,2)+25*SIGMA(2,2)
      LAPON=C
      91
      280
      285

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 GIONEUT 2103  
 GIONEUT 2104

60	R(1)=K(1)*Y(7)*Y(17) R(2)=K(2)*Y(7)*Y(10) R(3)=K(3)*Y(7)*Y(12) R(4)=K(4)*Y(7)*Y(19) R(5)=K(5)*Y(11)*Y(12) R(6)=K(6)*Y(11)*Y(12) R(7)=K(7)*Y(11)*Y(9) R(8)=K(8)*Y(16)*Y(9) R(9)=K(9)*Y(16)*Y(19) R(10)=K(10)*Y(16)*Y(19) R(11)=K(11)*Y(16)*Y(19) R(12)=K(12)*Y(10)*Y(10) R(13)=K(13)*Y(10)*Y(12) R(14)=K(14)*Y(17)*Y(8) R(15)=K(15)*Y(27)*Y(13) R(16)=K(16)*Y(27)*Y(57) R(17)=K(17)*Y(27)*Y(15) R(18)=K(18)*Y(20)*Y(57) R(19)=K(19)*Y(20)*Y(57) R(20)=K(20)*Y(55)*Y(7) R(21)=K(21)*Y(55)*Y(10) R(22)=K(22)*Y(28)*Y(30) R(23)=K(23)*Y(28)*Y(30) R(24)=K(24)*Y(41)*Y(30) R(25)=K(25)*Y(42)*Y(30) R(26)=K(26)*Y(43)*Y(30) R(27)=K(27)*Y(44)*Y(30) R(28)=K(28)*Y(45)*Y(30) R(29)=K(29)*Y(47)*Y(30) R(30)=K(30)*Y(49)*Y(30) R(31)=K(31)*Y(7)*Y(30) R(32)=K(32)*Y(8)*Y(23)*Y(30) R(33)=K(33)*Y(4)*Y(18) R(34)=K(34)*Y(4)*Y(16) R(35)=K(35)*Y(4)*Y(19) R(36)=K(36)*Y(39)*Y(7) R(37)=K(37)*Y(39)*Y(13) R(38)=K(38)*Y(28)*Y(7) R(39)=K(39)*Y(28)*Y(7) R(40)=K(40)*Y(3)*Y(11) R(41)=K(41)*Y(1)*Y(7) R(42)=K(42)*Y(6)*Y(8) R(43)=K(43)*Y(6)*Y(8) R(44)=K(44)*Y(6)*Y(8) R(45)=K(45)*Y(2)*Y(8) R(46)=K(46)*Y(2)*Y(8) R(47)=K(47)*Y(2)*Y(23) R(48)=K(48)*Y(2)*Y(23) R(49)=K(49)*Y(2)*Y(18) R(50)=K(50)*Y(40)*Y(18) R(51)=K(51)*Y(42)*Y(25)*Y(57) R(52)=K(52)*Y(44)*Y(13)*Y(57) R(53)=K(53)*Y(50)*Y(13) R(54)=K(54)*Y(50)*Y(13) R(55)=K(55)*Y(53)*Y(13) R(56)=K(56)*Y(54)*Y(13) R(57)=K(57)*Y(46)*Y(25)	GIONEUT 2595 GIONEUT 2596 GIONEUT 2597 GIONEUT 2598 GIONEUT 2599 GIONEUT 2600 GIONEUT 2601 GIONEUT 2602 GIONEUT 2603 GIONEUT 2604 GIONEUT 2605 GIONEUT 2606 GIONEUT 2607 GIONEUT 2608 GIONEUT 2609 GIONEUT 2610 GIONEUT 2611 GIONEUT 2612 GIONEUT 2613 GIONEUT 2614 GIONEUT 2615 GIONEUT 2616 GIONEUT 2617 GIONEUT 2618 GIONEUT 2619 GIONEUT 2620 GIONEUT 2621 GIONEUT 2622 GIONEUT 2623 GIONEUT 2624 GIONEUT 2625 GIONEUT 2626 GIONEUT 2627 GIONEUT 2628 GIONEUT 2629 GIONEUT 2630 GIONEUT 2631 GIONEUT 2632 GIONEUT 2633 GIONEUT 2634 GIONEUT 2635 GIONEUT 2636 GIONEUT 2637 GIONEUT 2638 GIONEUT 2639 GIONEUT 2640 GIONEUT 2641 GIONEUT 2642 GIONEUT 2643 GIONEUT 2644 GIONEUT 2645 GIONEUT 2646 GIONEUT 2647 GIONEUT 2648 GIONEUT 2649 GIONEUT 2650 GIONEUT 2651
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1      SUBROUTINE CHEMPR(IZ)
C
C      THIS SUBROUTINE PRINTS OUT THE FULL CHEMISTRY LIST ALONG WITH
C      THE RATE COEFFICIENTS AND THE RATES OF ALL REACTIONS AT THE
C      ALTITUDE CORRESPONDING TO THE INDEX IZ.
5
C
C      DIMENSION Y(57),R(215),K(215)
C
C      COMMON N(692,30),CONC(424,26),U(692,26),NZERO(692),UZERO(692)
C
C      COMMON FORM(692),REMV(692),E(692),F(692),Z(692),
2      DEDY(692),TEMP(692),STEMDZ(692),DELTAZ(692),SUNSET(692)
C
C      COMMON GRAV,COSD,SIND,TIME,CXI,RADIUS,ISPECI,KSPECI,NREAC,KTOP,
1      K2,KMIN1,ITURB,CXINCON,SCXI,NREAC2
C
C      COMMON/ESM/OLDN(692,30),OLDCON(424,26),OLDU(692,26),RATES(88,692)
C
C      COMMON/LOGIC/NIGHT,DAY,JLOOK,RESET,END
C
C      COMMON/RATECON/AK(88),BK(88),CK(88),DK(215),CYMB(6,215)
C
C      LEVEL 3, OLDN,OLDCON,OLDU,RATES
C      REAL K,N,NZERO
C      LOGICAL NIGHT
C      EQUIVALENCE (Y,E),(R,F),(NZERO,K)
C
C      WRITE(6,1) Z(IZ),SCXI
30      FORMAT(1H1," CHEMISTRY AT ",F7.2," KM. AND AT", 1PE12.5
1,"DEGREES.")
C      WRITE(6,5)
5      FORMAT(1H0,18X,"CHEMICAL REACTION",35X,"RATE CONSTANT",5X,
1,"FORWARD RATE(/CM3/SEC)*")
C      DO 6 I=1,NREAC
C      K(I)=DK(I)
6      CONTINUE
C      IF(.NOT. NIGHT) GO TO 10
C      K(96)=K(99)=K(104)=K(105)=K(110)=0.
C      K(113)=K(114)=K(118)=K(120)=K(123)=0.
C      CALL MOVLEV(RATES(1,IZ),K(128),88)
10     IF(IZ .LE. K2) GO TO 11
C      K(31)=K(32)=K(35)=0.
C      K(160)=K(161)=K(162)=K(165)=K(166)=0.
45     DO 25 I=1,ISPECI
C      IF(I .GT. 30) GO TO 4
C      Y(I)=N(IZ,I)
C      GO TO 25
4     IF(IZ .GT. K2) GO TO 15
C      Y(1)=CONC(IZ,1-30)
C      GO TO 25
15     Y(1)=0.
25     CONTINUE
C      Y(57)=0.
C      DO 30 I=1,ISPECI
C      Y(57)=Y(57)+Y(I)
55     CONTINUE
30

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 GIONEUT 2594



1		SUBROUTINE INDEX(COL,LIM,I,DEL)	GIONEUT 2509
	C		GIONEUT 2510
	C	THIS SUBROUTINE COMPUTES AN INDEX I AND AN INCREMENT DEL FROM	GIONEUT 2511
	C	THE COLUMN DENSITY COL.	GIONEUT 2512
5	C		GIONEUT 2513
		REAL LOG2,LOG5	GIONEUT 2514
		LOGICAL ISKIP	GIONEUT 2515
		DATA ISKIP/.FALSE./	GIONEUT 2516
	C		GIONEUT 2517
10		IF(ISKIP) GO TO 5	GIONEUT 2518
		LOG2=ALOG10(2.0)	GIONEUT 2519
		LOG5=ALOG10(5.0)	GIONEUT 2520
		ISKIP=.TRUE.	GIONEUT 2521
	C		GIONEUT 2522
15	5	A=ALOG10(COL)	GIONEUT 2523
		INTA=INT(A)	GIONEUT 2524
		FA=A-INTA	GIONEUT 2525
		I=3*(INTA-LIM)+1	GIONEUT 2526
		IF(FA .GT. LOG2) GO TO 10	GIONEUT 2527
20		DEL=FA/LOG2	GIONEUT 2528
		RETURN	GIONEUT 2529
	10	IF(FA .GT. LOG5) GO TO 20	GIONEUT 2530
		DEL=(FA-LOG2)/(LOG5-LOG2)	GIONEUT 2531
		I=I+1	GIONEUT 2532
		RETURN	GIONEUT 2533
25	20	DEL=(FA-LOG5)/(1.0-LOG5)	GIONEUT 2534
		I=I+2	GIONEUT 2535
		RETURN	GIONEUT 2536
		END	GIONEUT 2537

1		FUNCTION TRPLT1 (ARRAY, IO3, DELO3)	GIONEUT 2497
	C		GIONEUT 2498
	C	THIS FUNCTION INTERPOLATES IN THE ONE DIMENSIONAL PHOTODISSOCIATION	GIONEUT 2499
	C	RATE COEFFICIENT TABLES.	GIONEUT 2500
5	C		GIONEUT 2501
	C	DIMENSION ARRAY(1)	GIONEUT 2502
	C		GIONEUT 2503
		A=ARRAY(IO3)	GIONEUT 2504
		B=ARRAY(IO3+1)	GIONEUT 2505
10		TRPLT1=10.0** (A-DELO3*(A-B))	GIONEUT 2506
		RETURN	GIONEUT 2507
		END	GIONEUT 2508

```

1      FUNCTION TRPLT2(ARRAY,N,M,IO2,DELO2,IO3,DELO3)
C
C      THIS FUNCTION INTERPOLATES IN THE TWO DIMENSIONAL PHOTODISSOCIATION
C      RATE COEFFICIENT TABLES.
C
5      DIMENSION ARRAY(N,M)
C
C      A=ARRAY(IO2,IO3)
C      B=ARRAY(IO2,IO3+1)
C      C=ARRAY(IO2+1,IO3)
C      D=ARRAY(IO2+1,IO3+1)
C      Y1=A-DELO3*(A-B)
C      Y2=C-DELO3*(C-D)
C      TRPLT2=10.0*(Y1-DELO2*(Y1-Y2))
C      RETURN
C      END
15

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GIONEUT 2486
GIONEUT 2487
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GIONEUT 2495
GIONEUT 2496

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 GIONEUT 2479  
 GIONEUT 2480

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IF(O2COL .GT. 23.5) GO TO 210
DO 200 I1=1,12
IF(O2COL .LT. O2C(I1)) GO TO 215
CONTINUE
STOP 7
205 DISC(I3)=10.0*(PNO(I1))
GO TO 220
210 DISC(I3)=0.
GO TO 220
215 DELO2=(O2COL-O2C(I1-1))/(O2C(I1)-O2C(I1-1))
DISC(I3)=10.0*(PNO(I1-1)-PNO(I1))
220 O2COL=10.0*(O2COL
RETURN
END
  
```

230

235

240

175	IF(O3COLM.GT. 1.0E+21) O3COL=1.0E+21 LIMIT=14 CALL INDEX(O3COL,LIMIT,I03,DELO3) DISOC(9)=TRPLT1(J202,I03,DELO3)	GIONEUT 2410 GIONEUT 2411 GIONEUT 2412 GIONEUT 2413 GIONEUT 2414 GIONEUT 2415 GIONEUT 2416 GIONEUT 2417 GIONEUT 2418 GIONEUT 2419 GIONEUT 2420 GIONEUT 2421 GIONEUT 2422 GIONEUT 2423 GIONEUT 2424 GIONEUT 2425 GIONEUT 2426 GIONEUT 2427 GIONEUT 2428 GIONEUT 2429 GIONEUT 2430 GIONEUT 2431 GIONEUT 2432 GIONEUT 2433 GIONEUT 2434 GIONEUT 2435 GIONEUT 2436 GIONEUT 2437 GIONEUT 2438 GIONEUT 2439 GIONEUT 2440 GIONEUT 2441 GIONEUT 2442 GIONEUT 2443 GIONEUT 2444 GIONEUT 2445 GIONEUT 2446 GIONEUT 2447 GIONEUT 2448 GIONEUT 2449 GIONEUT 2450 GIONEUT 2451 GIONEUT 2452 GIONEUT 2453 GIONEUT 2454 GIONEUT 2455 GIONEUT 2456 GIONEUT 2457 GIONEUT 2458 GIONEUT 2459 GIONEUT 2460 GIONEUT 2461 GIONEUT 2462 GIONEUT 2463 GIONEUT 2464 GIONEUT 2465 GIONEUT 2466
	C REACTION C02 + HV = CO + O1D IN DISOC(10)	
180	O2COL=O2COLM IF(O2COLM.LT. 1.0E+13) O2COL=1.1E+13 IF(O2COLM.GT. 5.0E+22) O2COL=5.0E+22 LIMIT=13 CALL INDEX(O2COL,LIMIT,I02,DELO2) O3COL=O3COLM IF(O3COLM.LT. 1.0E+11) O3COL=1.1E+11 IF(O3COLM.GT. 2.0E+20) O3COL=2.0E+20 LIMIT=11 CALL INDEX(O3COL,LIMIT,I03,DELO3) DISOC(10)=TRPLT2(J203,30,29,I02,DELO2,I03,DELO3)	
185		
190	C REACTION C02 + HV = CO + O IN DISOC(11)	
	C	
195	O2COL=O2COLM IF(O2COLM.LT. 1.0E+13) O2COL=1.1E+13 IF(O2COLM.GT. 2.0E+24) O2COL=2.0E+24 LIMIT=13 CALL INDEX(O2COL,LIMIT,I02,DELO2) O3COL=O3COLM IF(O3COLM.LT. 1.0E+12) O3COL=1.1E+12 IF(O3COLM.GT. 1.0E+21) O3COL=1.0E+21 LIMIT=12 CALL INDEX(O3COL,LIMIT,I03,DELO3) DISOC(11)=TRPLT2(J204,35,28,I02,DELO2,I03,DELO3)	
200		
205	C REACTION H02 + HV = O2 + H IN DISOC(12)	
	C	
210	O2COL=O2COLM IF(O2COLM.LT. 1.0E+17) O2COL=1.1E+17 IF(O2COLM.GT. 2.0E+25) O2COL=2.0E+25 LIMIT=17 CALL INDEX(O2COL,LIMIT,I02,DELO2) O3COL=O3COLM IF(O3COLM.LT. 1.0E+12) O3COL=1.1E+12 IF(O3COLM.GT. 1.0E+21) O3COL=1.0E+21 LIMIT=12 CALL INDEX(O3COL,LIMIT,I03,DELO3) DISOC(12)=TRPLT2(J198,26,28,I02,DELO2,I03,DELO3)	
215		
220	C REACTION N03 + HV = N02 + O2 IN DISOC(14)	
	C	
225	O3COL=O3COLM IF(O3COLM.LT. 1.0E+14) O3COL=1.1E+14 IF(O3COLM.GT. 1.0E+21) O3COL=1.0E+21 LIMIT=14 CALL INDEX(O3COL,LIMIT,I03,DELO3) DISOC(14)=TRPLT1(J205,I03,DELO3) O2COL=ALOG10(O2COLM) IF(O2COL.LT. 18.0) GO TO 205	

115	C	DISOC(4)=TRPLT2(J197,27,28,102,DELO2,103,DELO3)	GIONEUT	2353
	C	REACTION O3 + HV = O1D + O21D IN DISOC(5)	GIONEUT	2354
	C		GIONEUT	2355
120		O2COL=O2COLM	GIONEUT	2356
		IF(O2COLM.LT. 1.0E+15) O2COL=1.1E+15	GIONEUT	2357
		IF(O2COLM.GT. 2.0E+25) O2COL=2.0E+25	GIONEUT	2358
		LIMIT=15	GIONEUT	2359
		CALL INDEX(O2COL,LIMIT,102,DELO2)	GIONEUT	2360
		O3COL=O3COLM	GIONEUT	2361
125		IF(O3COLM.LT. 1.0E+12) O3COL=1.1E+12	GIONEUT	2362
		IF(O3COLM.GT. 1.0E+21) O3COL=1.0E+21	GIONEUT	2363
		LIMIT=12	GIONEUT	2364
		CALL INDEX(O3COL,LIMIT,103,DELO3)	GIONEUT	2365
		DISOC(5)=TRPLT2(J195,32,28,102,DELO2,103,DELO3)	GIONEUT	2366
130	C		GIONEUT	2367
	C	REACTION O3 + HV = O + O2 IN DISOC(6)	GIONEUT	2368
	C		GIONEUT	2369
135		O3COL=O3COLM	GIONEUT	2370
		IF(O3COLM.LT. 1.0E+14) O3COL=1.1E+14	GIONEUT	2371
		IF(O3COLM.GT. 1.0E+21) O3COL=1.0E+21	GIONEUT	2372
		LIMIT=14	GIONEUT	2373
		CALL INDEX(O3COL,LIMIT,103,DELO3)	GIONEUT	2374
		DISOC(6)=TRPLT1(J194,103,DELO3)	GIONEUT	2375
140	C		GIONEUT	2376
	C	REACTION NO2 + HV = NO + O1D IN DISOC(7)	GIONEUT	2377
	C		GIONEUT	2378
145		O2COL=O2COLM	GIONEUT	2379
		IF(O2COLM.LT. 1.0E+19) O2COL=1.1E+19	GIONEUT	2380
		IF(O2COLM.GT. 1.0E+25) O2COL=1.0E+25	GIONEUT	2381
		LIMIT=19	GIONEUT	2382
		CALL INDEX(O2COL,LIMIT,102,DELO2)	GIONEUT	2383
		O3COL=O3COLM	GIONEUT	2384
		IF(O3COLM.LT. 1.0E+14) O3COL=1.1E+14	GIONEUT	2385
		IF(O3COLM.GT. 5.0E+18) O3COL=5.0E+18	GIONEUT	2386
		LIMIT=14	GIONEUT	2387
150		CALL INDEX(O3COL,LIMIT,103,DELO3)	GIONEUT	2388
		DISOC(7)=TRPLT2(J200,19,15,102,DELO2,103,DELO3)	GIONEUT	2389
155	C		GIONEUT	2390
	C	REACTION N2O + HV = N2 + O1D IN DISOC(8)	GIONEUT	2391
	C		GIONEUT	2392
160		O2COL=O2COLM	GIONEUT	2393
		IF(O2COLM.LT. 1.0E+17) O2COL=1.1E+17	GIONEUT	2394
		IF(O2COLM.GT. 2.0E+25) O2COL=2.0E+25	GIONEUT	2395
		LIMIT=17	GIONEUT	2396
		CALL INDEX(O2COL,LIMIT,102,DELO2)	GIONEUT	2397
		O3COL=O3COLM	GIONEUT	2398
		IF(O3COLM.LT. 1.0E+11) O3COL=1.1E+11	GIONEUT	2399
		IF(O3COLM.GT. 5.0E+19) O3COL=5.0E+19	GIONEUT	2400
		LIMIT=11	GIONEUT	2401
165		CALL INDEX(O3COL,LIMIT,103,DELO3)	GIONEUT	2402
		DISOC(8)=TRPLT2(J201,26,27,102,DELO2,103,DELO3)	GIONEUT	2403
	C	REACTION HNO2 + HV = OH + OH IN DISOC(9)	GIONEUT	2404
	C		GIONEUT	2405
170		O3COL=O3COLM	GIONEUT	2406
		IF(O3COLM.LT. 1.0E+14) O3COL=1.1E+14	GIONEUT	2407
			GIONEUT	2408
			GIONEUT	2409



```

1      SUBROUTINE DISSOC(DISOC,IALT)
C
C      DIMENSION DISOC(14),O2C(12),PNO(12)
C
5      COMMON N(692,30),CONC(424,26),U(692,26),NZERO(692),UZERO(692)
C
C      COMMON FORM(692),REMV(692),E(692),F(692),Z(692),
2      DEDY(692),TEMP(692),DTEMZ(692),DELTAZ(692),SUNSET(692)
C
10     COMMON GRAV,COSD,SIND,TIME,CXI,RADIUS,ISPECI,KSPECI,NREAC,K,
C      K2,KMIN1,ITURB,CXINOO,SCXI,NREAC2
C
15     COMMON/ATCONS/ATWT(26),MASS(26),THERM(26),SYMBOL(56),POLAR(26)
C
C      COMMON/CONSTAN/PI,RADDEG,DEGRAD,RADSEC,BOLTZ,SIN2I,ATCON
C
C      COMMON/JAYS/J192(26,25),J193(28,26),J194(22),J195(32,28),
1      J196(31,30),J197(27,28),J198(26,28),J200(19,15),
2      J201(26,27),J202(22),J203(30,29),J204(35,28),J205(22)
C
20     COMMON/COLUM/O2COLM,O3COLM,DIS(19,59)
C
C      REAL N,MASS,J192,J193,J194,J195,J196,J197,J198,J200,J201,J202
REAL J203,J204,J205
25     LOGICAL JSTART
DATA JSTART/.TRUE./
C
C      THE FOLLOWING TWO DATA STATEMENTS CONTAIN THE NO PHOTODISSOCIATION
C      RATE COEFFICIENTS (PNO) AS FUNCTIONS OF THE COLUMN DENSITY OF
C      O2 (O2C). DATA FROM CIESLIK AND NICOLET, PLANET SPACE SCI.
C      21, 925, 1973.
C
35     DATA O2C/18.0,18.5,19.0,19.5,20.0,20.5,21.0,21.5,22.0,22.5,23.0,
1      23.5/
DATA PNO/1.41E-5,1.40E-5,1.38E-5,1.33E-5,1.22E-5,1.02E-5,
1      6.98E-6,3.58E-6,6.93E-7,1.26E-7,4.45E-12,1.50E-29/
C
C      GRAVCOR(ZE)=1.0/((1.0+ZE/RADIUS)**2)
C
40     COMPUTE COLUMN DENSITIES OF O2 AND O3 USING THE SWIDER
C      APPROXIMATION TO THE CHAPMAN FUNCTION.
C
C      ALT=Z(IALT)
T=(BOLTZ*TEMP(IALT))/(GRAV*GRAVCOR(ALT))
45     SCALE=T/MASS(8)
CALL CHAPMAN(CXI,ALT,RADIUS,SCALE,APPROX)
O2COLM=N(IALT,8)*SCALE*APPROX
SCALE=T/MASS(9)
CALL CHAPMAN(CXI,ALT,RADIUS,SCALE,APPROX)
50     O3COLM=N(IALT,9)*SCALE*APPROX
IF(.NOT. JSTART) GO TO 35
JSTART=.FALSE.
C
C      REDUCE THE NO PHOTODISSOCIATION RATE COEFFICIENTS BY FACTOR OF 4.
C
55     DO 1 I=1,12
PNO(I)=ALOG10(PNO(I))/4.0

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G1ONEUT 2239  
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 G1ONEUT 2241  
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 G1ONEUT 2291  
 G1ONEUT 2292  
 G1ONEUT 2293  
 G1ONEUT 2294  
 G1ONEUT 2295



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1      SUBROUTINE CHAPMAN(CXI,Z,R,H,F)
C
C      THIS SUBROUTINE COMPUTES AN APPROXIMATION FOR THE CHAPMAN
C      FUNCTION USING EQUATIONS F(2) AND FH OF SWIDER FROM
C      *ON THE ACCURACY OF CERTAIN APPROXIMATIONS FOR THE CHAPMAN
C      FUNCTION* AFCL-67-0468.
C
C      DATA P1OV2/1.570796326795/.SQPI2/8.862269254528E-01/
C      DATA PI/3.14159265359/
C      X=(R+Z)/(H*1.0E-05)
C      Y=X*SIN(CXI)
C      IF(CXI.GT. P1OV2) GO TO 10
C      W=X-Y
C      IF(W.NE. 0.) GO TO 1
C      F=SQRT(1.0+2.0*X)*SQPI2
C      RETURN
C
15     1      A=SQRT(W)
C      IF(W.GE. 9.5) GO TO 5
C      COM=ERFC(A)
C      F=-X*COM(CXI)+SQRT(1.0+2.0*X-W)*(A+SQPI2*COM*EXP(W))
C      RETURN
C
20     5      F=-X*COM(CXI)+SQRT(1.0+2.0*X-W)*(A+(1.0/(2.0*A))*(1.0
C      1      -(1.0/(2.0*W)))+(3.0/(4.0*(W**2)))-(15.0/(8.0*(W**3))))))
C      RETURN
C
25     10     A=-SQRT(Y/2.0)/TAN(CXI)
C      EF=ERF(A)
C      F=SQRT(PI*Y/2.0)*(1.0+EF)
C      RETURN
C      END
G1ONEUT 2210
G1ONEUT 2211
G1ONEUT 2212
G1ONEUT 2213
G1ONEUT 2214
G1ONEUT 2215
G1ONEUT 2216
G1ONEUT 2217
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GIONEUT 2190  
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 GIONEUT 2208  
 GIONEUT 2209

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60      RETURN
      C  ERROR EXITS.
      C
20      PRINT 902, J, J1, JX, JH, X(J), X(J1), DX
902     FORMAT(" ERROR IN YINT.  DX .LE. 0.",
1/     J=" ,I4," J1=" ,I4," JX=" ,I4," JH=" ,I4," X(J)=" ,1PE13.5,
2     X(J1)=" ,E13.5," DX=" ,E13.5)
      GO TO 910
30      PRINT 903, JX, JH, X1, X(JX-1), X(JH)
903     FORMAT(" ERROR IN YINT.  X1 OUTSIDE RANGE OF X.",
1/     JX=" ,I4," JH=" ,I4," X1=" ,1PE13.5," X(JX-1)=" ,E13.5,
2     X(JH)=" ,E13.5)
      GO TO 910
40      PRINT 904, J, J1, JX, JH, X(J), X(J+1), DX1
904     FORMAT(" ERROR IN YINT.  DX1 .LE. 0.",
1/     J=" ,I4," J1=" ,I4," JX=" ,I4," JH=" ,I4," X(J)=" ,1PE13.5,
2     X(J+1)=" ,E13.5," DX1=" ,E13.5)
910     STOP
      END
75
  
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```

1      FUNCTION YINT(XII,X,Y,JHI)
2
3      C THIS FUNCTION RETURNS INTERPOLATED YINT FOR INPUT XII. ARRAY X
4      C MUST BE MONOTONICALLY INCREASING. JHI IS NUMBER OF POINTS IN
5      C X AND Y ARRAYS.
6
7      C INITIALIZE BY CALL WITH JHI=0 BEFORE EACH ARRAY CALL.
8
9      C EXAMPLE
10     C INITIALIZE
11     C YY=YINT(XII,X,Y,0)
12     C LOOP ARRAY INTERPOLATE
13     C DO 10 K=1,100
14     C XII=K
15     C 10 YI(K)=YINT(XII,X,Y,JHI)
16
17     C DIMENSION X(1),Y(1)
18     C JH=JHI
19     C XI=XII
20     C IF(JH.GT. 0) GO TO 8
21     C INITIALIZE
22     C J1=0
23     C RETURN
24
25     8 IF(J1.LT. 1) JX=2
26     IF(J1.LT. 1) GO TO 1
27     C TEST IF XI BETWEEN CURRENT X(J1),X(J1+1)
28     IF(XI.GE. X(J1).AND. XI.LE. X(J1+1)) GO TO 2
29     C SEARCH FOR STRADDLING X VALUES
30     1 DO 10 J=JX,JH
31     J1=J-1
32     DX=X(J)-X(J1)
33     C TEST FOR NON-ZERO DX
34     IF(DX.LE. 0.) GO TO 20
35     IF(XI.GE. X(J1).AND. XI.LE. X(J)) GO TO 4
36     10 CONTINUE
37     C ERROR
38     GO TO 30
39
40     C COMPUTE SA=AVG SLOPE BETWEEN X(J1) AND X(J1+1)
41     4 SA=(Y(J)-Y(J1))/DX
42     JX=J
43     C SET PV,NXT SLOPE TO SA TEMPORARILY
44     SAP=SAN=SA
45     C SET PVS SLOPE IF J1.GT.1
46     IF(J1.GT. 1) SAP=(Y(J1)-Y(J1-1))/(X(J1)-X(J1-1))
47     IF(J.GE. JH) GO TO 6
48     DX1=X(J+1)-X(J)
49     IF(DX1.LE. 0.) GO TO 40
50     C SET NEXT SLOPE IF J1.LT. JH1-1
51     SAN=(Y(J+1)-Y(J))/DX1
52     S1=S2=0.
53     IF(SA*SAP.GT. 0.) S1=2.*SA*SAP/(SA+SAP)
54     IF(SA*SAN.GT. 0.) S2=2.*SA*SAN/(SA+SAN)
55     A2=(3.*SA-2.*S1-S2)/DX
56     A3=(SA-S1-A2*DX)/DX/DX
57     C THIS IS CUBIC FIT FOR STRADDLES XI
58     2 DX1=X1-X(J1)
59     YINT=Y(J1)+DX1*(S1+DX1*(A2+DX1*A3))
60

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GIONEUT 2133  
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 GIONEUT 2189

290	96	IF(POWER .GT. 650.) GO TO 96 EXPON=EXP(-POWER) LYBETA=4.0E-03*SIGMA(4,2)*FLUX(2)=EXPON POWER=AA*SIGMA(1,55)+AB*SIGMA(2,55)+AC*SIGMA(3,55) EXPON=0. IF(POWER .GT. 650.) GO TO 100 EXPON=EXP(-POWER) HEI=1.1E-03*FLUX(55)*EXPON POWER=AA*SIGMA(1,68)+AB*SIGMA(2,68)+AC*SIGMA(3,68) EXPON=0. IF(POWER .GT. 650.) GO TO 105 EXPON=EXP(-POWER) HEI1=1.0E-03*FLUX(68)*EXPON DK(185)=DK(185)+HEI*SIGMA(6,55)+HEI1*SIGMA(6,68) DK(186)=DK(186)+LYBETA+HEI*SIGMA(4,55)+HEI1*SIGMA(4,68) DK(187)=DK(187)+HEI*SIGMA(5,55)+HEI1*SIGMA(5,68) DK(188)=DK(188)+LYALFA DK(190)=DK(190)+HEI*SIGMA(7,55)+HEI1*SIGMA(7,68) DK(191)=DK(191)+HEI*SIGMA(8,55)+HEI1*SIGMA(8,68)	GIONEUT 2105 GIONEUT 2106 GIONEUT 2107 GIONEUT 2108 GIONEUT 2109 GIONEUT 2110 GIONEUT 2111 GIONEUT 2112 GIONEUT 2113 GIONEUT 2114 GIONEUT 2115 GIONEUT 2116 GIONEUT 2117 GIONEUT 2118 GIONEUT 2119 GIONEUT 2120 GIONEUT 2121 GIONEUT 2122 GIONEUT 2123 GIONEUT 2124 GIONEUT 2125 GIONEUT 2126 GIONEUT 2127 GIONEUT 2128 GIONEUT 2129 GIONEUT 2130 GIONEUT 2131 GIONEUT 2132
305	C	ADD COSMIC RAY IONIZATION. Q=1.0E-17-N	
310	110	DO 110 I=185,191 DK(I)=DK(I)+COSMIC CONTINUE DK(206)=DK(185) RETURN END	

115	R(58)=K(58)*Y(48)*Y(13)*Y(23) R(59)=K(59)*Y(49)*Y(13) R(60)=K(60)*Y(48)*Y(13) R(61)=K(61)*Y(47)*Y(13) R(62)=K(62)*Y(41)*Y(35) R(63)=K(63)*Y(41)*Y(36) R(64)=K(64)*Y(41)*Y(37) R(65)=K(65)*Y(42)*Y(32) R(66)=K(66)*Y(42)*Y(35) R(67)=K(67)*Y(42)*Y(36) R(68)=K(68)*Y(42)*Y(37) R(69)=K(69)*Y(42)*Y(38) R(70)=K(70)*Y(43)*Y(35) R(71)=K(71)*Y(43)*Y(36) R(72)=K(72)*Y(43)*Y(37) R(73)=K(73)*Y(43)*Y(38) R(74)=K(74)*Y(44)*Y(35) R(75)=K(75)*Y(44)*Y(36) R(76)=K(76)*Y(44)*Y(37) R(77)=K(77)*Y(44)*Y(38) R(78)=K(78)*Y(45)*Y(35) R(79)=K(79)*Y(45)*Y(36) R(80)=K(80)*Y(45)*Y(37) R(81)=K(81)*Y(45)*Y(38) R(82)=K(82)*Y(51)*Y(35) R(83)=K(83)*Y(51)*Y(36) R(84)=K(84)*Y(51)*Y(37) R(85)=K(85)*Y(52)*Y(35) R(86)=K(86)*Y(52)*Y(36) R(87)=K(87)*Y(52)*Y(37) R(88)=K(88)*Y(53)*Y(35) R(89)=K(89)*Y(53)*Y(36) R(90)=K(90)*Y(53)*Y(37) R(91)=K(91)*Y(48)*Y(36) R(92)=K(92)*Y(48)*Y(37) R(93)=K(93)*Y(48)*Y(38) R(94)=K(94)*Y(49)*Y(37) R(95)=K(95)*Y(49)*Y(38) R(96)=K(96)*Y(31) R(97)=K(97)*Y(31)*Y(7) R(98)=K(98)*Y(31)*Y(9) R(99)=K(99)*Y(32) R(100)=K(100)*Y(32)*Y(7) R(101)=K(101)*Y(32)*Y(7) R(102)=K(102)*Y(32)*Y(9) R(103)=K(103)*Y(32)*Y(20) R(104)=K(104)*Y(33) R(105)=K(105)*Y(33) R(106)=K(106)*Y(33)*Y(7) R(107)=K(107)*Y(34)*Y(7) R(108)=K(108)*Y(34)*Y(7) R(109)=K(109)*Y(34)*Y(25) R(110)=K(110)*Y(37) R(111)=K(111)*Y(37)*Y(7) R(112)=K(112)*Y(37)*Y(19) R(113)=K(113)*Y(38) R(114)=K(114)*Y(38)	GIONEUT 2652 GIONEUT 2653 GIONEUT 2654 GIONEUT 2655 GIONEUT 2656 GIONEUT 2657 GIONEUT 2658 GIONEUT 2659 GIONEUT 2660 GIONEUT 2661 GIONEUT 2662 GIONEUT 2663 GIONEUT 2664 GIONEUT 2665 GIONEUT 2666 GIONEUT 2667 GIONEUT 2668 GIONEUT 2669 GIONEUT 2670 GIONEUT 2671 GIONEUT 2672 GIONEUT 2673 GIONEUT 2674 GIONEUT 2675 GIONEUT 2676 GIONEUT 2677 GIONEUT 2678 GIONEUT 2679 GIONEUT 2680 GIONEUT 2681 GIONEUT 2682 GIONEUT 2683 GIONEUT 2684 GIONEUT 2685 GIONEUT 2686 GIONEUT 2687 GIONEUT 2688 GIONEUT 2689 GIONEUT 2690 GIONEUT 2691 GIONEUT 2692 GIONEUT 2693 GIONEUT 2694 GIONEUT 2695 GIONEUT 2696 GIONEUT 2697 GIONEUT 2698 GIONEUT 2699 GIONEUT 2700 GIONEUT 2701 GIONEUT 2702 GIONEUT 2703 GIONEUT 2704 GIONEUT 2705 GIONEUT 2706 GIONEUT 2707 GIONEUT 2708
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175	R(115)=K(115)•Y(38)•Y(7) R(116)=K(116)•Y(38)•Y(9) R(117)=K(117)•Y(38)•Y(18) R(118)=K(118)•Y(35) R(119)=K(119)•Y(35)•Y(9) R(120)=K(120)•Y(36) R(121)=K(121)•Y(36)•Y(7) R(122)=K(122)•Y(56)•Y(18) R(123)=K(123)•Y(36) R(124)=K(124)•Y(31)•Y(9) R(125)=K(125)•Y(29)•Y(23) R(126)=K(126)•Y(29)•Y(8) R(127)=K(127)•Y(3)•Y(25) R(128)=K(128)•Y(7)•Y(7)•Y(57) R(129)=K(129)•Y(7)•Y(8)•Y(57) R(130)=K(130)•Y(7)•Y(9) R(131)=K(131)•Y(7)•Y(15) R(132)=K(132)•Y(7)•Y(14) R(133)=K(133)•Y(7)•Y(14) R(134)=K(134)•Y(11)•Y(14) R(135)=K(135)•Y(11)•Y(14) R(136)=K(136)•Y(11)•Y(8)•Y(57) R(137)=K(137)•Y(16)•Y(8) R(138)=K(138)•Y(16)•Y(18) R(139)=K(139)•Y(16)•Y(7)•Y(57) R(140)=K(140)•Y(10)•Y(9) R(141)=K(141)•Y(10)•Y(14) R(142)=K(142)•Y(18)•Y(9) R(143)=K(143)•Y(18)•Y(7)•Y(57) R(144)=K(144)•Y(12)•Y(12) R(145)=K(145)•Y(12)•Y(9) R(146)=K(146)•Y(19)•Y(11) R(147)=K(147)•Y(26)•Y(10) R(148)=K(148)•Y(26)•Y(7)•Y(57) R(149)=K(149)•Y(17)•Y(30) R(150)=K(150)•Y(5)•Y(30) R(151)=K(151)•Y(5)•Y(30) R(152)=K(152)•Y(4)•Y(30) R(153)=K(153)•Y(3)•Y(30) R(154)=K(154)•Y(6)•Y(30) R(155)=K(155)•Y(1)•Y(30) R(156)=K(156)•Y(40)•Y(30) R(157)=K(157)•Y(51)•Y(30) R(158)=K(158)•Y(52)•Y(30) R(159)=K(159)•Y(53)•Y(30) R(160)=K(160)•Y(8)•Y(8)•Y(30) R(161)=K(161)•Y(9)•Y(30) R(162)=K(162)•Y(4)•Y(8)•Y(57) R(163)=K(163)•Y(39)•Y(57) R(164)=K(164)•Y(39)•Y(27) R(165)=K(165)•Y(5)•Y(25)•Y(23) R(166)=K(166)•Y(5)•Y(13)•Y(57) R(167)=K(167)•Y(28)•Y(8) R(168)=K(168)•Y(3)•Y(23) R(169)=K(169)•Y(3)•Y(8) R(170)=K(170)•Y(41)•Y(13)•Y(57) R(171)=K(171)•Y(41)•Y(23)•Y(23)	GIONEUT 2709 GIONEUT 2710 GIONEUT 2711 GIONEUT 2712 GIONEUT 2713 GIONEUT 2714 GIONEUT 2715 GIONEUT 2716 GIONEUT 2717 GIONEUT 2718 GIONEUT 2719 GIONEUT 2720 GIONEUT 2721 GIONEUT 2722 GIONEUT 2723 GIONEUT 2724 GIONEUT 2725 GIONEUT 2726 GIONEUT 2727 GIONEUT 2728 GIONEUT 2729 GIONEUT 2730 GIONEUT 2731 GIONEUT 2732 GIONEUT 2733 GIONEUT 2734 GIONEUT 2735 GIONEUT 2736 GIONEUT 2737 GIONEUT 2738 GIONEUT 2739 GIONEUT 2740 GIONEUT 2741 GIONEUT 2742 GIONEUT 2743 GIONEUT 2744 GIONEUT 2745 GIONEUT 2746 GIONEUT 2747 GIONEUT 2748 GIONEUT 2749 GIONEUT 2750 GIONEUT 2751 GIONEUT 2752 GIONEUT 2753 GIONEUT 2754 GIONEUT 2755 GIONEUT 2756 GIONEUT 2757 GIONEUT 2758 GIONEUT 2759 GIONEUT 2760 GIONEUT 2761 GIONEUT 2762 GIONEUT 2763 GIONEUT 2764 GIONEUT 2765
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230	R(172)=K(172)*Y(42)*Y(13)*Y(57)	GIONEUT	2766
	R(173)=K(173)*Y(43)*Y(13)*Y(57)	GIONEUT	2767
	R(174)=K(174)*Y(43)*Y(57)	GIONEUT	2768
	R(175)=K(175)*Y(44)*Y(57)	GIONEUT	2769
	R(176)=K(176)*Y(45)*Y(57)	GIONEUT	2770
	R(177)=K(177)*Y(51)*Y(3)*Y(57)	GIONEUT	2771
235	R(178)=K(178)*Y(52)*Y(13)*Y(57)	GIONEUT	2772
	R(179)=K(179)*Y(31)*Y(8)*Y(8)	GIONEUT	2773
	R(180)=K(180)*Y(32)*Y(8)*Y(8)	GIONEUT	2774
	R(181)=K(181)*Y(32)*Y(8)*Y(25)	GIONEUT	2775
	R(182)=K(182)*Y(33)*Y(25)	GIONEUT	2776
240	R(183)=K(183)*Y(34)*Y(57)	GIONEUT	2777
	R(184)=K(184)*Y(37)*Y(18)	GIONEUT	2778
	R(185)=K(185)*Y(7)	GIONEUT	2779
	R(186)=K(186)*Y(8)	GIONEUT	2780
245	R(187)=K(187)*Y(23)	GIONEUT	2781
	R(188)=K(188)*Y(18)	GIONEUT	2782
	R(189)=K(189)*Y(16)	GIONEUT	2783
	R(190)=K(190)*Y(19)	GIONEUT	2784
	R(191)=K(191)*Y(29)	GIONEUT	2785
250	P(192)=K(192)*Y(8)	GIONEUT	2786
	R(193)=K(193)*Y(8)	GIONEUT	2787
	R(194)=K(194)*Y(9)	GIONEUT	2788
	R(195)=K(195)*Y(9)	GIONEUT	2789
255	R(196)=K(196)*Y(13)	GIONEUT	2790
	R(197)=K(197)*Y(14)	GIONEUT	2791
	R(198)=K(198)*Y(12)	GIONEUT	2792
	R(199)=K(199)*Y(18)	GIONEUT	2793
	R(200)=K(200)*Y(19)	GIONEUT	2794
260	R(201)=K(201)*Y(24)	GIONEUT	2795
	R(202)=K(202)*Y(55)	GIONEUT	2796
	R(203)=K(203)*Y(25)	GIONEUT	2797
	R(204)=K(204)*Y(25)	GIONEUT	2798
	R(205)=K(205)*Y(56)	GIONEUT	2799
265	R(206)=K(206)*Y(7)	GIONEUT	2800
	R(207)=K(207)*Y(20)	GIONEUT	2801
	R(208)=K(208)*Y(23)	GIONEUT	2802
	R(209)=K(209)*Y(8)	GIONEUT	2803
	R(210)=K(210)*Y(8)	GIONEUT	2804
	R(211)=K(211)*Y(7)	GIONEUT	2805
270	R(212)=K(212)*Y(7)	GIONEUT	2806
	R(213)=K(213)*Y(23)	GIONEUT	2807
	R(214)=K(214)*Y(8)	GIONEUT	2808
	R(215)=K(215)*Y(23)	GIONEUT	2809
275	NN=NREAC+NREAC2	GIONEUT	2810
	WRITE(6,20) (J,CYMB(I,J),I=1,6),K(J),R(J),J=1,NN)	GIONEUT	2811
	FORMAT(14,5A10,A8,9X,1PE12.5,9X,E12.5)	GIONEUT	2812
	RETURN	GIONEUT	2813
	END	GIONEUT	2814





## References

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- C2. Cieslik, S., and Nicolet, M. (1973) The aeronomic dissociation of nitric oxide, Planet. Space Sci. 21:925-938.
- C3. List, R.J., Ed. (1963) Smithsonian Meteorological Tables, Sixth Revised Edition, Washington, D.C.

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